

## DESCRIPTION

The MP2158 is a monolithic step-down switch mode converter with built-in internal power MOSFETs. It achieves 1A continuous output current from a 2.5V to 6V input voltage with excellent load and line regulation. The output voltage can be regulated as low as 0.6V.

The Constant-On-Time control scheme provides fast transient response and eases loop stabilization. Fault condition protection includes cycle-by-cycle current limiting and thermal shutdown.

The MP2158 is available in the small QFN8 2.0x1.5mm package and requires a minimum number of readily available standard external components.

The MP2158 is ideal for a wide range of applications including High Performance DSPs, FPGAs, PDAs, and portable instruments.

## FEATURES

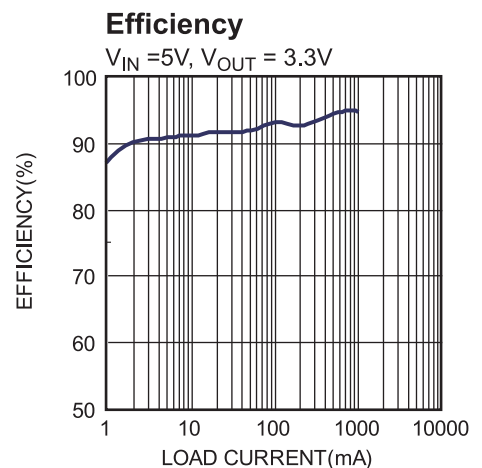
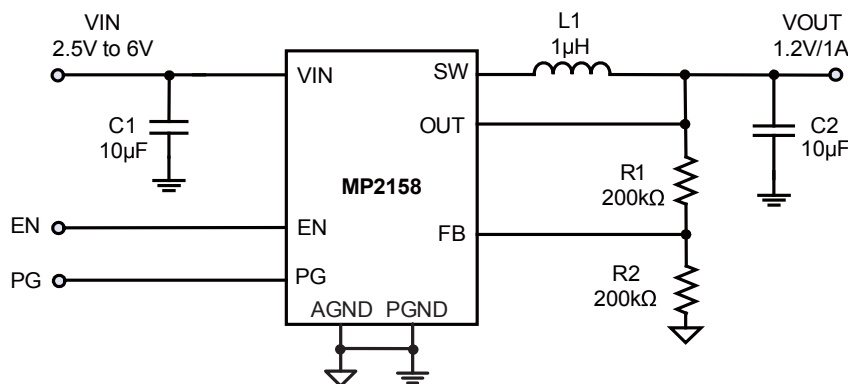
- Very Low I<sub>Q</sub>: 17 $\mu$ A
- Default 1.5MHz Switching Frequency
- EN and Power Good for Power Sequencing
- Ultra-small 2.0x1.5mm QFN8 Package
- Wide 2.5V to 6V Operating Input Range Output Adjustable from 0.6V
- Up to 1A Output Current
- 100% Duty Cycle in Dropout
- 118m $\Omega$  and 88m $\Omega$  Internal Power MOSFET Switches
- Cycle-by-Cycle Over Current Protection
- Short Circuit Protect with Hiccup Mode
- Stable with Low ESR Output Ceramic Capacitors

## APPLICATIONS

- Wireless/Networking Cards
- Portable Instruments
- Battery Powered Devices
- Low Voltage I/O System Power

All MPS parts are lead-free and adhere to the RoHS directive. For MPS green status, please visit MPS website under Products, Quality Assurance page.  
"MPS" and "The Future of Analog IC Technology" are registered trademarks of Monolithic Power Systems, Inc.

## TYPICAL APPLICATION



### ORDERING INFORMATION

Part Number*	Package	Top Marking
MP2158GQH	QFN-8 (2.0mmx1.5mm)	See Below

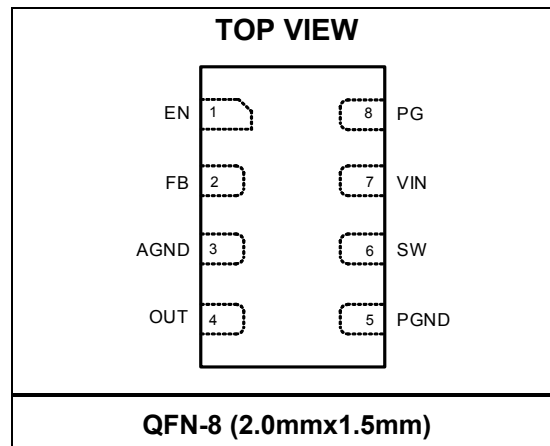
\* For Tape & Reel, add suffix –Z (e.g. MP2158GQH–Z);

### TOP MARKING

—  
BE  
LL

BE: product code of MP2158GQH;  
LL: lot number;

### PACKAGE REFERENCE



#### ABSOLUTE MAXIMUM RATINGS <sup>(1)</sup>

Supply Voltage  $V_{IN}$  ..... 6.5V  
 $V_{SW}$  .....  
 -0.3V (-1.5V for <20ns&-4V for <8ns) to 6.5V  
 (10V for <10ns)  
 All Other Pins .....-0.3V to 6.5 V  
 Junction Temperature ..... 150°C  
 Lead Temperature ..... 260°C  
 Continuous Power Dissipation ( $T_A = +25^\circ\text{C}$ ) <sup>(2)</sup>  
 ..... 1.14W  
 Storage Temperature ..... -65°C to +150°C

#### Recommended Operating Conditions <sup>(3)</sup>

Supply Voltage  $V_{IN}$  ..... 2.5V to 6V  
 Operating Junction Temp. ( $T_J$ ). -40°C to +125°C

**Thermal Resistance <sup>(4)</sup>**  $\theta_{JA}$   $\theta_{JC}$   
 QFN-8 (2.0mmx1.5mm)..... 110 ..... 55... °C/W

#### Notes:

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature  $T_J$  (MAX), the junction-to-ambient thermal resistance  $\theta_{JA}$ , and the ambient temperature  $T_A$ . The maximum allowable continuous power dissipation at any ambient temperature is calculated by  $P_D$  (MAX) =  $(T_J$  (MAX)- $T_A$ )/ $\theta_{JA}$ . Exceeding the maximum allowable power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 3) The device is not guaranteed to function outside of its operating conditions.
- 4) Measured on JESD51-7, 4-layer PCB.

**ELECTRICAL CHARACTERISTICS <sup>(5)</sup>**
 **$V_{IN} = 5V$ ,  $T_A = +25^{\circ}C$ , unless otherwise noted.**

Parameter	Symbol	Condition	Min	Typ	Max	Units
Feedback Voltage	$V_{FB}$	$2.5V \leq V_{IN} \leq 6V$	-3%	0.600	+3%	V/%
		$T_A = -40^{\circ}C$ to $+85^{\circ}C$ <sup>(6)</sup>	-3.5%		+3.5%	
Feedback Current	$I_{FB}$	$V_{FB} = 0.6V$		10	50	nA
PFET Switch On Resistance	$R_{DSON\_P}$			118		m $\Omega$
NFET Switch On Resistance	$R_{DSON\_N}$			88		m $\Omega$
Switch Leakage		$V_{EN} = 0V$ , $V_{IN} = 6V$ $V_{SW} = 0V$ and $6V$		0	1	$\mu A$
PFET Current Limit				2		A
ON Time	$T_{ON}$	$V_{IN}=5V$ , $V_{OUT}=1.2V$		185		ns
		$V_{IN}=3.6V$ , $V_{OUT}=1.2V$		245		
Switching frequency	$F_s$	$V_{OUT}=1.2V$	-20%	1500	+20%	kHz/%
		$T_A = -40^{\circ}C$ to $+85^{\circ}C$ <sup>(6)</sup>	-25%	1500	+25%	kHz/%
Minimum Off Time	$T_{MIN-OFF}$			60		ns
Soft-Start Time	$T_{SS-ON}$			1.5		ms
Power Good Upper Trip Threshold	$PG_H$	FB voltage respect to the regulation		+10		%
Power Good Lower Trip Threshold	$PG_L$			-10		%
Power Good Delay	$PG_D$			50		$\mu s$
Power Good Sink Current Capability	$V_{PG-L}$	Sink 1mA			0.4	V
Power Good Logic High Voltage	$V_{PG-H}$	$V_{IN}=5V$ , $V_{FB}=0.6V$	4.9			V
Power Good Internal Pull Up Resistor	$R_{PG}$			550		k $\Omega$
Under Voltage Lockout Threshold Rising			2.15	2.3	2.45	V
Under Voltage Lockout Threshold Hysteresis				260		mV
EN Input Logic Low Voltage					0.4	V
EN Input Logic High Voltage			1.2			V
EN Input Current		$V_{EN}=2V$		1.5		$\mu A$
		$V_{EN}=0V$		0		$\mu A$
Supply Current (Shutdown)		$V_{EN}=0V$		0	1	$\mu A$
Supply Current (Quiescent)		$V_{EN}=2V$ , $V_{FB}=0.63V$ , $V_{IN}=5V$		17	20	$\mu A$
Thermal Shutdown <sup>(5)</sup>				150		$^{\circ}C$
Thermal Hysteresis <sup>(5)</sup>				30		$^{\circ}C$

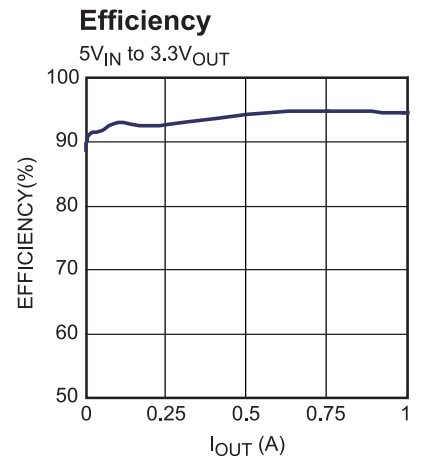
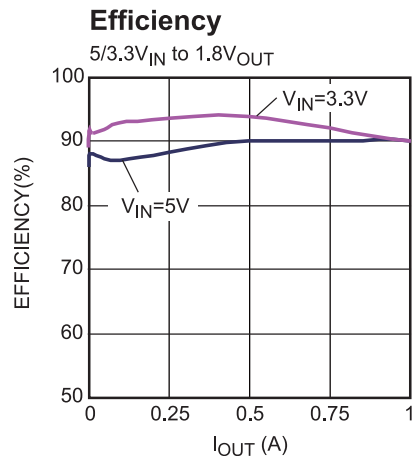
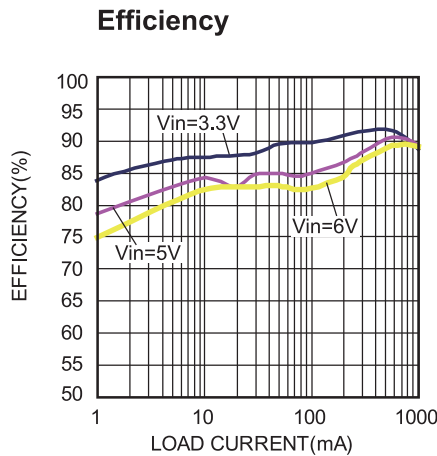
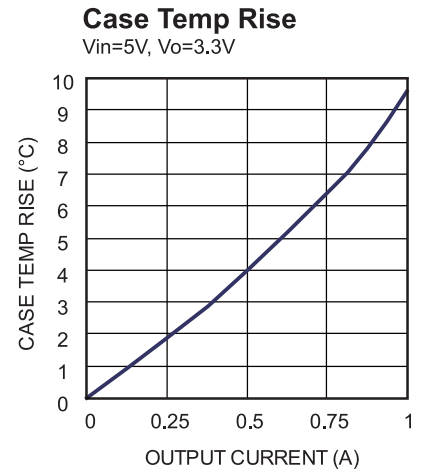
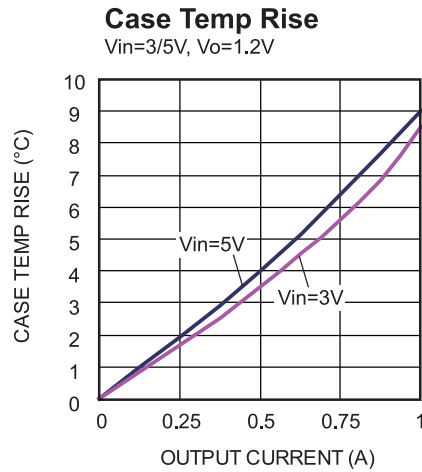
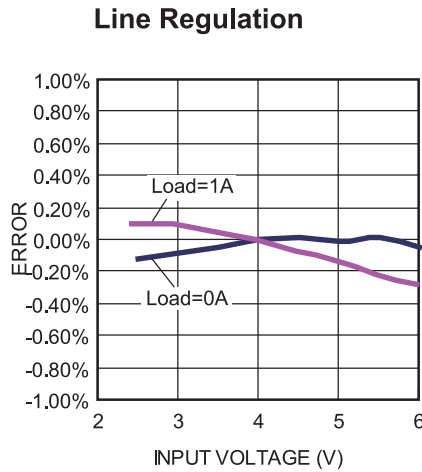
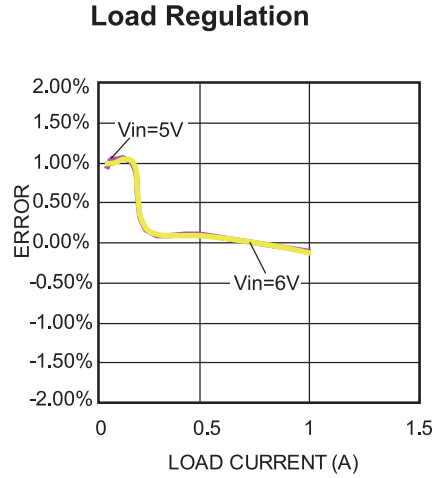
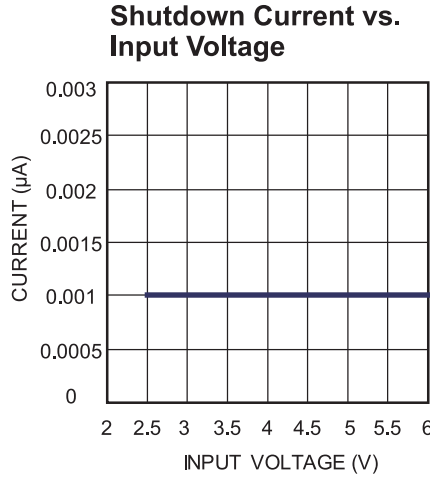
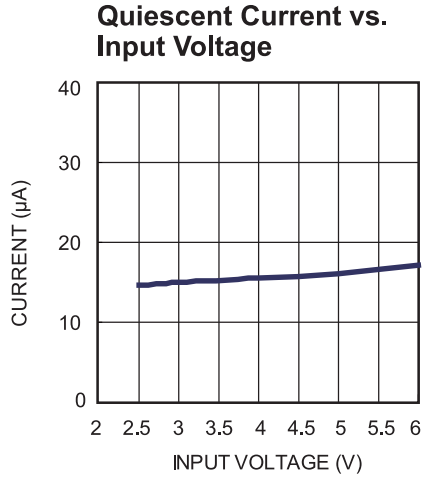
**Notes:**

5) Guaranteed by design.

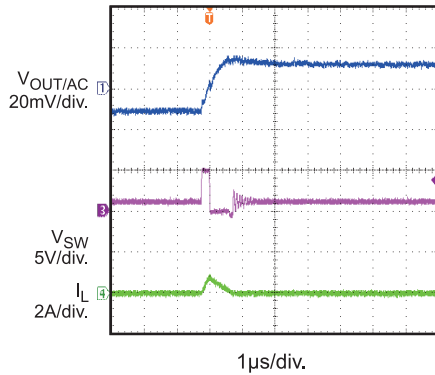
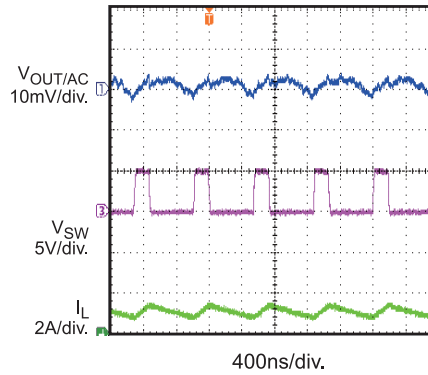
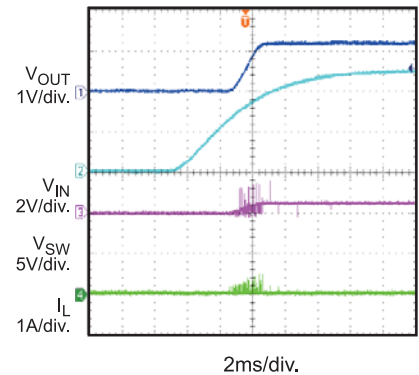
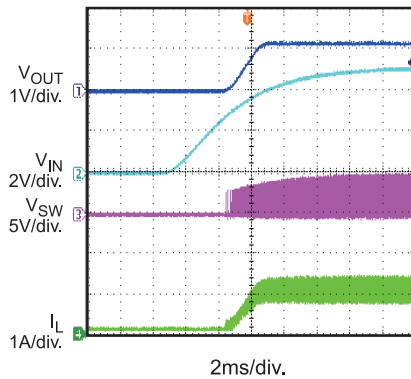
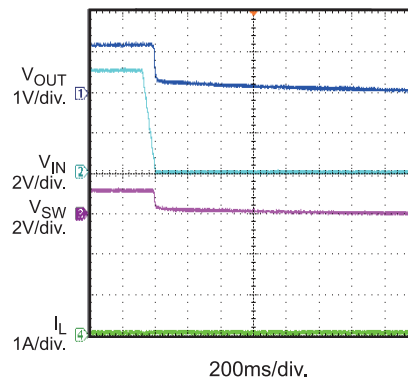
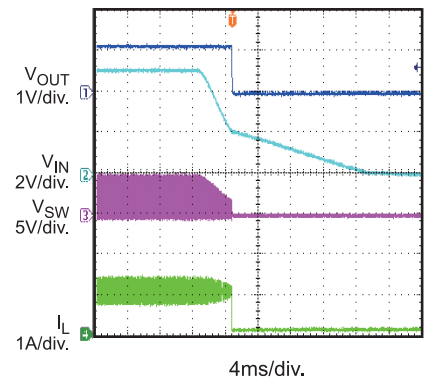
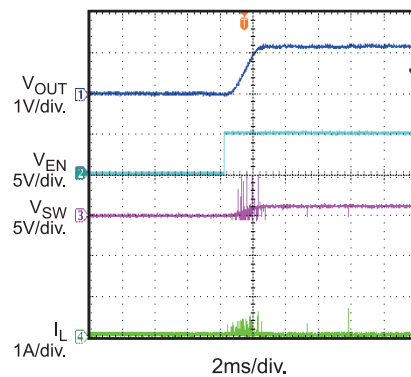
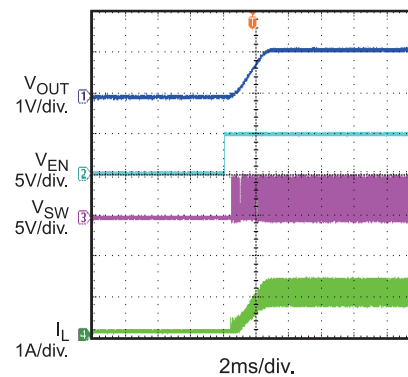
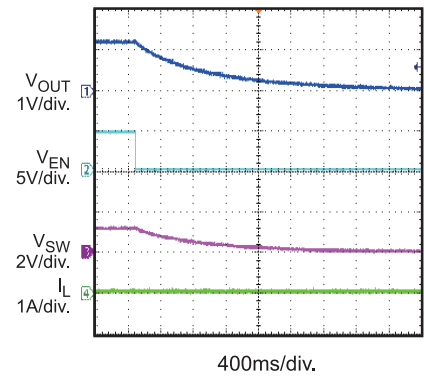
6) Guaranteed by characterization test.

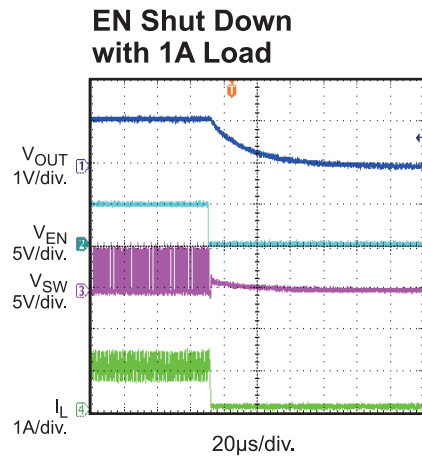
## TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$ ,  $L = 1.0\mu H$ ,  $T_A = +25^\circ C$ , unless otherwise noted.



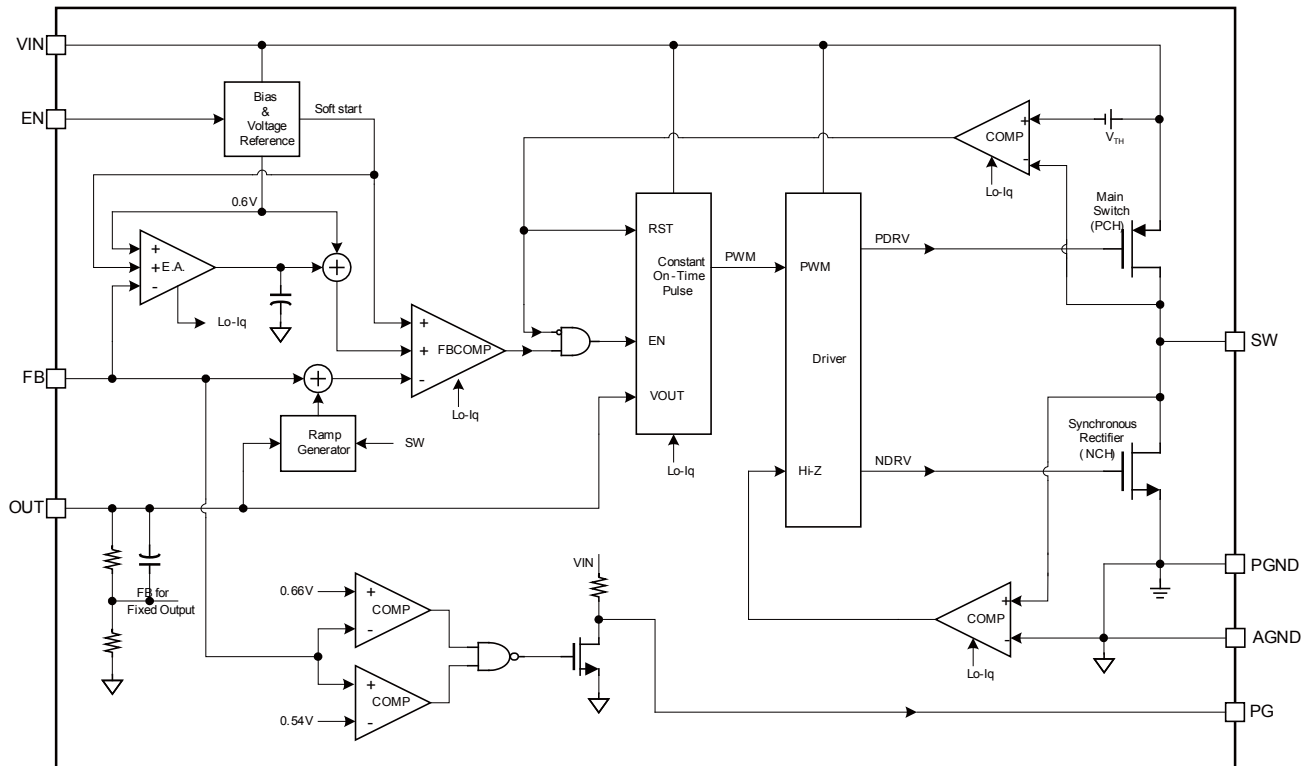
**TYPICAL PERFORMANCE CHARACTERISTICS (continued)**
 $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$ ,  $L = 1.0\mu H$ ,  $T_A = +25^\circ C$ , unless otherwise noted.

**Output Ripple**

**Output Ripple**

**VIN Power Up without Load**

**VIN Power Up with 1A Load**

**VIN Shut Down without Load**

**VIN Shut Down with 1A Load**

**EN Start Up without Load**

**EN Start Up with 1A Load**

**EN Shut Down without Load**


**TYPICAL PERFORMANCE CHARACTERISTICS** *(continued)* $V_{IN} = 5V$ ,  $V_{OUT} = 1.2V$ ,  $L = 1.0\mu H$ ,  $T_A = +25^\circ C$ , unless otherwise noted

## PIN FUNCTIONS

Pin #	Name	Description
1	EN	On/Off Control
2	FB	Feedback pin. An external resistor divider from the output to AGND, tapped to the FB pin, sets the output voltage.
3	AGND	Analogy ground for internal control circuit
4	OUT	Input sense pin for output voltage
5	PGND	Power ground
6	SW	Switch Output
7	VIN	Supply Voltage. The MP2158 operates from a +2.5V to +6V unregulated input. C1 is needed to prevent large voltage spikes from appearing at the input.
8	PG	Power Good Indicator. The output of this pin is an open drain with internal pull up resistor to VIN. PG is pulled up to VIN when the FB voltage is within $\pm 10\%$ of the regulation level, if FB voltage is out of that regulation range, it is LOW.

**BLOCK DIAGRAM**

**Figure 1: MP2158 Block Diagram**



## OPERATION

MP2158 uses constant on-time control with input voltage feed forward to stabilize the switching frequency over full input range. At light load, MP2158 employs a proprietary control of low side switch and inductor current to eliminate ringing on switching node and improve efficiency.

### Constant On-time Control

Compare to fixed frequency PWM control, constant on-time control offers the advantage of simpler control loop and faster transient response. By using input voltage feed forward, MP2158 maintains a nearly constant switching frequency across input and output voltage range. The on-time of the switching pulse can be estimated as:

$$T_{ON} = \frac{V_{OUT}}{V_{IN}} \cdot 0.667\mu s$$

To prevent inductor current run away during load transient, MP2158 fixes the minimum off time to be 60ns. However, this minimum off time limit will not affect operation of MP2158 in steady state in any way.

### Light Load Operation

In light load condition, MP2158 uses a proprietary control scheme to save power and improve efficiency. The MP2158 will turn off the low side switch when inductor current starts to reverse. Then MP2158 works in discontinuous conduction mode (DCM) operation.

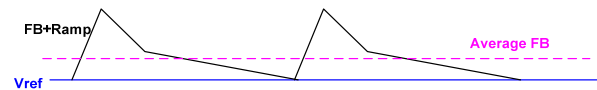
The DCM mode happens only after low side switch turned off by ZCD circuit. Considering the ZCD circuit propagation time, the typical delay is 30ns. It means the inductor current still fall after the ZCD is trigger during this delay. If the inductor current falling slew rate is fast ( $V_o$  voltage is high or close to  $V_{in}$ ), the low side MOSFET is turned off at the moment inductor current may be negative. This phenomena will cause MP2158 can not enter DCM operation. If the DCM mode is required, the off time of low side MOSFET in CCM should be longer than 60ns. It means the maximum duty is 90% to guarantee DCM mode at light load.

For example,  $V_{IN}$  is 3.4V and  $V_{OUT}$  is 3.3V, the off time in CCM is 20ns. It is difficult to enter DCM at light load. And using smaller inductor can improve it and make it enter DCM easily.

### Sleep/DCM Mode Transition

MP2158 features sleep mode to get higher extreme light load efficiency. Operating in sleep mode, IC consumes ultra low quiescent current, typical 17uA here.

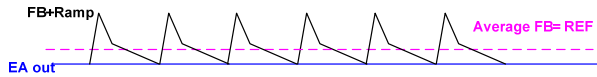
At extreme light load condition, when internal error amplifier output (EAO) drop to sleep threshold and next pulse interval is longer than 4μs typically, IC enters into sleep mode to improve efficiency. Both EAO and pulse interval meet upper condition, IC works in sleep mode. In sleep mode, IC disables the most parts of internal control circuits to lower the quiescent current. At this time, Error amplifier will dominate the output voltage, FB voltage plus internal Ramp ripple compare with reference voltage. When FB voltage plus internal Ramp ripple drop to touch reference voltage, the IC wakes up previous disabled circuits and SW pulse happens. If the EAO and pulse interval meet the sleep condition, the IC will enter sleep mode again. Operating in sleep mode, average FB is above on the reference voltage, output voltage is a little higher than normal value. At the same time, pulse width in sleep mode is a little longer than normal SW on pulse, it because that wake up other control circuits need some delay time.



**Figure 2: Sleep Mode Control**

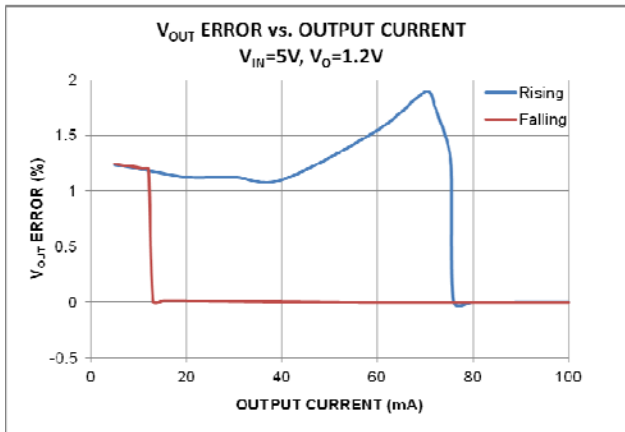
With load increasing, the output ripple is decreasing. The EAO ripple also decreases. Either EAO cannot reach sleep threshold or pulse interval is less than 4μs typically, IC quit sleep mode and works in DCM (Discontinue Control Mode). In DCM mode, all the internal control circuits work normally. Error amplifier and FBCOMP comparator will dominate the output voltage together. FB voltage plus internal Ramp ripple compare with EAO. And the EAO will self-adjust to get FB equal to REF. When FB voltage plus internal Ramp ripple drops to

touch EA output, the IC SW pulse happen. In DCM mode, output voltage is equal to normal value. And the pulse width in DCM mode is normal SW on pulse.



**Figure 3: DCM Mode Control**

Due to sleep mode and DCM operated under different control logic, the mode transition has a hysteresis. The hysteresis is related to input voltage, output voltage, inductor and output capacitor. Below is a typical hysteresis voltage.



**Figure 4: Sleep/DCM Transition @  $V_{IN}=5V$ ,  $V_{OUT}=1.2V$**

### Enable

When input voltage is greater than the under-voltage lockout threshold (UVLO), typically 2.3V, MP2158 can be enabled by pulling EN pin to higher than 1.2V. Leaving EN pin float or pull down to ground will disable MP2158. There is an internal 1Meg Ohm resistor from EN pin to ground.

### Soft Start

MP2158 has built-in soft start that ramps up the output voltage in a controlled slew rate, avoiding overshoot at startup. The soft start time is about 1.5ms typical.

### Power GOOD Indicator

MP2158 has an open drain with 550k $\Omega$  pull-up resistor pin for power good indicator PG. When FB pin is within +/-10% of regulation voltage, i.e. 0.6V, PG pin is pulled up to  $V_{IN}$  by the internal resistor. If FB pin voltage is out of the +/-10% window, PG pin is pulled down to ground by an internal MOSFET. The MOSFET has a maximum  $R_{dson}$  of less than 150 $\Omega$ .

### Current limit

MP2158 has a typical 2A current limit for the high side switch. When the high side switch hits current limit, MP2158 will touch the hiccup threshold until the current lower down. This will prevent inductor current from continuing to build up which will result in damage of the components.

### Short Circuit and Recovery

MP2158 enters short circuit protection mode also when the current limit is hit, and tries to recover from short circuit with hiccup mode. In short circuit protection, MP2158 will disable output power stage, discharge soft-start cap and then automatically try to soft-start again. If the short circuit condition still holds after soft-start ends, MP2158 repeats this operation cycle till short circuit disappears and output rises back to regulation level.

## APPLICATION INFORMATION

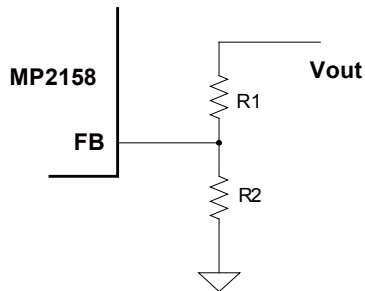
### COMPONENT SELECTION

#### Setting the Output Voltage

The external resistor divider is used to set the output voltage (see Typical Application on page 1). The feedback resistor R1 can not be too large neither too small considering the trade-off for stability and dynamic. Choose R1 to be around 120kΩ to 200kΩ. R2 is then given by:

$$R2 = \frac{R1}{\frac{V_{out}}{0.6} - 1}$$

The feedback circuit is shown as Figure 5.



**Figure 5: Feedback Network**

Table 1 lists the recommended resistors value for common output voltages.

**Table 1—Resistor Selection for Common Output Voltages**

V <sub>OUT</sub> (V)	R1 (kΩ)	R2 (kΩ)
1.0	200(1%)	300(1%)
1.2	200(1%)	200(1%)
1.8	200(1%)	100(1%)
2.5	200(1%)	63.2(1%)
3.3	200(1%)	44.2(1%)

#### Selecting the Inductor

A 0.68μH to 2.2μH inductor is recommended for most applications. For highest efficiency, the inductor DC resistance should be less than 15mΩ. For most designs, the inductance value can be derived from the following equation.

$$L_1 = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} \times \Delta I_L \times f_{OSC}}$$

Where ΔI<sub>L</sub> is the inductor ripple current.

Choose inductor current to be approximately 30% of the maximum load current. The maximum inductor peak current is:

$$I_{L(MAX)} = I_{LOAD} + \frac{\Delta I_L}{2}$$

#### Selecting the Input Capacitor

The input current to the step-down converter is discontinuous, therefore a capacitor is required to supply the AC current to the step-down converter while maintaining the DC input voltage. Use low ESR capacitors for the best performance. Ceramic capacitors with X5R or X7R dielectrics are highly recommended because of their low ESR and small temperature coefficients. For most applications, a 10μF capacitor is sufficient. For higher output voltage, 47μF may be needed for more stable system.

Since the input capacitor absorbs the input switching current it requires an adequate ripple current rating. The RMS current in the input capacitor can be estimated by:

$$I_{C1} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)}$$

The worse case condition occurs at V<sub>IN</sub> = 2V<sub>OUT</sub>, where:

$$I_{C1} = \frac{I_{LOAD}}{2}$$

For simplification, choose the input capacitor whose RMS current rating greater than half of the maximum load current.

The input capacitor can be electrolytic, tantalum or ceramic. When using electrolytic or tantalum capacitors, a small and high quality ceramic capacitor, i.e. 0.1μF, should be placed as close to the IC as possible. When using ceramic capacitors, make sure that they have enough capacitance to provide sufficient charge to prevent excessive voltage ripple at input. The input voltage ripple caused by capacitance can be estimated by:

$$\Delta V_{IN} = \frac{I_{LOAD}}{f_s \times C1} \times \frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

### Selecting the Output Capacitor

The output capacitor (C2) is required to maintain the DC output voltage. Ceramic capacitors are recommended. Low ESR capacitors are preferred to keep the output voltage ripple low. The output voltage ripple can be estimated by:

$$\Delta V_{OUT} = \frac{V_{OUT}}{f_s \times L_1} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \times \left(R_{ESR} + \frac{1}{8 \times f_s \times C2}\right)$$

Where  $L_1$  is the inductor value and  $R_{ESR}$  is the equivalent series resistance (ESR) value of the output capacitor.

Using ceramic capacitors, the impedance at the switching frequency is dominated by the capacitance. The output voltage ripple is mainly caused by the capacitance. For simplification, the output voltage ripple can be estimated by:

$$\Delta V_{OUT} = \frac{V_{OUT}}{8 \times f_s^2 \times L_1 \times C2} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

In the case of tantalum or electrolytic capacitors, the ESR dominates the impedance at the switching frequency. For simplification, the output ripple can be approximated to:

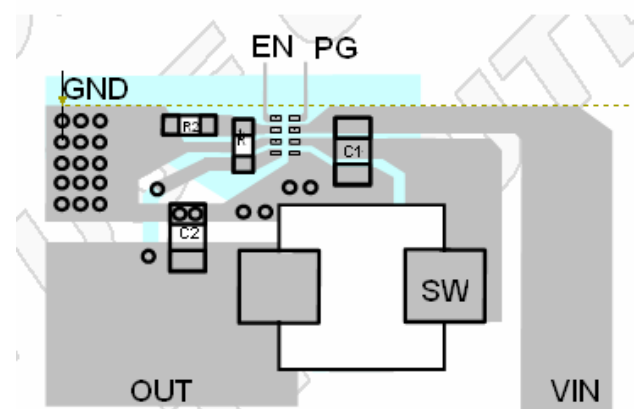
$$\Delta V_{OUT} = \frac{V_{OUT}}{f_s \times L_1} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \times R_{ESR}$$

The characteristics of the output capacitor also affect the stability of the regulation system.

### PCB Layout

Proper layout of the switching power supplies is very important, and sometimes critical for proper function. For the high-frequency switching converter, poor layout design can result in poor line or load regulation and stability issues.

The high current paths (GND, VIN and SW) should be placed very close to the device with short, direct and wide traces. The input capacitor needs to be as close as possible to the VIN and GND pins. The external feedback resistors should be placed next to the FB pin. Keep the switching node SW short and away from the feedback network.



**Figure 5: PCB Layout Recommendation**

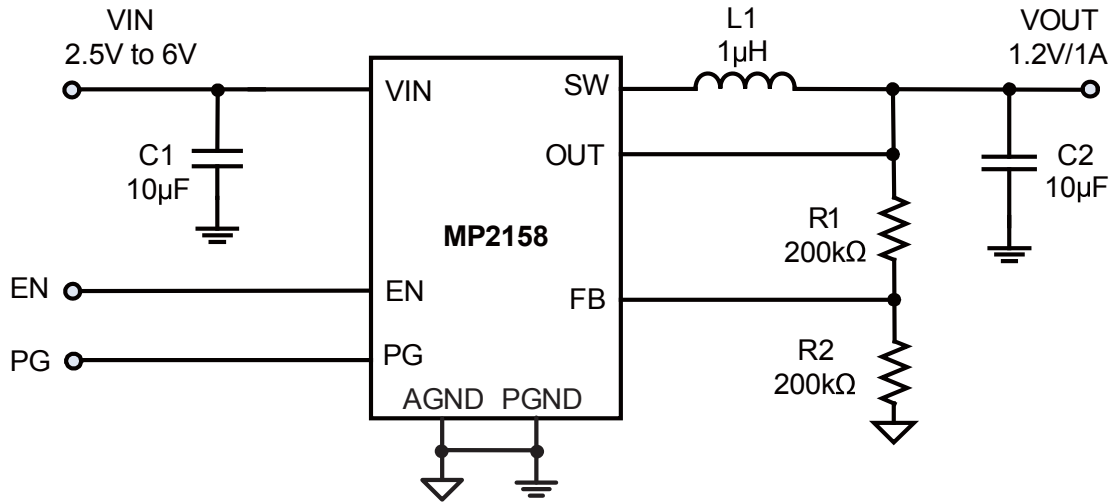
### Design Example

Below is a design example following the application guidelines for the specifications:

**Table 2: Design Example**

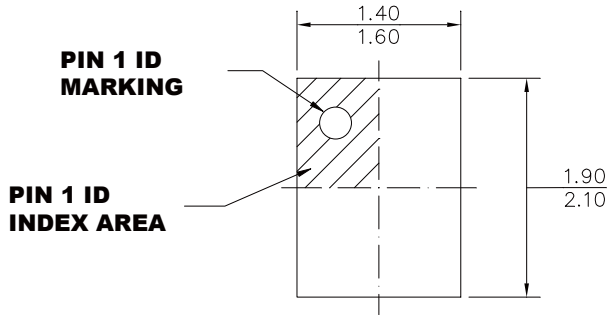
$V_{IN}$	5V
$V_{OUT}$	1.2V
$f_{SW}$	1500kHz

The detailed application schematic is shown in Figure 6. The typical performance and circuit waveforms have been shown in the Typical Performance Characteristics section. For more device applications, please refer to the related Evaluation Board Datasheets.

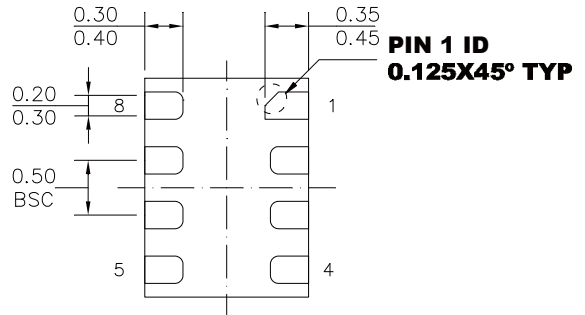
**TYPICAL APPLICATION CIRCUITS**

**Figure 6: Typical Application Circuit**

**PACKAGE INFORMATION**

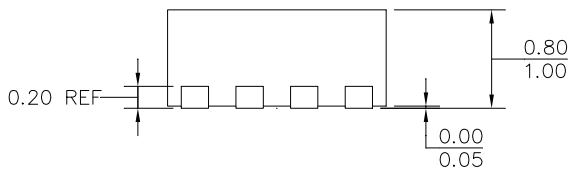
**QFN-8 (2.0mmX1.5mm)**



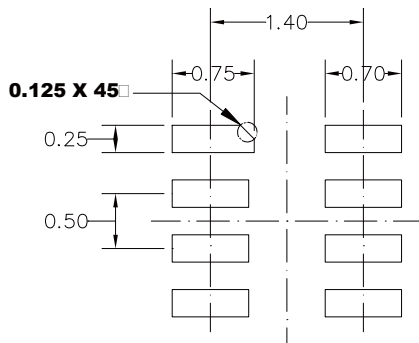
**TOP VIEW**



**BOTTOM VIEW**



**SIDE VIEW**



**RECOMMENDED LAND PATTERN**

**NOTE:**

- 1) ALL DIMENSIONS ARE IN MILLIMETERS.
- 2) EXPOSED PADDLE SIZE DOES NOT INCLUDE MOLD FLASH.
- 3) LEAD COPLANARITY SHALL BE 0.10 MILLIMETERS MAX.
- 4) JEDEC REFERENCE IS MO-220.
- 5) DRAWING IS NOT TO SCALE.

**NOTICE:** The information in this document is subject to change without notice. Please contact MPS for current specifications. Users should warrant and guarantee that third party Intellectual Property rights are not infringed upon when integrating MPS products into any application. MPS will not assume any legal responsibility for any said applications.