

# TPS2597xx 具有精确电流监视器和瞬态过流消隐功能的 2.7V 至 23V、7A、9.8mΩ 电子保险丝

## 1 特性

- 宽工作输入电压范围：2.7V 至 23V
  - 绝对最大值为 28V
- 具有低导通电阻的集成 FET： $R_{ON} = 9.8m\Omega$  (典型值)
- 快速过压保护
  - 过压钳位 (OVC)，可通过引脚选择阈值 (3.89V、5.76V、13.88V)，响应时间为 5 $\mu$ s (典型值)，或
  - 可调节过压锁定 (OVLO)，响应时间为 1.2 $\mu$ s (典型值)
- 过流保护，具有负载电流监控器输出 (ILM)
  - 主动电流限制或断路器选项
  - 可调节阈值 ( $I_{LIM}$ )：0.87A 至 7.7A
    - $I_{LIM} > 1.74 A$  时精度为  $\pm 10\%$
  - 可调瞬态消隐计时器 (ITIMER)，支持高达  $2 \times I_{LIM}$  的峰值电流
  - 输出负载电流监控精度： $\pm 8\%$  (最大值)
- 通过快速跳变响应实现短路保护
  - 响应时间为 550ns (典型值)
  - 可调节 ( $2 \times I_{LIM}$ ) 和固定阈值
- 带有可调节欠压锁定阈值 (UVLO) 的高电平有效使能输入
- 可调节的输出压摆率控制 (dVdt)
- 过热保护
- 数字输出
  - 故障指示 (FLT) 或
  - 具有可调节阈值 (PGTH) 的电源正常状态指示 (PG)
- UL2367 认证 (正在申请中)
- IEC 62368 CB 认证 (正在申请中)
- 小尺寸：QFN 2mm  $\times$  2mm，0.45mm 间距

## 2 应用

- 服务器、PC 主板和插件卡
- 企业级存储 - RAID/HBA/SAN/eSSD
- 患者监护仪
- 电器和电动工具
- 零售销售点终端
- 智能手机和平板电脑

## 3 说明

TPS2597xx 系列电子保险丝是采用小型封装的高度集成电路保护和电源管理解决方案。此类器件只需很少的外部元件即可提供多种保护模式，能够非常有效地抵御过载、短路、电压浪涌和过多浪涌电流。

可以使用单个外部电容器来调节输出压摆率和浪涌电流。通过将输出钳制到安全的固定最大电压 (可通过引脚选择) 或在输入超过可调过压阈值时切断输出，可以保护负载免受输入过压情况的影响。此类器件通过主动限制电流或断开电路来响应输出过载。用户可以调节输出电流限制阈值以及瞬态过流消隐计时器。电流限制控制引脚还用作模拟负载电流监控器。

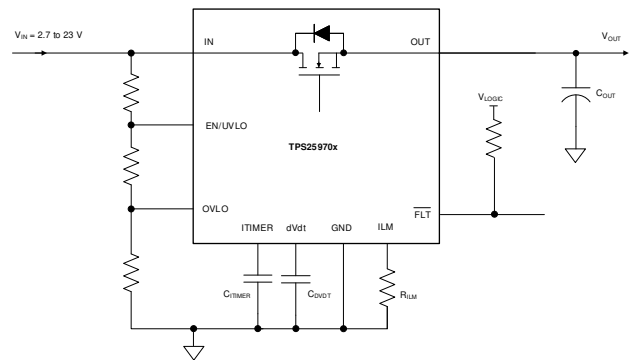
器件采用 2mm  $\times$  2mm 10 引脚 HotRod™ QFN 封装，旨在改善热性能并减小系统尺寸。

这些器件的额定工作结温范围为  $-40^{\circ}\text{C}$  至  $+125^{\circ}\text{C}$ 。

### 器件信息

器件型号	封装 <sup>(1)</sup>	封装尺寸 (标称值)
TPS2597xxRPW	QFN (10)	2mm $\times$ 2mm

(1) 如需了解所有可用封装，请参阅数据表末尾的可订购产品附录。



简化版原理图



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## 4 Revision History

注：以前版本的页码可能与当前版本的页码不同

Changes from Revision A (December 2021) to Revision B (January 2022)	Page
• Added <i>Thermal Information</i> table to the document.....	5

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Changes from Revision * (November 2021) to Revision A (December 2021)	Page
• 将状态从“预告信息”更改为“量产数据”.....	1

## 5 Device Comparison Table

PART NUMBER	OVERVOLTAGE RESPONSE	OVERCURRENT RESPONSE	PG and PGTH	FLT	RESPONSE TO FAULT
TPS25970ARPW	Adjustable OVLO	Active Current Limit	N	Y	Auto-Retry
TPS25970LRPW					Latch-Off
TPS25972ARPW	Pin Selectable OVC (3.89 V/5.76 V/13.88 V)		Y	N	Auto-Retry
TPS25972LRPW					Latch-Off
TPS25974ARPW	Adjustable OVLO	Circuit Breaker			Auto-Retry
TPS25974LRPW					Latch-Off

## 6 Pin Configuration and Functions

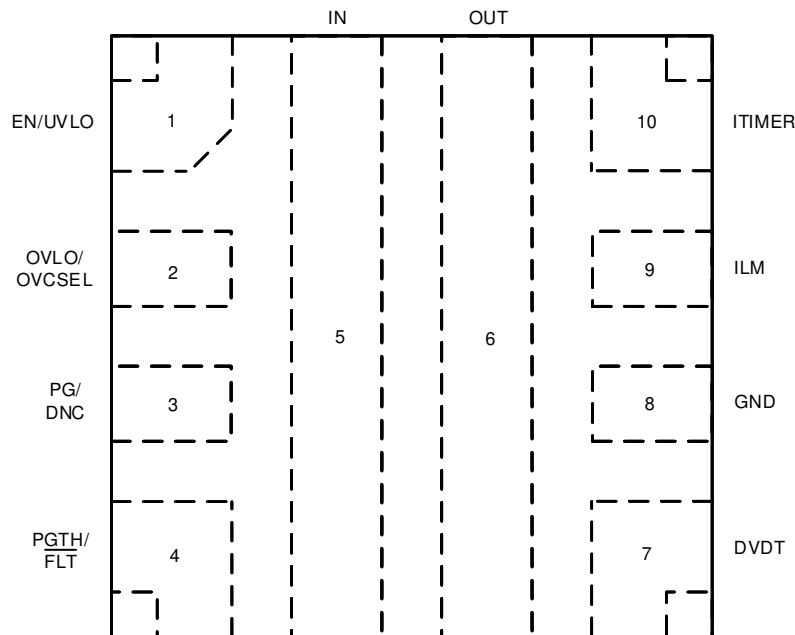


图 6-1. TPS2597xx RPW Package 10-Pin QFN (Top View)

表 6-1. Pin Functions

PIN		TYPE	DESCRIPTION
NAME	NO.		
EN/UVLO	1	Analog Input	Active high enable for the device. A resistor divider on this pin from input supply to GND can be used to adjust the undervoltage lockout threshold. <i>Do not leave floating.</i> Refer to <a href="#">Undervoltage Lockout (UVLO and UVP)</a> for details.
OVLO	2	Analog Input	<i>TPS25970x and TPS25974x:</i> A resistor divider on this pin from supply to GND can be used to adjust the overvoltage lockout threshold. This pin can also be used as an active low enable for the device. <i>Do not leave floating.</i> Refer to <a href="#">Overvoltage Lockout (OVLO)</a> for details.
OVCSEL		Analog Input	<i>TPS25972x:</i> Overvoltage clamp threshold select pin. Refer to <a href="#">Overvoltage Clamp (OVC)</a> for details.
PG	3	Digital Output	<i>TPS25972x and TPS25974x:</i> Power-good indication. This is an open-drain signal, which is asserted high when the internal powerpath is fully turned ON and the PGTH input exceeds a certain threshold. Refer to <a href="#">Power Good Indication (PG)</a> for more details.
DNC		Digital Output	<i>TPS25970x:</i> Can be left floating
FLT	4	Digital Output	<i>TPS25970x:</i> Active low fault event indicator. This pin is an open-drain signal that is pulled low when a fault is detected. Refer to <a href="#">Fault Response and Indication (FLT)</a> for more details.
PGTH		Analog Input	<i>TPS25972x and TPS25974x:</i> Power-good threshold. Refer to <a href="#">Power Good Indication (PG)</a> for more details.
IN	5	Power	Power input
OUT	6	Power	Power output
DVDT	7	Analog Output	A capacitor from this pin to GND sets the output turn on slew rate. Leave this pin floating for the fastest turn on slew rate. Refer to <a href="#">Slew Rate (dVdt) and Inrush Current Control</a> for details.
GND	8	Ground	This pin is the ground reference for all internal circuits and must be connected to system GND.
ILM	9	Analog Output	This pin is a dual function pin used to limit and monitor the output current. An external resistor from this pin to GND sets the output current limit threshold during start-up as well as steady state. The pin voltage can also be used as analog output load current monitor signal. <i>Do not leave floating.</i> Refer to <a href="#">Circuit-Breaker</a> or <a href="#">Active Current Limiting</a> for more details.
ITIMER	10	Analog Output	A capacitor from this pin to GND sets the overcurrent blanking interval during which the output current can temporarily exceed set current limit (but lower than fast-trip threshold) before the device overcurrent response takes action. Leave this pin open for the fastest response to overcurrent events. Refer to <a href="#">Circuit-Breaker</a> or <a href="#">Active Current Limiting</a> for more details.

## 7 Specifications

### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

Parameter		Pin	MIN	MAX	UNIT
V <sub>IN</sub>	Maximum input voltage range, $-40\text{ °C} \leq T_J \leq 125\text{ °C}$	IN	-0.3	28	V
V <sub>OUT</sub>	Maximum output voltage range, $-40\text{ °C} \leq T_J \leq 125\text{ °C}$	OUT	-0.3	V <sub>IN</sub> + 0.3	
V <sub>OUT,PLS</sub>	Minimum output voltage pulse (< 1 $\mu$ s)	OUT	-0.8		
V <sub>EN/UVLO</sub>	Maximum Enable pin voltage range	EN/UVLO	-0.3	6.5	V
V <sub>OV</sub>	Maximum OVCSEL/OVLO pin voltage range	OVCSEL/OVLO	-0.3	6.5	V
V <sub>dVdT</sub>	Maximum dVdT pin voltage range	dVdT	Internally limited		V
V <sub>ITIMER</sub>	Maximum ITIMER pin voltage range	ITIMER	Internally limited		V
V <sub>PGTH</sub>	Maximum PGTH pin voltage range	PGTH	-0.3	6.5	V
V <sub>PG</sub>	Maximum PG pin voltage range	PG	-0.3	6.5	V
V <sub>FLT<math>\bar</math>B</sub>	Maximum FLT pin voltage range	FLT $\bar$	-0.3	6.5	V
V <sub>ILM</sub>	Maximum ILM pin voltage range	ILM	Internally limited		V
I <sub>MAX</sub>	Maximum continuous switch current	IN to OUT	Internally limited		A
T <sub>J</sub>	Junction temperature		Internally limited		°C
T <sub>LEAD</sub>	Maximum lead temperature			300	°C
T <sub>stg</sub>	Storage temperature		-65	150	°C

- (1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

### 7.2 ESD Ratings

			VALUE	UNIT
V <sub>(ESD)</sub>	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	V
		Charged device model (CDM), per ANSI/ESDA/JEDEC JS-002 <sup>(2)</sup>	±500	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.  
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

Parameter		Pin	MIN	MAX	UNIT
V <sub>IN</sub>	Input voltage range	IN	2.7	23 <sup>(1)</sup>	V
V <sub>OUT</sub>	Output voltage range	OUT		V <sub>IN</sub>	V
V <sub>EN/UVLO</sub>	EN/UVLO pin voltage range	EN/UVLO		5 <sup>(2)</sup>	V
V <sub>OV</sub>	OVLO pin voltage range (TPS25970x and TPS25974x variants only)	OVLO	0.5	1.5	V
V <sub>dVdT</sub>	dVdT pin capacitor voltage rating	dVdT	V <sub>IN</sub> + 5 V		V
V <sub>PGTH</sub>	PGTH pin voltage range	PGTH		5	V
V <sub>FLT<math>\bar</math>B</sub>	FLT pin voltage range	FLT		5	V
V <sub>PG</sub>	PG pin voltage range	PG		5	V
V <sub>ITIMER</sub>	ITIMER pin capacitor voltage rating	ITIMER	4		V
R <sub>ILM</sub>	ILM pin resistance to GND	ILM	715	6650	$\Omega$
I <sub>MAX</sub>	Continuous switch current, $T_J \leq 125\text{ °C}$	IN to OUT		7	A
T <sub>J</sub>	Junction temperature		-40	125	°C

- (1) For TPS25972x OVC variants, the input operating voltage must be limited to the selected Output Voltage Clamp Option as listed in the Electrical Characteristics section.

- (2) For supply voltages below 5 V, it is okay to pull up the EN pin to IN directly. For supply voltages greater than 5 V, TI recommends to use a resistor divider with a minimum pullup resistor value of 350 k $\Omega$ .

## 7.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		TPS2597xx	UNIT
		RPW (QFN)	
		10 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	49.7 <sup>(2)</sup>	°C/W
		71.8 <sup>(3)</sup>	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	15.7	°C/W
Ψ <sub>JT</sub>	Junction-to-top characterization parameter	2.1 <sup>(2)</sup>	°C/W
	Junction-to-top characterization parameter	1.3 <sup>(3)</sup>	°C/W
Ψ <sub>JB</sub>	Junction-to-board characterization parameter	23 <sup>(2)</sup>	°C/W
		14.5 <sup>(3)</sup>	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.
- (2) Based on simulations conducted with the device mounted on a custom 4-layer PCB (2s2p) with 8 thermal vias under device.
- (3) Based on simulations conducted with the device mounted on a JEDEC 4-layer PCB (2s2p) with no thermal vias under device.

## 7.5 Electrical Characteristics

(Test conditions unless otherwise noted)  $-40^{\circ}\text{C} \leq T_J \leq 125^{\circ}\text{C}$ ,  $V_{\text{IN}} = 12\text{ V}$ ,  $\text{OUT} = \text{Open}$ ,  $V_{\text{EN/UVLO}} = 2\text{ V}$ ,  $V_{\text{OVLO}} = 0\text{ V}$  for TPS25970x/4x,  $\text{OVCSEL} = 390\text{ k}\Omega$  to GND for TPS25972x,  $R_{\text{ILM}} = 715\ \Omega$ ,  $dVdT = \text{Open}$ ,  $\text{ITIMER} = \text{Open}$ ,  $\overline{\text{FLT}} = \text{Open}$  for TPS25970x,  $\text{PGTH} = \text{Open}$  for TPS25972x/4x,  $\text{PG} = \text{Open}$  for TPS25972x/4x. All voltages referenced to GND.

Test Parameter	Description	MIN	TYP	MAX	UNITS
<b>INPUT SUPPLY (IN)</b>					
$I_{\text{Q(ON)}}$	IN supply quiescent current (TPS25970x)		413	650	$\mu\text{A}$
	IN supply quiescent current (TPS25972x)		407	650	$\mu\text{A}$
	IN supply quiescent current (TPS25974x)		413	650	$\mu\text{A}$
	IN supply quiescent current during OVC (TPS25972x)		429	650	$\mu\text{A}$
$I_{\text{Q(OFF)}}$	IN supply OFF state current ( $V_{\text{SD(F)}} < V_{\text{EN}} < V_{\text{UVLO(F)}}$ )		67	131	$\mu\text{A}$
$I_{\text{SD}}$	IN supply shutdown current ( $V_{\text{EN}} < V_{\text{SD(F)}}$ )		2.3	25	$\mu\text{A}$
$V_{\text{UVP(R)}}$	IN supply UVP rising threshold	2.44	2.54	2.64	V
$V_{\text{UVP(F)}}$	IN supply UVP falling threshold	2.35	2.45	2.55	V
<b>OUTPUT VOLTAGE CLAMP (OUT) - TPS25972x</b>					
$V_{\text{OVC}}$	Overvoltage Clamp threshold, OVCSEL = Shorted to GND	3.65	3.89	4.1	V
	Overvoltage Clamp threshold, OVCSEL = Open	5.25	5.76	6.2	V
	Overvoltage Clamp threshold, OVCSEL = 390 k $\Omega$ to GND	13.2	13.88	14.5	V
$V_{\text{CLAMP}}$	Output voltage during clamping, OVCSEL = Shorted to GND, $I_{\text{OUT}} = 10\text{ mA}$	3.2	3.82	4.2	V
	Output voltage during clamping, OVCSEL = Open, $I_{\text{OUT}} = 10\text{ mA}$	5	5.68	6.12	V
	Output voltage during clamping, OVCSEL = 390 k $\Omega$ to GND, $I_{\text{OUT}} = 10\text{ mA}$	13	13.79	14.6	V
<b>OUTPUT LOAD CURRENT MONITOR (ILM)</b>					
$G_{\text{IMON}}$	Analog load current monitor gain ( $I_{\text{MON}} : I_{\text{OUT}}$ ), $1\text{ A} \leq I_{\text{OUT}} \leq 7.7\text{ A}$ , $I_{\text{OUT}} < I_{\text{LIM}}$	98	105.5	114	$\mu\text{A/A}$
<b>OVERCURRENT PROTECTION (OUT)</b>					
$I_{\text{LIM}}$	Overcurrent threshold, $R_{\text{ILM}} = 6.65\text{ k}\Omega$	0.745	0.87	0.97	A
	Overcurrent threshold, $R_{\text{ILM}} = 3.32\text{ k}\Omega$	1.55	1.73	1.905	A
	Overcurrent threshold, $R_{\text{ILM}} = 1.65\text{ k}\Omega$	3.2	3.48	3.715	A
	Overcurrent threshold, $R_{\text{ILM}} = 750\ \Omega$	7.03	7.67	8.15	A
$I_{\text{SPFLT}}$	Circuit-Breaker threshold, ILM pin open (Single point failure)			0.1	A
$I_{\text{SPFLT}}$	Circuit-Breaker threshold, ILM pin shorted to GND (Single point failure)		2	3.1	A
$I_{\text{SCGain}}$	Scalable fast-trip threshold ( $I_{\text{SC}}$ ) : $I_{\text{LIM}}$ ratio	170	201	240	%
VFB	$V_{\text{OUT}}$ threshold to exit current limit foldback	1.55	1.88	2.23	V
<b>ON RESISTANCE (IN - OUT)</b>					
$R_{\text{ON}}$	$2.7 \leq V_{\text{IN}} \leq 4\text{ V}$ , $I_{\text{OUT}} = 3\text{ A}$ , $T_J = 25^{\circ}\text{C}$		10	18.3	m $\Omega$
	$4 < V_{\text{IN}} \leq 23\text{ V}$ , $I_{\text{OUT}} = 3\text{ A}$ , $T_J = 25^{\circ}\text{C}$		9.8	18.3	m $\Omega$
<b>ENABLE/UNDERVOLTAGE LOCKOUT (EN/UVLO)</b>					
$V_{\text{UVLO(R)}}$	EN/UVLO rising threshold	1.183	1.2	1.228	V
$V_{\text{UVLO(F)}}$	EN/UVLO falling threshold	1.076	1.1	1.12	V
$V_{\text{SD(F)}}$	EN/UVLO falling threshold for lowest shutdown current	0.45	0.75	0.95	V
$I_{\text{ENLKG}}$	EN/UVLO pin leakage current	-0.1		0.1	$\mu\text{A}$
<b>OVERVOLTAGE LOCKOUT (OVLO) - TPS25970x/4x</b>					
$V_{\text{OV(R)}}$	OVLO rising threshold	1.183	1.2	1.228	V
$V_{\text{OV(F)}}$	OVLO falling threshold	1.076	1.1	1.12	V

## 7.5 Electrical Characteristics (continued)

(Test conditions unless otherwise noted)  $-40^{\circ}\text{C} \leq T_J \leq 125^{\circ}\text{C}$ ,  $V_{IN} = 12\text{ V}$ ,  $\text{OUT} = \text{Open}$ ,  $V_{EN/UVLO} = 2\text{ V}$ ,  $V_{OVLO} = 0\text{ V}$  for TPS25970x/4x,  $\text{OVCSEL} = 390\text{ k}\Omega$  to GND for TPS25972x,  $R_{ILIM} = 715\ \Omega$ ,  $\text{dVdT} = \text{Open}$ ,  $\text{ITIMER} = \text{Open}$ ,  $\overline{\text{FLT}} = \text{Open}$  for TPS25970x,  $\text{PGTH} = \text{Open}$  for TPS25972x/4x,  $\text{PG} = \text{Open}$  for TPS25972x/4x. All voltages referenced to GND.

Test Parameter	Description	MIN	TYP	MAX	UNITS
$I_{OVLKG}$	OVLO pin leakage current ( $0.5\text{ V} < V_{OVLO} < 1.5\text{ V}$ )	-0.1		0.1	$\mu\text{A}$
<b>OVERCURRENT FAULT TIMER (ITIMER)</b>					
$I_{ITIMER}$	ITIMER pin internal discharge current, $I_{OUT} > I_{LIM}$	1.5	2	2.72	$\mu\text{A}$
$R_{ITIMER}$	ITIMER pin internal pullup resistance		13.8	35	$\text{k}\Omega$
$V_{INT}$	ITIMER pin internal pullup voltage	2.1	2.57	2.74	V
$V_{ITIMER(F)}$	ITIMER comparator threshold, $I_{OUT} > I_{LIM}$	0.609	1.05	1.37	V
$\Delta V_{ITIMER}$	ITIMER discharge differential voltage threshold, $I_{OUT} > I_{LIM}$	1.286	1.52	1.741	V
<b>POWER GOOD INDICATION (PG) - TPS25972x/4x</b>					
$V_{PGD}$	PG pin voltage while de-asserted. $V_{IN} < V_{UVP(F)}$ , $V_{EN} < V_{SD(F)}$ , Weak pull-up ( $I_{PG} = 26\ \mu\text{A}$ )		663	1000	mV
	PG pin voltage while de-asserted. $V_{IN} < V_{UVP(F)}$ , $V_{EN} < V_{SD(F)}$ , Strong pull-up ( $I_{PG} = 242\ \mu\text{A}$ )		782	1000	mV
	PG pin voltage while de-asserted, $V_{IN} > V_{UVP(R)}$		0	600	mV
$I_{PGLKG}$	PG pin leakage current, PG asserted			3	$\mu\text{A}$
<b>POWERGOOD THRESHOLD (PGTH)</b>					
$V_{PGTH(R)}$	PGTH rising threshold	1.178	1.2	1.23	V
$V_{PGTH(F)}$	PGTH falling threshold	1.071	1.1	1.13	V
$I_{PGTHLKG}$	PGTH pin leakage current	-1		1	$\mu\text{A}$
<b>FAULT INDICATION (FLT) - TPS25970x</b>					
$I_{FLT LKG}$	$\overline{\text{FLT}}$ pin leakage current	-1		1	$\mu\text{A}$
$R_{FLT B}$	$\overline{\text{FLT}}$ pin internal pull-down resistance		12.4		$\Omega$
<b>OVERTEMPERATURE PROTECTION (OTP)</b>					
TSD	Thermal Shutdown rising threshold, $T_J \uparrow$		154		$^{\circ}\text{C}$
TSD <sub>HYS</sub>	Thermal Shutdown hysteresis, $T_J \downarrow$		10		$^{\circ}\text{C}$
<b>DVDT</b>					
$I_{dVdt}$	dVdt pin internal charging current	1.4	3.4	5.7	$\mu\text{A}$

## 7.6 Timing Requirements

PARAMETER		TEST CONDITIONS			MIN	TYP	MAX	UNIT
$t_{OVLO}$	Overvoltage lockout response time	TPS25970x and TPS25974x, $V_{OVLO} > V_{OV(R)}$ to $V_{OUT \downarrow}$				1.2		$\mu\text{s}$
$t_{OVC}$	Overvoltage clamp response time	TPS25972x, $V_{IN} > V_{OVC}$ to $V_{OUT \downarrow}$				5		$\mu\text{s}$
$t_{CB}$	Circuit-Breaker response time	TPS25974x, $I_{OUT} > I_{LIM} + 30\%$ to $V_{OUT \downarrow}$				2		$\mu\text{s}$
$t_{LIM}$	Current limit response time	TPS25970x and TPS25972x, $I_{OUT} > I_{LIM} + 30\%$ to $I_{OUT}$ settling to within 5% of $I_{LIM}$				465		$\mu\text{s}$
$t_{SC}$	Short-circuit response time	$I_{OUT} > 3 \times I_{LIM}$ to output current cut off				550		ns
$t_{FT}$	Fixed fast-trip response time	$I_{OUT} > I_{FT}$ to $I_{OUT \downarrow}$				550		ns
$t_{TSD, RST}$	Thermal Shutdown auto-retry Interval	Device enabled and $T_J < \text{TSD} - \text{TSD}_{HYS}$				110		ms
$t_{PGA}$	PG assertion de-glitch time	$V_{PGTH} > V_{PGTH(R)}$ to $\text{PG} \uparrow$				14		$\mu\text{s}$
$t_{PGD}$	PG de-assertion de-glitch time	$V_{PGTH} < V_{PGTH(F)}$ to $\text{PG} \downarrow$				14		$\mu\text{s}$

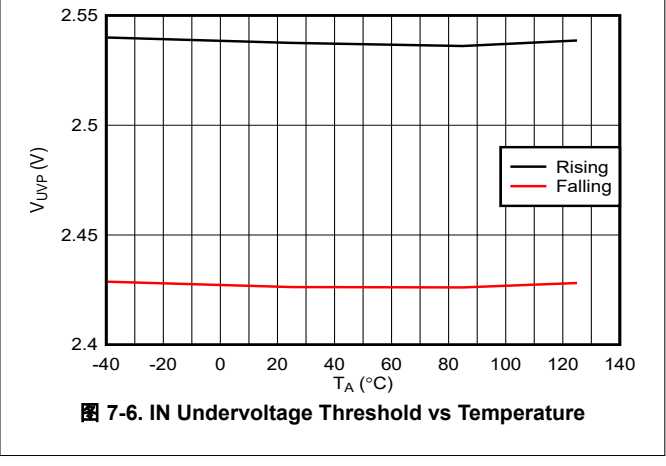
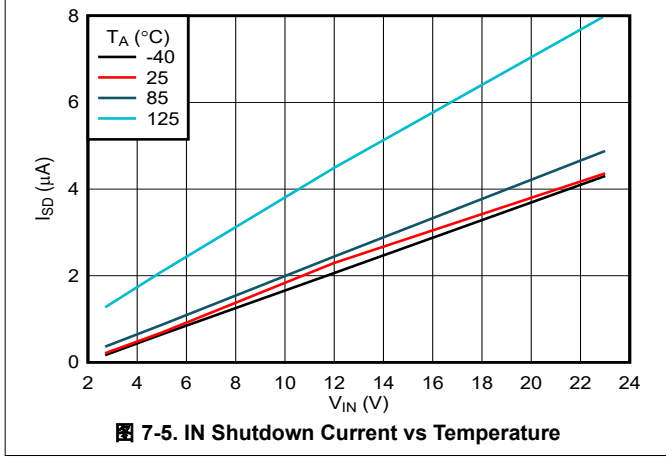
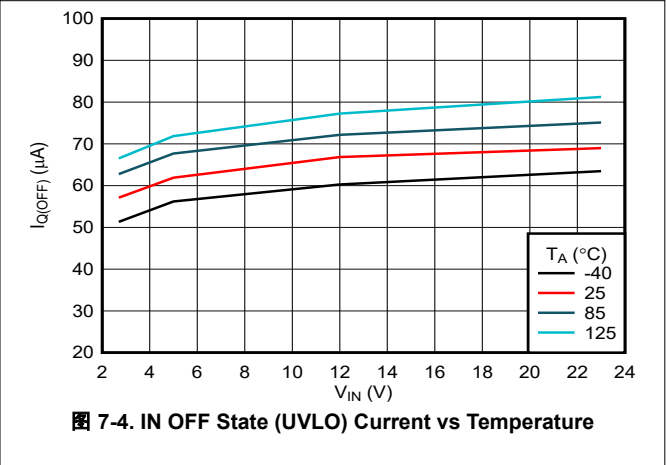
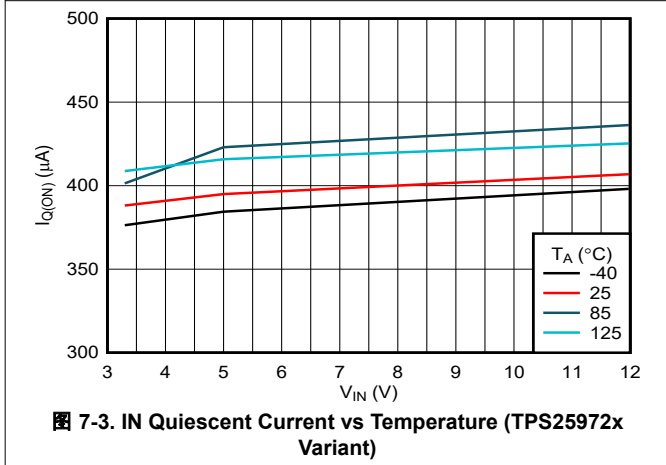
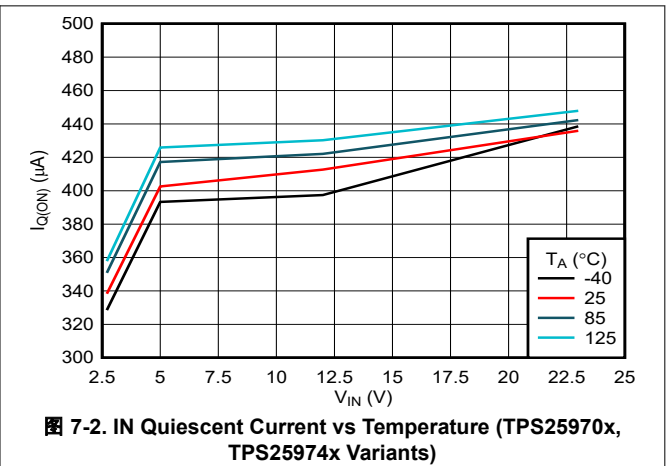
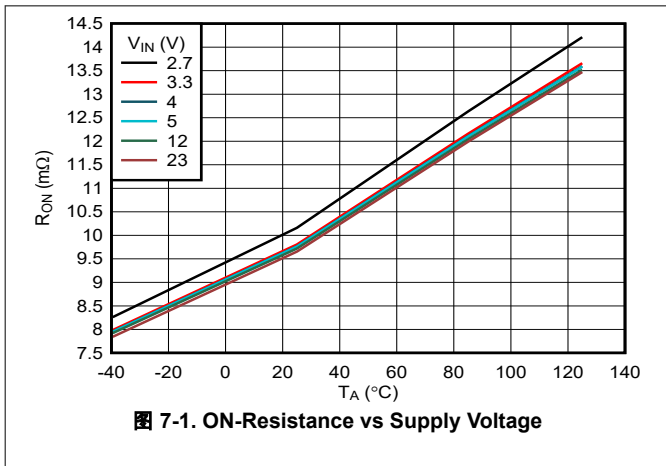


## 7.7 Switching Characteristics

The output rising slew rate is internally controlled and constant across the entire operating voltage range to ensure the turn on timing is not affected by the load conditions. The rising slew rate can be adjusted by adding capacitance from the dVdt pin to ground. As  $C_{dVdt}$  is increased it will slow the rising slew rate (SR). See Slew Rate and Inrush Current Control (dVdt) section for more details. The Turn-Off Delay and Fall Time, however, are dependent on the RC time constant of the load capacitance ( $C_{OUT}$ ) and Load Resistance ( $R_L$ ). The Switching Characteristics are only valid for the power-up sequence where the supply is available in steady state condition and the load voltage is completely discharged before the device is enabled. Typical values are taken at  $T_J = 25^\circ\text{C}$  unless specifically noted otherwise.  $R_L = 100\ \Omega$ ,  $C_{OUT} = 1\ \mu\text{F}$ .

PARAMETER		$V_{IN}$	$C_{dVdt} = \text{Open}$	$C_{dVdt} = 1800\ \text{pF}$	$C_{dVdt} = 3300\ \text{pF}$	UNITS
$SR_{ON}$	Output rising slew rate	2.7 V	8.922	1.218	0.72	V/ms
		12 V	21.45	1.562	0.901	
		23 V	34.16	1.761	1.003	
$t_{D,ON}$	Turn-on delay	2.7 V	0.138	0.505	0.79	ms
		12 V	0.145	0.979	1.659	
		23 V	0.15	1.478	2.562	
$t_R$	Rise time	2.7 V	0.242	1.771	2.993	ms
		12 V	0.446	6.131	10.63	
		23 V	0.538	10.43	18.31	
$t_{ON}$	Turn-on time	2.7 V	0.379	2.277	3.783	ms
		12 V	0.582	7.11	12.29	
		23 V	0.668	11.91	20.87	
$t_{D,OFF}$	Turn-off delay	2.7 V	22.1	22.1	22.1	$\mu\text{s}$
		12 V	18.9	18.9	18.9	
		23 V	16.5	16.5	16.5	

### 7.8 Typical Characteristics



### 7.8 Typical Characteristics (continued)

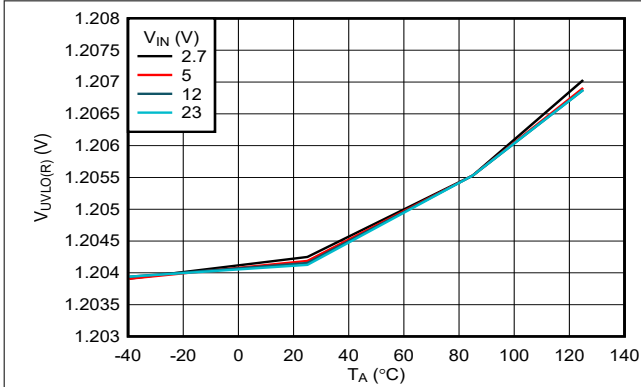


图 7-7. EN/UVLO Rising Threshold vs Temperature

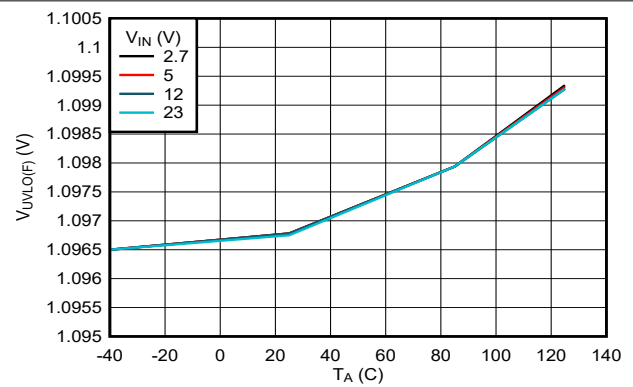


图 7-8. EN/UVLO Falling Threshold vs Temperature

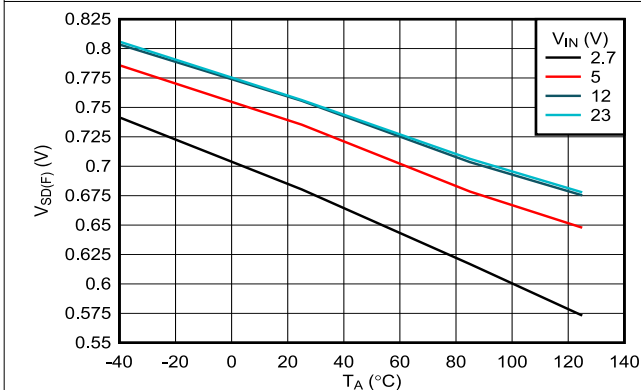


图 7-9. EN/UVLO Shutdown Falling Threshold vs Temperature

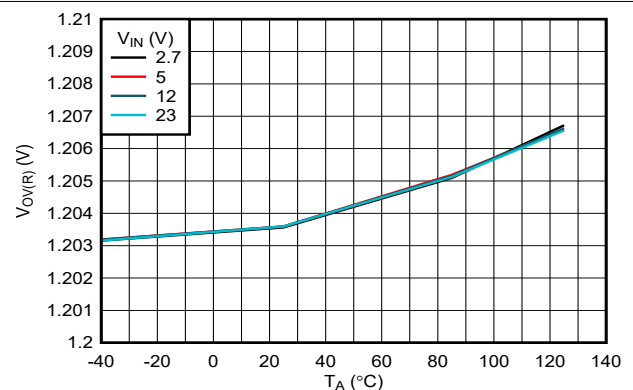


图 7-10. OVLO Rising Threshold vs Temperature (TPS25970x, TPS25974x Variants)

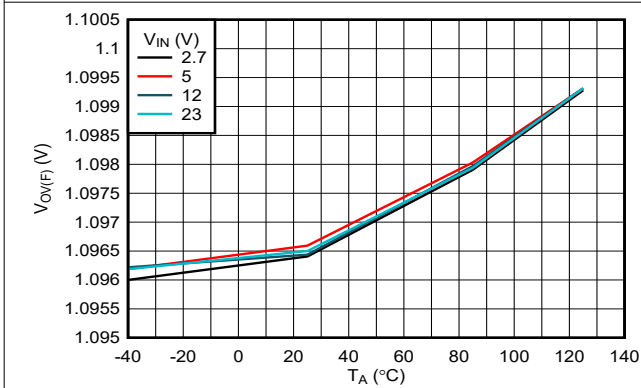


图 7-11. OVLO Falling Threshold vs Temperature (TPS25970x, TPS25974x Variants)

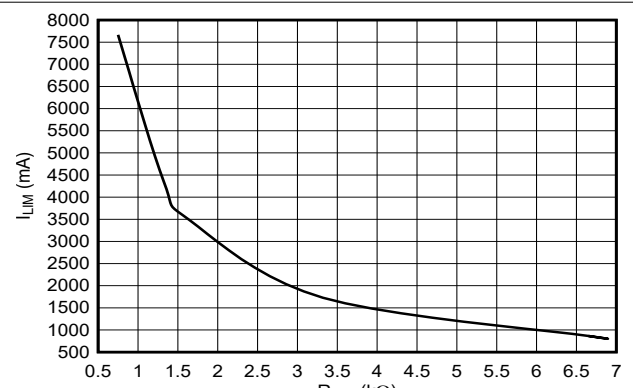
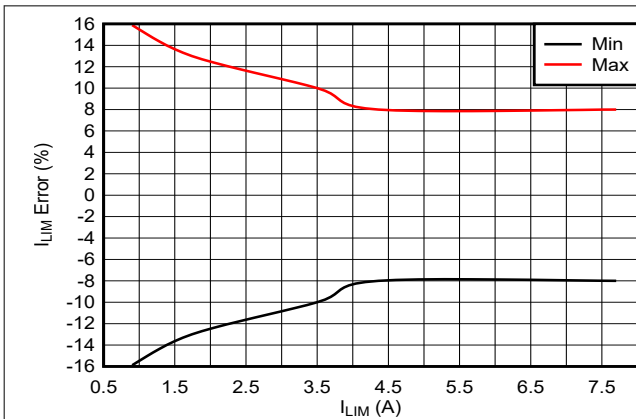
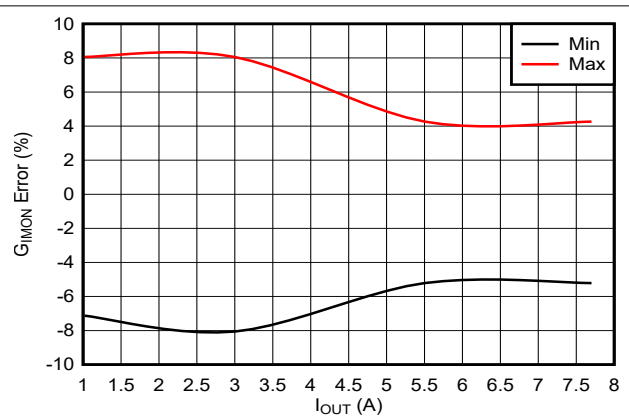


图 7-12. Overcurrent Threshold vs ILM Resistor

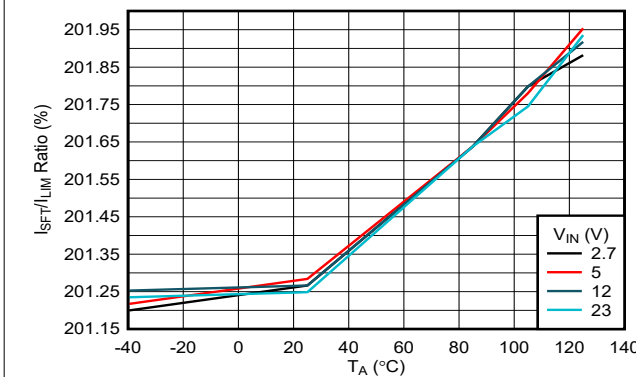
### 7.8 Typical Characteristics (continued)



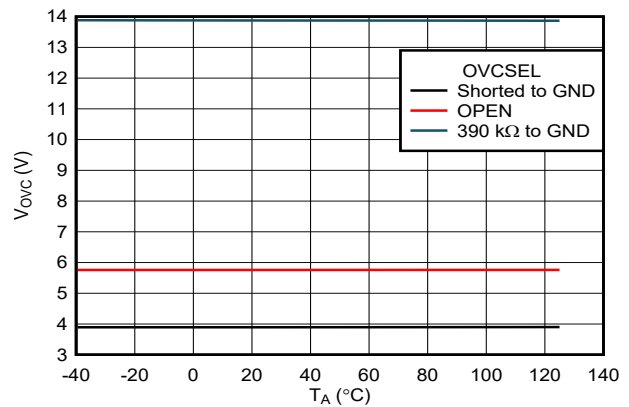
**图 7-13. Overcurrent Threshold Accuracy (Across Process, Voltage and Temperature)**



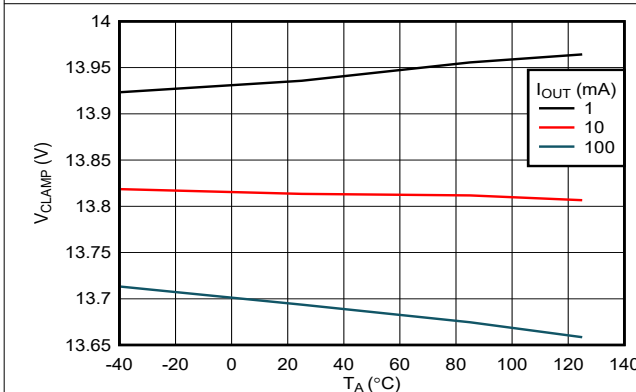
**图 7-14. Analog Current Monitor Gain Accuracy**



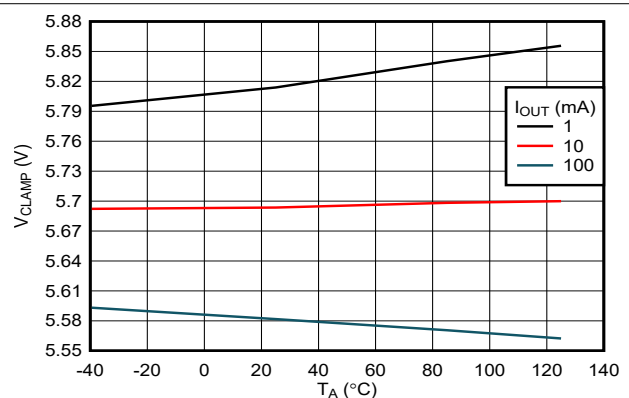
**图 7-15. Scalable Fast-Trip Threshold: Current Limit Threshold ( $I_{LIM}$ ) Ratio vs Temperature**



**图 7-16. OVC Threshold vs Temperature (TPS25972x Variant)**



**图 7-17. OVC Clamping Voltage (OVCSEL = 390 kΩ to GND) vs Load Current (TPS25972x Variant)**



**图 7-18. OVC Clamping Voltage (OVCSEL = OPEN) vs Load Current (TPS25972x Variant)**

### 7.8 Typical Characteristics (continued)

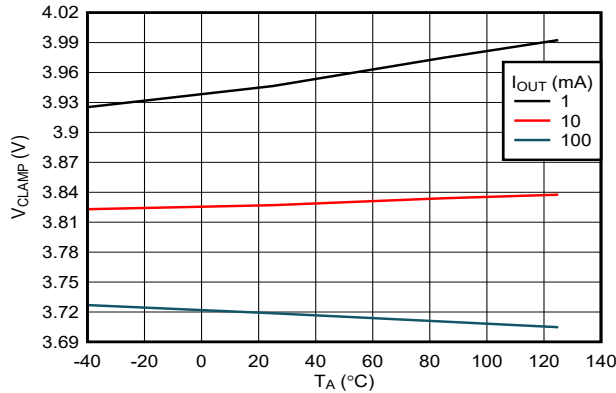


图 7-19. OVC Clamping Voltage (OVCSEL = GND) vs Load Current (TPS2597x Variant)

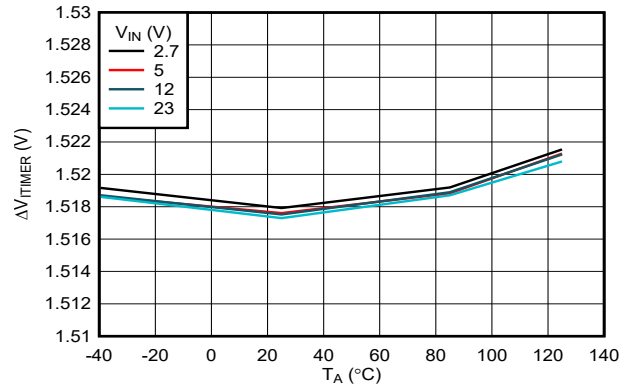


图 7-20. ITIMER Discharge Differential Voltage Threshold vs Temperature

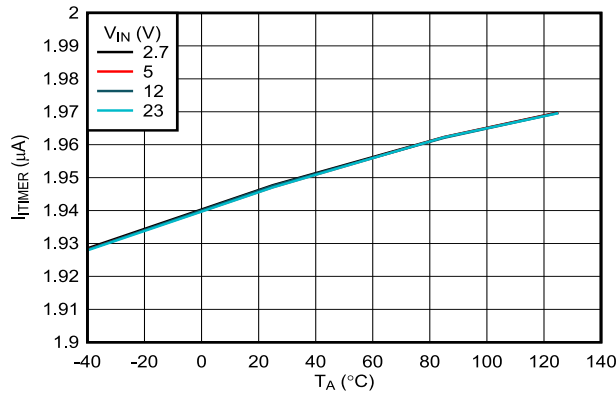


图 7-21. ITIMER Discharge Current vs Temperature

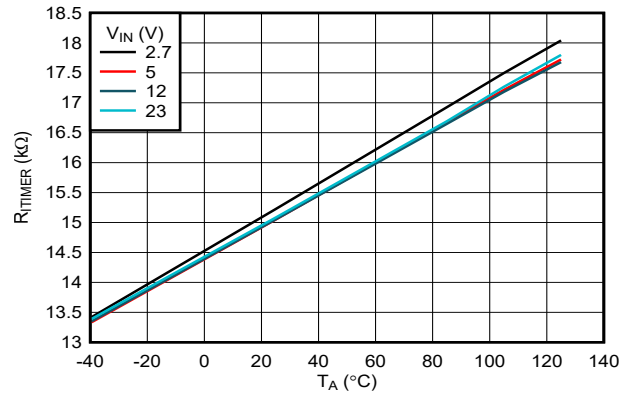


图 7-22. ITIMER Internal Pullup Resistance vs Temperature

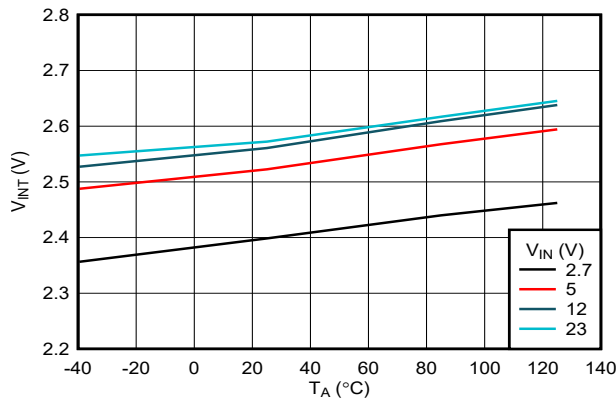


图 7-23. ITIMER internal Pullup Voltage vs Temperature

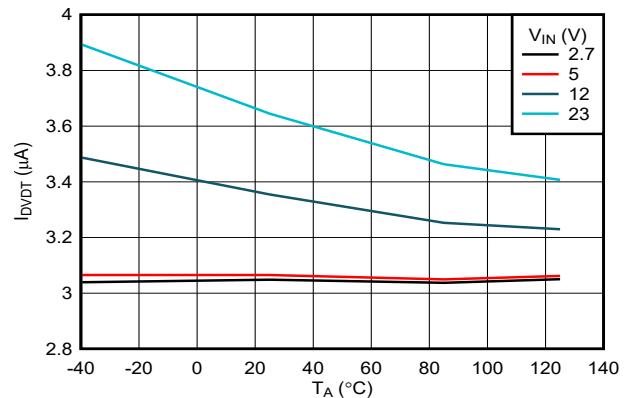


图 7-24. DVDT Charging Current vs Temperature

### 7.8 Typical Characteristics (continued)

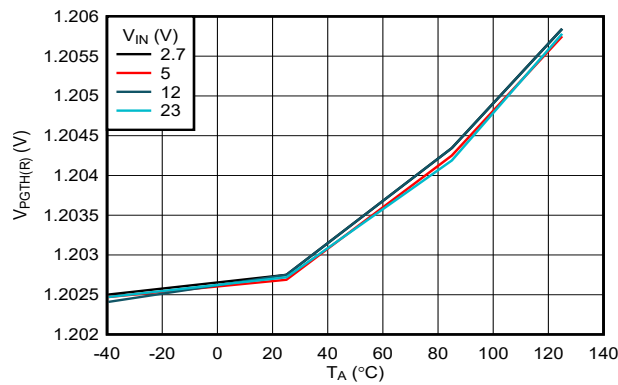


Fig 7-25. PGTH Threshold (Rising) vs Temperature (TPS25972x, TPS25974x Variants)

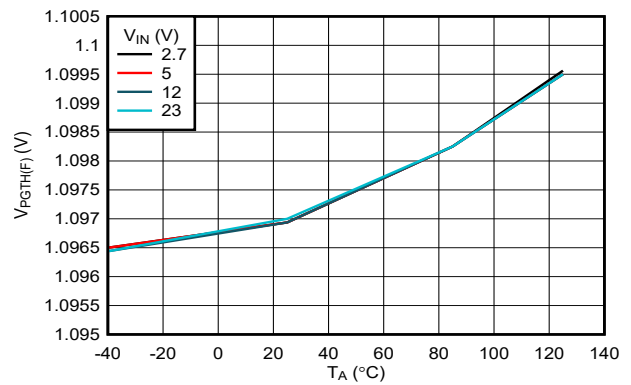


Fig 7-26. PGTH Threshold (Falling) vs Temperature (TPS25972x, TPS25974x Variants)

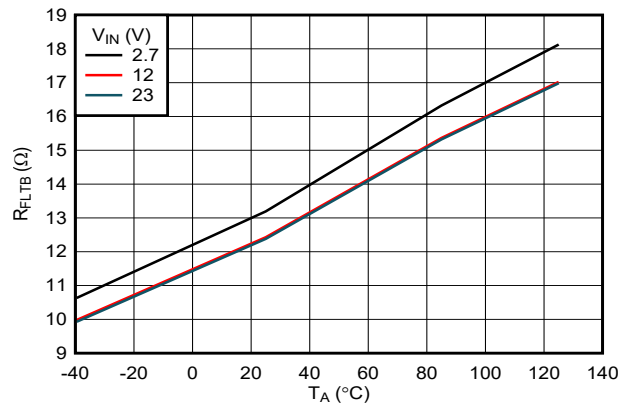


Fig 7-27. FLT Pin Pulldown Resistance vs Temperature

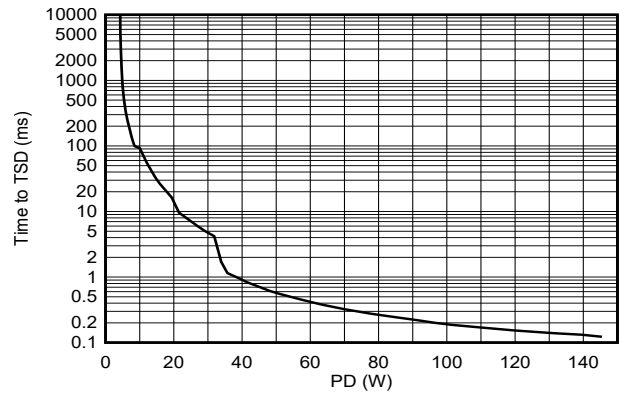


Fig 7-28. Time to Thermal Shut-Down During Inrush State

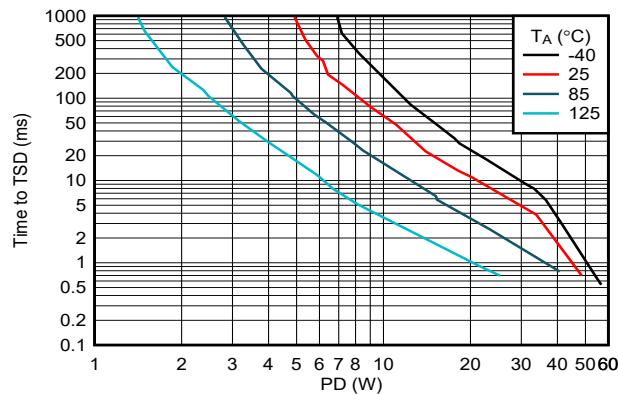


Fig 7-29. Time to Thermal Shut-Down During Steady State

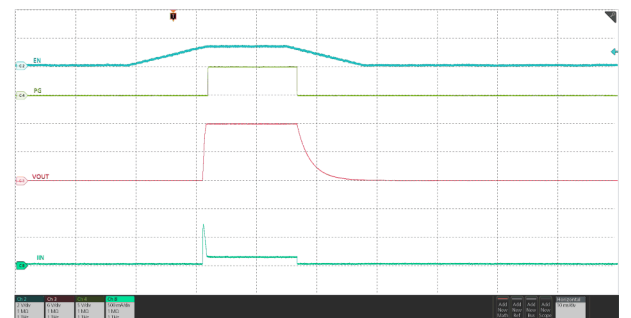
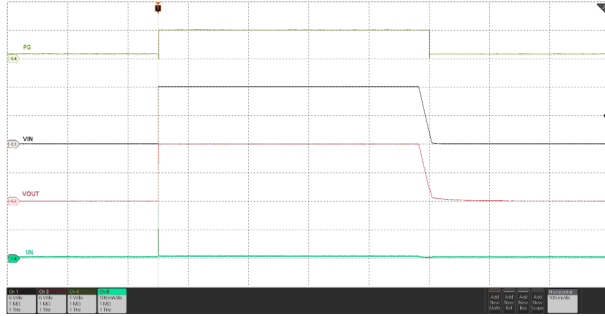


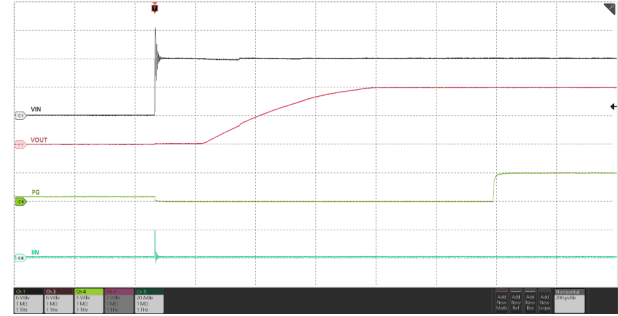
Fig 7-30. Power Up and Down With EN/UVLO Control  
 $V_{IN} = 12\text{ V}$ ,  $C_{OUT} = 22\ \mu\text{F}$ ,  $C_{dVdt} = \text{Open}$ ,  $V_{EN/UVLO}$  ramped from  $0\text{ V} \rightarrow 1.4\text{ V} \rightarrow 0\text{ V}$

## 7.8 Typical Characteristics (continued)



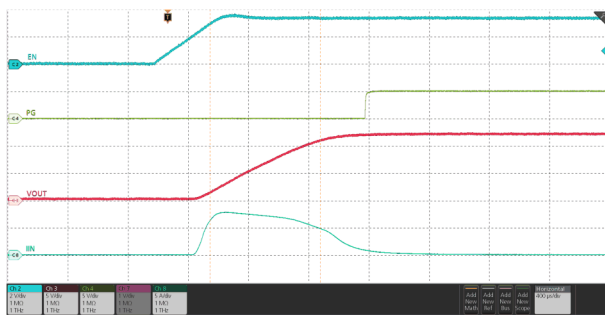
$V_{EN/UVLO} = 2\text{ V}$ ,  $C_{OUT} = 22\ \mu\text{F}$ ,  $C_{dVdt} = \text{Open}$ ,  $V_{IN}$  ramped from  $0\text{ V} \rightarrow 12\text{ V} \rightarrow 0\text{ V}$

**图 7-31. Power Up and Down With Input Supply**



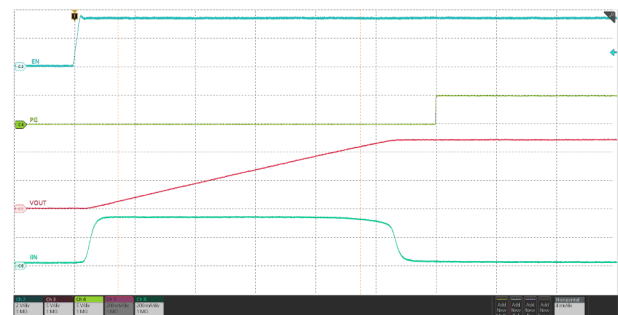
$C_{OUT} = 22\ \mu\text{F}$ ,  $C_{dVdt} = \text{Open}$ , EN/UVLO connected to IN through resistor ladder, 12 V hot-plugged to IN

**图 7-32. Input Hot-Plug**



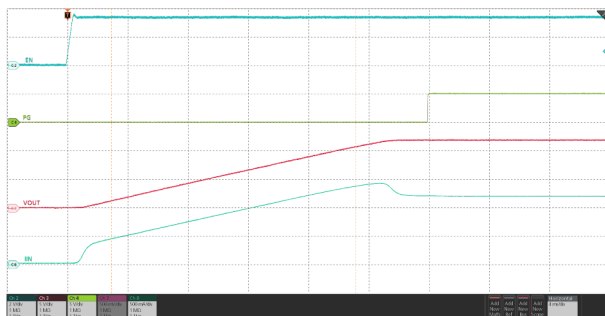
$V_{IN} = 12\text{ V}$ ,  $C_{OUT} = 470\ \mu\text{F}$ ,  $C_{dVdt} = \text{Open}$ ,  $V_{EN/UVLO}$  stepped up to 3.3 V

**图 7-33. Inrush Current Without Slew Rate Control – Capacitive Load**



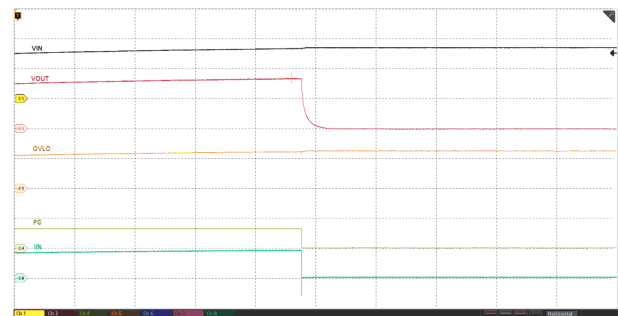
$V_{IN} = 12\text{ V}$ ,  $C_{OUT} = 470\ \mu\text{F}$ ,  $C_{dVdt} = 5100\ \text{pF}$ ,  $V_{EN/UVLO}$  stepped up to 3.3 V

**图 7-34. Inrush Current With Slew Rate Control – Capacitive Load**



$V_{IN} = 12\text{ V}$ ,  $C_{OUT} = 470\ \mu\text{F}$ ,  $R_{OUT} = 10\ \Omega$ ,  $C_{dVdt} = 5100\ \text{pF}$ ,  $V_{EN/UVLO}$  stepped up to 3.3 V

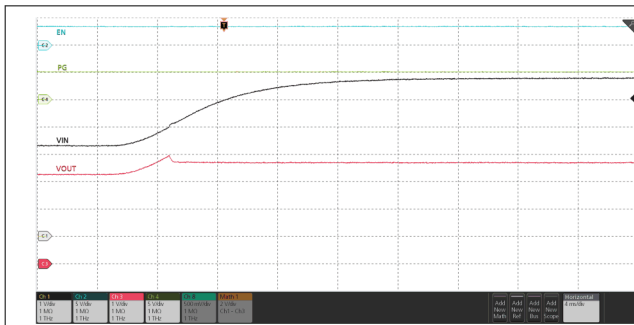
**图 7-35. Inrush Current With Slew Rate Control – Resistive and Capacitive Load**



OV threshold set to 16.7 V,  $V_{IN}$  ramped up from 12 V to 17 V

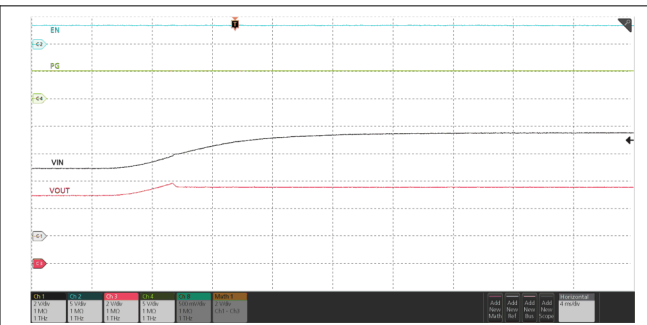
**图 7-36. Overvoltage Lockout Response – TPS25970x and TPS25974x**

## 7.8 Typical Characteristics (continued)



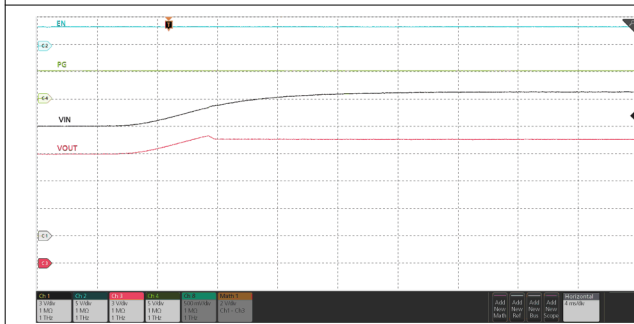
$R_{OVCSSEL} = GND$ ,  $C_{OUT} = 220 \mu F$ ,  $I_{OUT} = 200 \text{ mA}$ ,  $V_{IN}$  ramped up from 3.3 V to 5.8 V

图 7-37. Overvoltage Clamp Response – TPS25972x



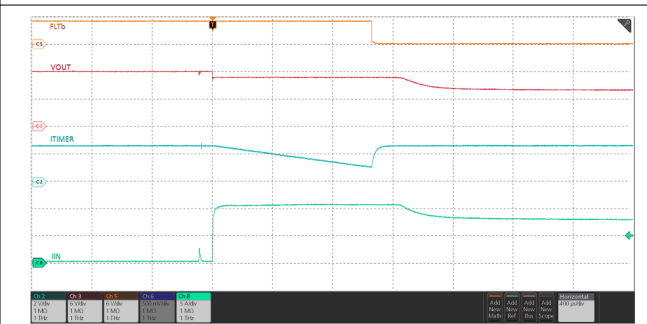
$R_{OVCSSEL} = \text{Open}$ ,  $C_{OUT} = 220 \mu F$ ,  $I_{OUT} = 200 \text{ mA}$ ,  $V_{IN}$  ramped up from 5 V to 7.5 V

图 7-38. Overvoltage Clamp Response – TPS25972x



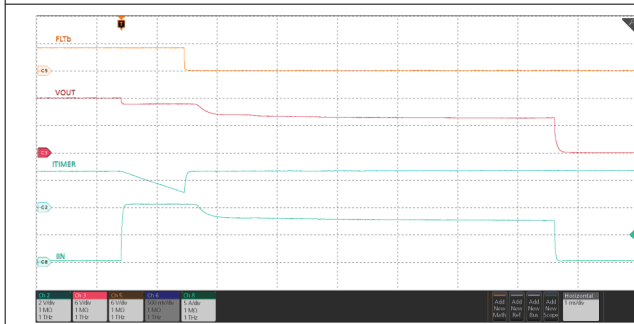
$R_{OVCSSEL} = 390 \text{ k}\Omega$ ,  $C_{OUT} = 220 \mu F$ ,  $I_{OUT} = 200 \text{ mA}$ ,  $V_{IN}$  ramped up from 12 V to 16.5 V

图 7-39. Overvoltage Clamp Response – TPS25972x



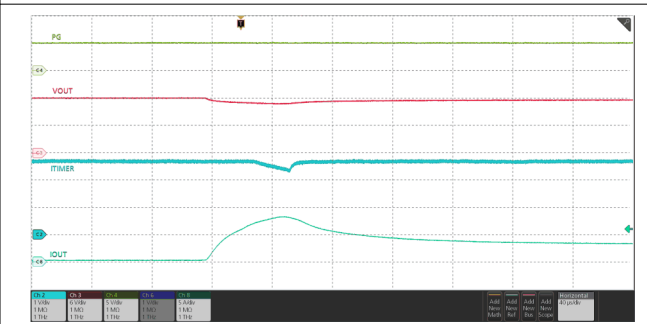
$V_{IN} = 12 \text{ V}$ ,  $C_{ITIMER} = 1.3 \text{ nF}$ ,  $C_{OUT} = 220 \mu F$ ,  $R_{ILM} = 715 \Omega$ ,  $I_{OUT}$  stepped from 0 A → 11 A

图 7-40. Active Current Limit Response – TPS25970x



$V_{IN} = 12 \text{ V}$ ,  $C_{ITIMER} = 1.3 \text{ nF}$ ,  $C_{OUT} = 220 \mu F$ ,  $R_{ILM} = 715 \Omega$ ,  $I_{OUT}$  stepped from 0 A → 11 A

图 7-41. Active Current Limit Response Followed by TSD – TPS25970x

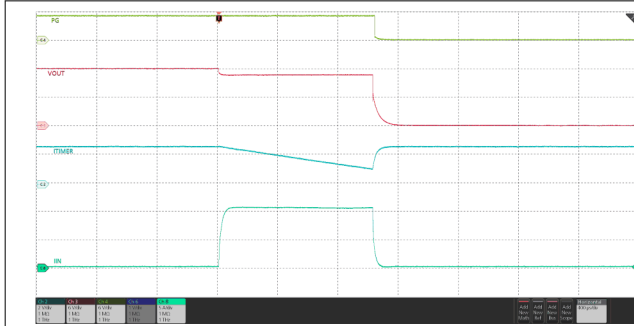


$V_{IN} = 12 \text{ V}$ ,  $C_{ITIMER} = 120 \text{ pF}$ ,  $C_{OUT} = 470 \mu F$ ,  $R_{ILM} = 715 \Omega$ ,  $I_{OUT}$  ramped from 0 A → 8 A → 4 A within 100  $\mu\text{s}$

图 7-42. Transient Overcurrent Blanking Timer Response

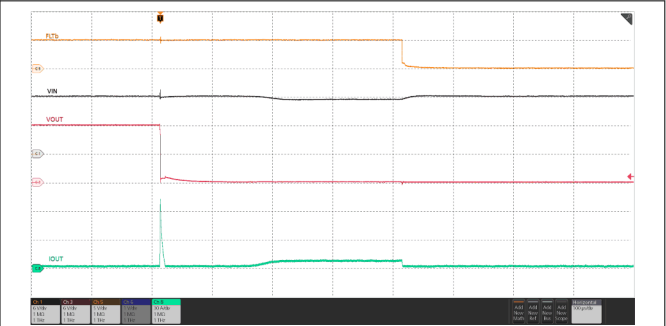


## 7.8 Typical Characteristics (continued)



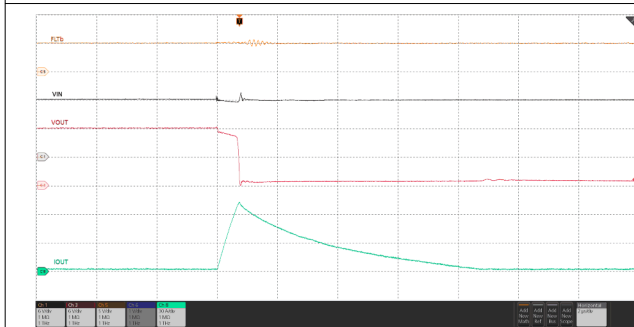
$V_{IN} = 12\text{ V}$ ,  $C_{ITIMER} = 1.3\text{ nF}$ ,  $C_{OUT} = 470\text{ }\mu\text{F}$ ,  $R_{ILM} = 715\text{ }\Omega$ ,  
 $I_{OUT}$  stepped from  $0\text{ A} \rightarrow 11\text{ A}$

**图 7-43. Circuit-Breaker Response TPS25974x**



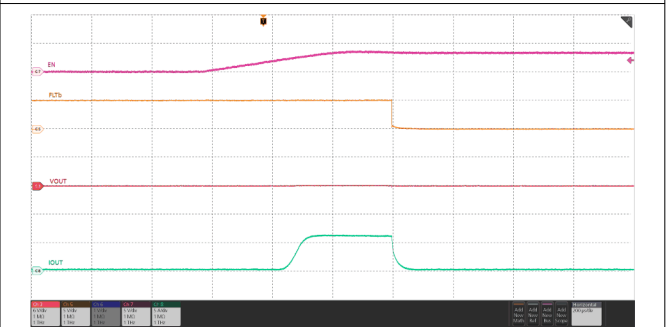
$V_{IN} = 12\text{ V}$ ,  $R_{ILM} = 715\text{ }\Omega$ ,  $I_{OUT}$  stepped from Open  $\rightarrow$  Short-circuit to GND

**图 7-44. Output Short-Circuit During Steady State**



$V_{IN} = 12\text{ V}$ ,  $R_{ILM} = 715\text{ }\Omega$ ,  $I_{OUT}$  stepped from Open  $\rightarrow$  Short-circuit to GND

**图 7-45. Output Short-Circuit During Steady State (Zoomed In)**



$V_{IN} = 12\text{ V}$ ,  $C_{OUT} = \text{Open}$ ,  $I_{OUT}$  short-circuit to GND,  $R_{ILM} = 715\text{ }\Omega$ ,  $V_{EN/UVLO}$  stepped from  $0\text{ V} \rightarrow 3.3\text{ V}$

**图 7-46. Power Up into Short-Circuit**

## 8 Detailed Description

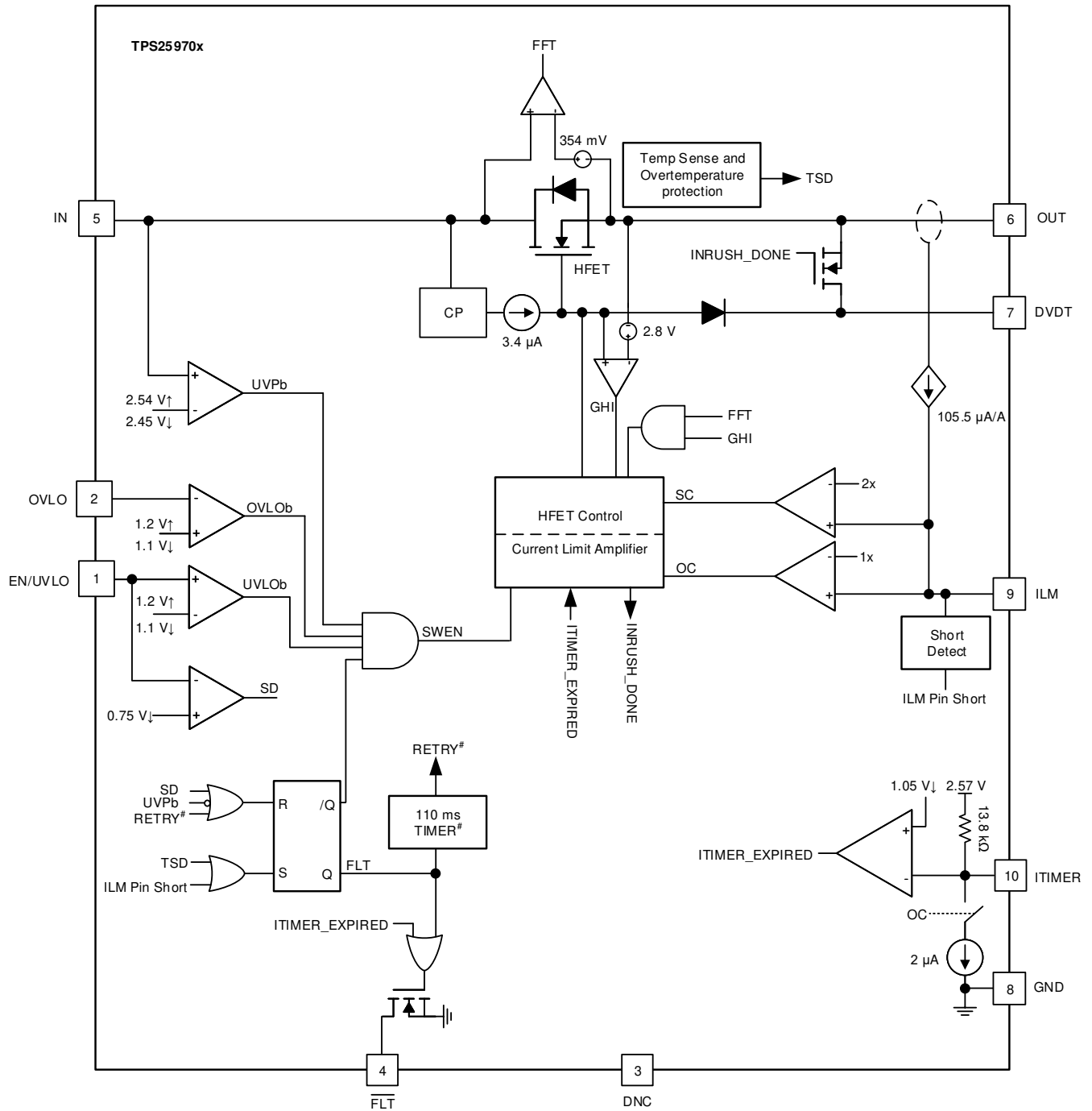
### 8.1 Overview

The TPS2597xx is an eFuse with an integrated power path that is used to ensure safe power delivery in a system. The device starts its operation by monitoring the IN bus. When the input supply voltage ( $V_{IN}$ ) exceeds the undervoltage protection threshold ( $V_{UVP}$ ), the device samples the EN/UVLO pin. A high level ( $> V_{UVLO}$ ) on this pin enables the internal power path (HFET) to start conducting and allow current to flow from IN to OUT. When EN/UVLO is held low ( $< V_{UVLO}$ ), the internal power path is turned off.

After a successful start-up sequence, the device now actively monitors its load current and input voltage, and controls the internal HFET to ensure that the user adjustable overcurrent limit threshold ( $I_{LIM}$ ) is not exceeded and overvoltage spikes are either safely clamped to the selected threshold voltage ( $V_{OVC}$ ) or cut-off after they cross the user-adjustable overvoltage lockout threshold ( $V_{OVLO}$ ). The device also provides fast protection against severe overcurrent during short-circuit events. This feature keeps the system safe from harmful levels of voltage and current. At the same time, a user-adjustable overcurrent blanking timer allows the system to pass moderate transient peaks in the load current profile without tripping the eFuse. This action ensures a robust protection solution against real faults which is also immune to transients, thereby ensuring maximum system uptime.

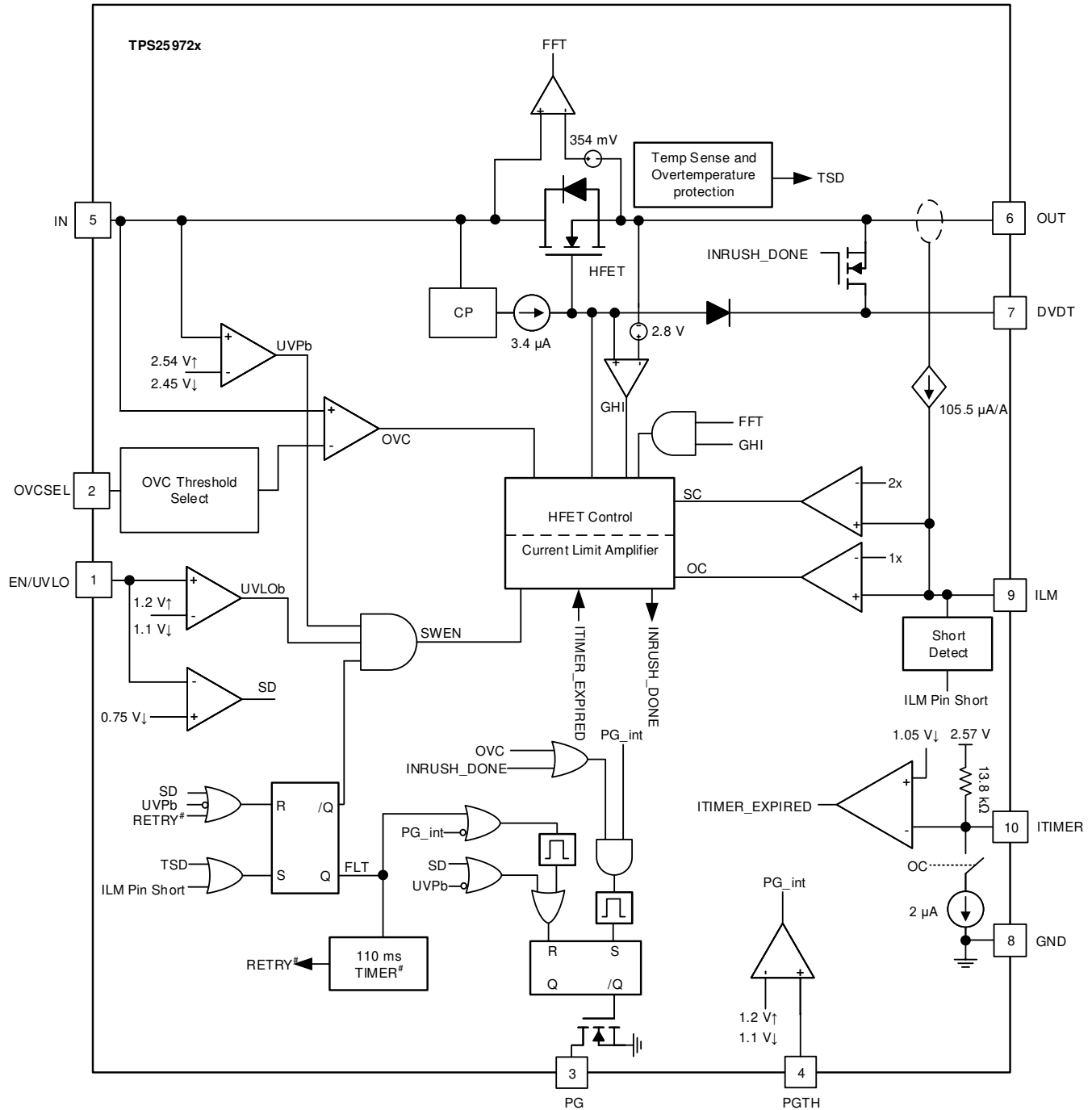
The device also has a built-in thermal sensor based shutdown mechanism to protect itself in case the device temperature ( $T_J$ ) exceeds the recommended operating conditions.

## 8.2 Functional Block Diagram



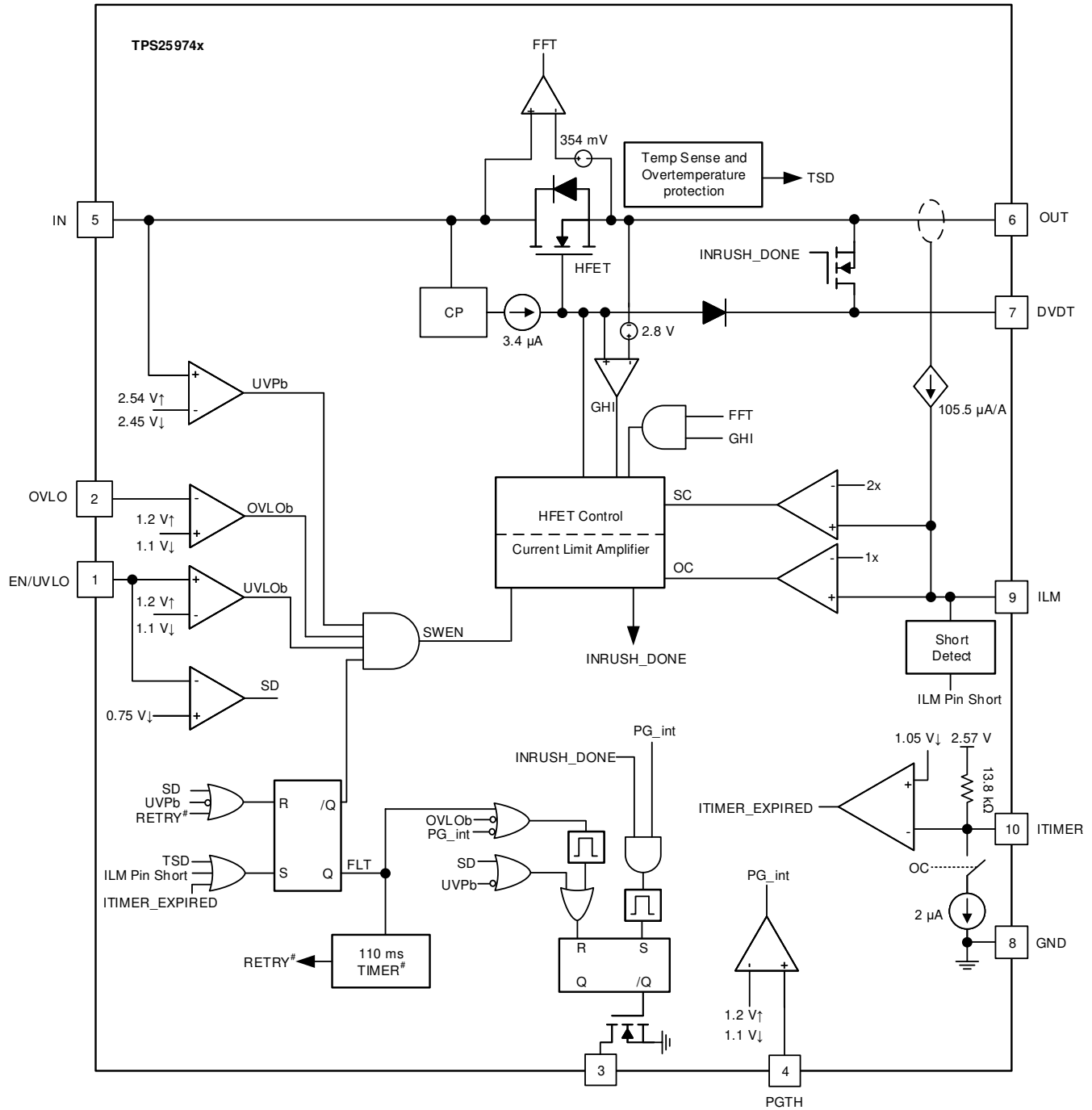
# Not applicable to Latch-off variants (TPS25970L)

图 8-1. TPS25970x Block Diagram



# Not applicable to Latch-off variants (TPS25972L)

**图 8-2. TPS25972x Block Diagram**



# Not applicable to Latch-off variants (TPS25974L)

图 8-3. TPS25974x Block Diagram

## 8.3 Feature Description

The TPS2597xx eFuse is a compact, feature-rich power management device that provides detection, protection, and indication in the event of system faults.

### 8.3.1 Undervoltage Lockout (UVLO and UVP)

The TPS2597xx implements undervoltage protection on IN in case the applied voltage becomes too low for the system or device to properly operate. The undervoltage protection has a default lockout threshold of  $V_{UVLP}$  which is fixed internally. Also, the UVLO comparator on the EN/UVLO pin allows the undervoltage protection threshold to be externally adjusted to a user-defined value. 图 8-4 和 方程式 1 show how a resistor divider can be used to set the UVLO set point for a given voltage supply.

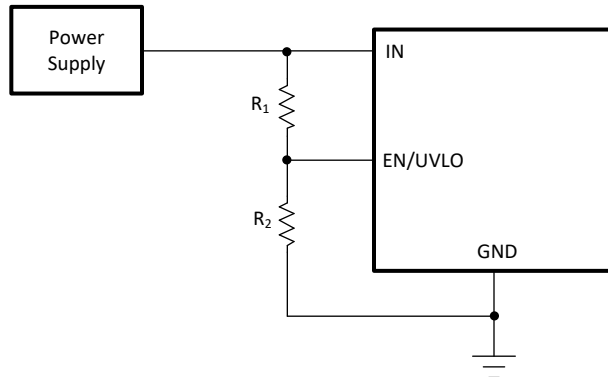


图 8-4. Adjustable Undervoltage Protection

$$V_{IN(UV)} = \frac{V_{UVLO} \times (R_1 + R_2)}{R_2} \quad (1)$$

### 8.3.2 Overvoltage Lockout (OVLO)

The TPS25970x and TPS25974x variants allow the user to implement overvoltage lockout to protect the load from input overvoltage conditions. The OVLO comparator on the OVLO pin allows the overvoltage protection threshold to be adjusted to a user-defined value. After the voltage at the OVLO pin crosses the OVLO rising threshold,  $V_{OV(R)}$ , the device turns off the power to the output. Thereafter, the devices wait for the voltage at the OVLO pin to fall below the OVLO falling threshold,  $V_{OV(F)}$  before the output power is turned ON again. The rising and falling thresholds are slightly different to provide hysteresis. 图 8-5 和 方程式 2 show how a resistor divider can be used to set the OVLO set point for a given voltage supply.

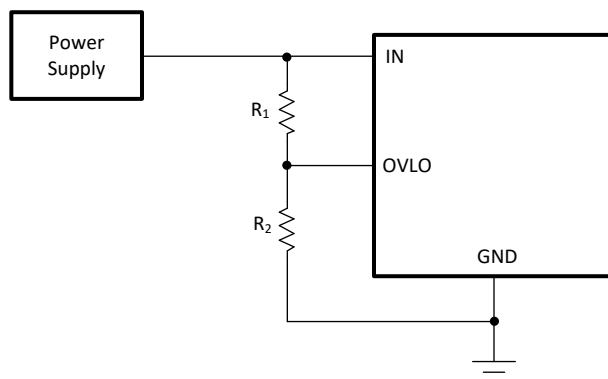


图 8-5. Adjustable Overvoltage Protection

$$V_{IN(OV)} = \frac{V_{OV} \times (R_1 + R_2)}{R_2} \quad (2)$$

While recovering from a OVLO event, the TPS25970x variants start up with inrush control (dVdt).

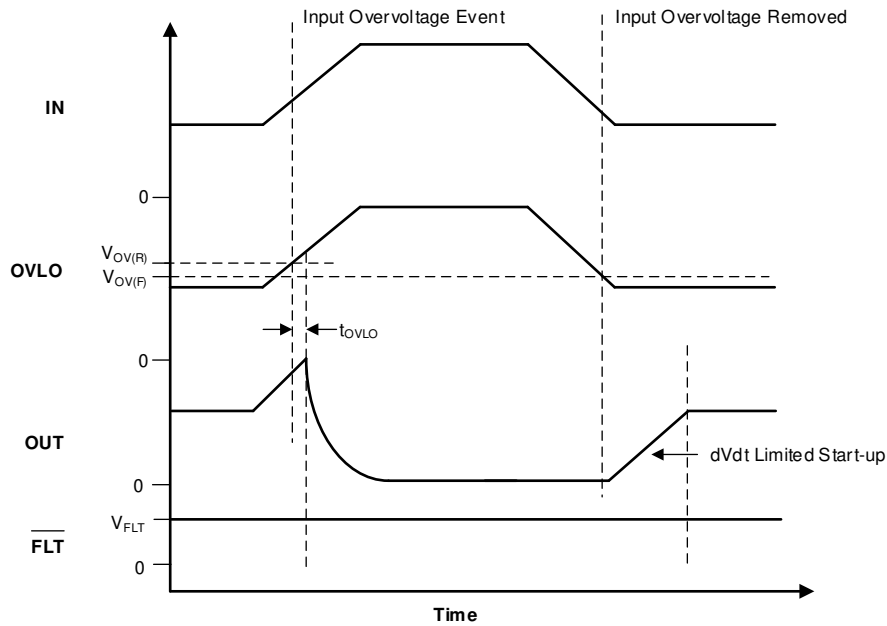


图 8-6. TPS25970x Overvoltage Lockout and Recovery

While recovering from an OVLO event, the TPS25974x variants start up with inrush control (dVdt).

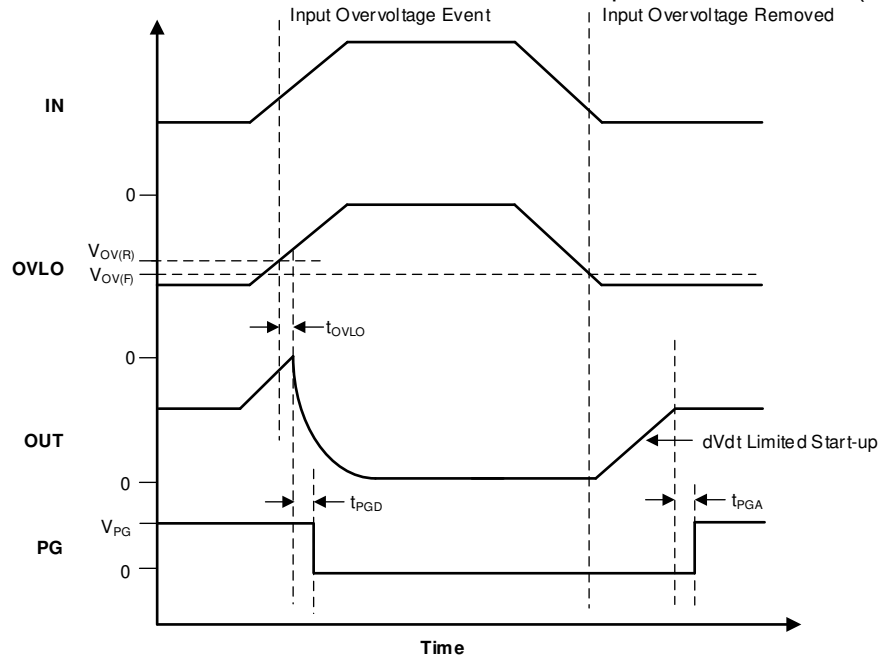


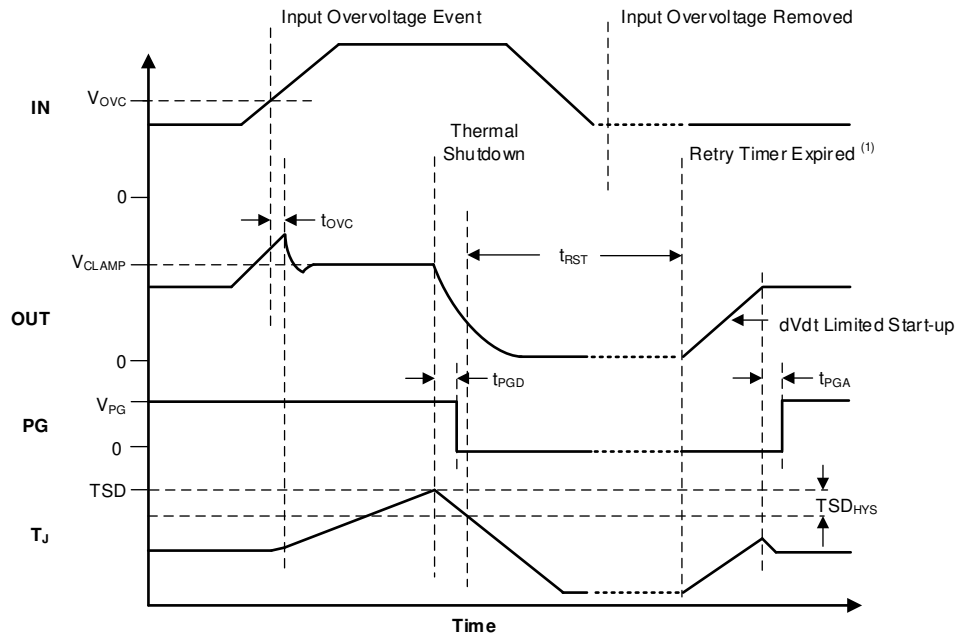
图 8-7. TPS25974x Overvoltage Lockout and Recovery

### 8.3.3 Overvoltage Clamp (OVC)

The TPS25972x variants implement a voltage clamp on the output to protect the system in the event of input overvoltage. When the device detects the input has exceeded the overvoltage clamp threshold ( $V_{OVC}$ ), it quickly responds within  $t_{OVC}$  and stops the output from rising further. The device then regulates the HFET linearly to clamp the output voltage below  $V_{CLAMP}$  as long as an overvoltage condition is present on the input.

If the part stays in clamping state for an extended period of time, there is higher power dissipation inside the part which can eventually lead to thermal shutdown (TSD). After the part shuts down due to TSD fault, it either

stays latched off (TPS25972L variant) or restart automatically after a fixed delay (TPS25972A variant). See [Overtemperature Protection \(OTP\)](#) for more details on device response to overtemperature.



<sup>(1)</sup> Applicable only for TPS25972A (Auto-retry variant)

**图 8-8. TPS2597x Overvoltage Response (Auto-Retry)**

There are three available overvoltage clamp threshold options, which can be configured using the OVCSEL pin.

**表 8-1. TPS2597x Overvoltage Clamp Threshold Selection**

OVCSEL PIN CONNECTION	OVERVOLTAGE CLAMP THRESHOLD
Shorted to GND	3.89 V
Open	5.76 V
Connected to GND through a 390-kΩ resistor	13.88 V

### 8.3.4 Inrush Current, Overcurrent, and Short Circuit Protection

TPS2597xx incorporates four levels of protection against overcurrent:

1. Adjustable slew rate (dVdt) for inrush current control
2. Adjustable threshold ( $I_{LIM}$ ) for overcurrent protection during start-up or steady-state
3. Adjustable threshold ( $I_{SC}$ ) for fast-trip response to severe overcurrent during start-up or steady-state
4. Fixed threshold ( $I_{FT}$ ) for fast-trip response to quickly protect against hard output short-circuits during steady-state

#### 8.3.4.1 Slew Rate (dVdt) and Inrush Current Control

During hot-plug events or while trying to charge a large output capacitance at start-up, there can be a large inrush current. If the inrush current is not managed properly, it can damage the input connectors or cause the system power supply to droop leading to unexpected restarts elsewhere in the system or both. The inrush current during turn on is directly proportional to the load capacitance and rising slew rate. Use [方程式 3](#) to find the slew rate (SR) required to limit the inrush current ( $I_{INRUSH}$ ) for a given load capacitance ( $C_{OUT}$ ):

$$SR (V/ms) = \frac{I_{INRUSH} (mA)}{C_{OUT} (\mu F)} \quad (3)$$

A capacitor can be connected to the dVdt pin to control the rising slew rate and lower the inrush current during turn on. Use [方程式 4](#) to calculate the required  $C_{dVdt}$  capacitance to produce a given slew rate.



$$C_{dVdt} (\text{pF}) = \frac{3300}{\text{SR} (\text{V/ms})} \quad (4)$$

The fastest output slew rate is achieved by leaving the dVdt pin open.

---

**备注**

For  $C_{dVdt} > 10 \text{ nF}$ , TI recommends to add a 100-Ω resistor in series with the capacitor on the dVdt pin.

---

### 8.3.4.2 Circuit-Breaker

The circuit-breaker variants (TPS25974x) respond to output overcurrent conditions by turning off the output after a user-adjustable transient fault blanking interval. When the load current exceeds the set overcurrent threshold ( $I_{LIM}$ ) set by the ILM pin resistor ( $R_{ILM}$ ), but stays lower than the fast-trip threshold ( $2 \times I_{LIM}$ ), the device starts discharging the ITIMER pin capacitor using an internal 2-μA pulldown current. If the load current drops below  $I_{LIM}$  before the ITIMER pin capacitor ( $C_{ITIMER}$ ) discharges by  $\Delta V_{ITIMER}$ , the ITIMER is reset by pulling it up to  $V_{INT}$  internally and the circuit breaker action is not engaged. This action allows short load transient pulses to pass through the device without tripping the circuit. If the overcurrent condition persists, the  $C_{ITIMER}$  continues to discharge and after it discharges by  $\Delta V_{ITIMER}$ , the circuit breaker action turns off the HFET immediately. At the same time, the  $C_{ITIMER}$  is charged up to  $V_{INT}$  again so that it is at its default state before the next overcurrent event. This action ensures the full blanking timer interval is provided for every overcurrent event. Use [方程式 5](#) to calculate the  $R_{ILM}$  value for an overcurrent threshold.

$$R_{ILM} (\Omega) = \frac{5747}{I_{LIM} (A)} \quad (5)$$

---

**备注**

1. Leaving the ILM pin Open sets the current limit to nearly zero and results in the part breaking the circuit with the slightest amount of loading at the output.
  2. Shorting the ILM pin to ground at any point during normal operation is detected as a fault and the part shuts down. There is a minimum current ( $I_{FLT}$ ) which the part allows in this condition before the pin short condition is detected.
- 

The duration for which transients are allowed can be adjusted using an appropriate capacitor value from ITIMER pin to ground. Use [方程式 6](#) to calculate the  $C_{ITIMER}$  value needed to set the desired transient overcurrent blanking interval.

$$t_{ITIMER} (\text{ms}) = \frac{\Delta V_{ITIMER} (V) \times C_{ITIMER} (\text{nF})}{I_{ITIMER} (\mu\text{A})} \quad (6)$$

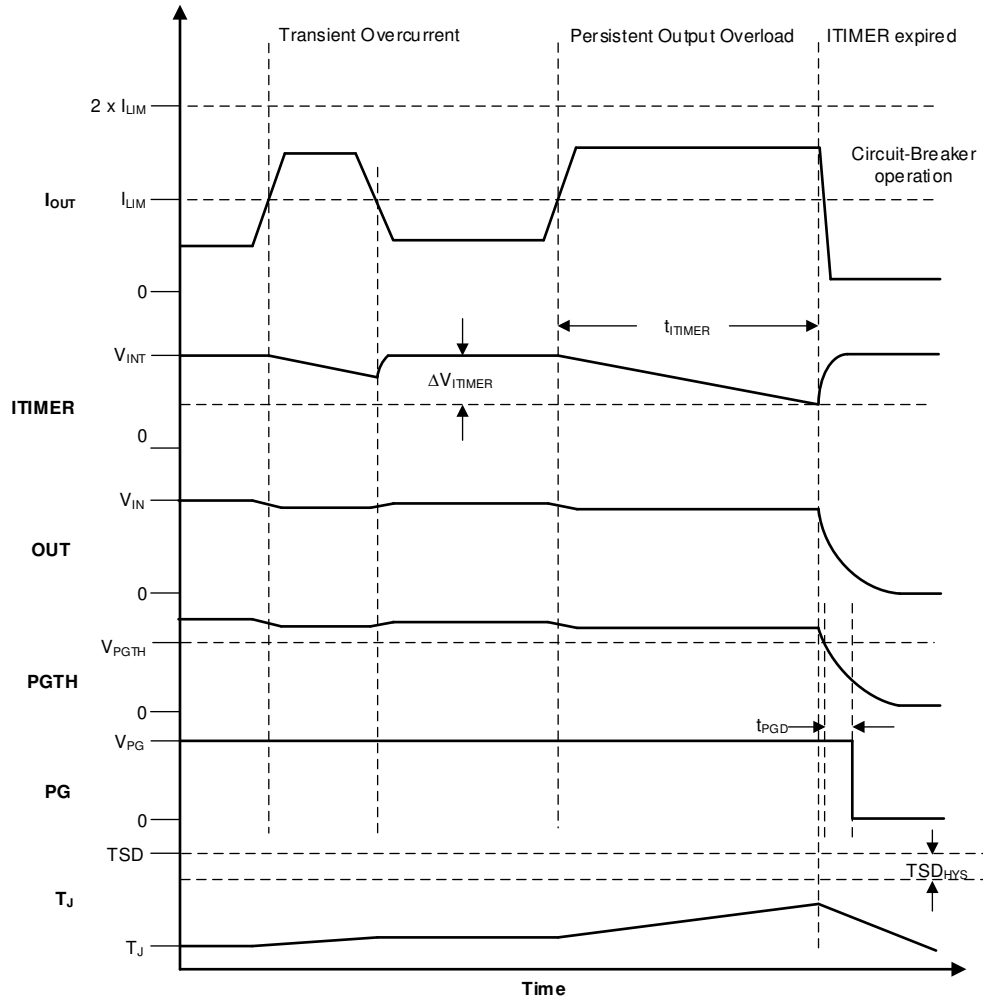


图 8-9. TPS25974x Overcurrent Response

## 备注

1. Leave the ITIMER pin open to allow the part to break the circuit with the minimum possible delay.
2. Shorting the ITIMER pin to ground results in minimum overcurrent response delay (similar to ITIMER pin open condition), but increases the device current consumption. This action is not a recommended mode of operation.
3. Increasing the ITIMER cap value extends the overcurrent blanking interval, but it also extends the time needed for the ITIMER cap to recharge up to  $V_{INT}$ . If the next overcurrent event occurs before the ITIMER cap is recharged fully, it takes less time to discharge to the ITIMER expiry threshold, thereby providing a shorter blanking interval than intended.

After the part shuts down due to a circuit-breaker fault, it either stays latched off (TPS25974L variant) or restart automatically after a fixed delay (TPS25974A variant).

### 8.3.4.3 Active Current Limiting

The active current limit variants (TPS25970x and TPS25972x) respond to output overcurrent conditions by actively limiting the current after a user adjustable transient fault blanking interval. When the load current exceeds the set overcurrent threshold ( $I_{LIM}$ ) set by the ILM pin resistor ( $R_{ILM}$ ), but stays lower than the short-circuit threshold ( $2 \times I_{LIM}$ ), the device starts discharging the ITIMER pin capacitor using an internal 2- $\mu$ A pulldown current. If the load current drops below the overcurrent threshold before the ITIMER capacitor ( $C_{ITIMER}$ ) discharges by  $\Delta V_{ITIMER}$ , the ITIMER is reset by pulling it up to  $V_{INT}$  internally and the current limit action is not

engaged. This event allows short load transient pulses to pass through the device without getting current limited. If the overcurrent condition persists, the  $C_{ITIMER}$  continues to discharge and after it discharges by  $\Delta V_{ITIMER}$ , the current limit starts regulating the HFET to actively limit the current to the set overcurrent threshold ( $I_{LIM}$ ). At the same time, the  $C_{ITIMER}$  is charged up to  $V_{INT}$  again so that it is at its default state before the next overcurrent event. This event ensures the full blanking timer interval is provided for every overcurrent event. Use [方程式 7](#) to calculate the  $R_{ILM}$  value for a desired overcurrent threshold.

$$R_{ILM} (\Omega) = \frac{5747}{I_{LIM} (A)} \quad (7)$$

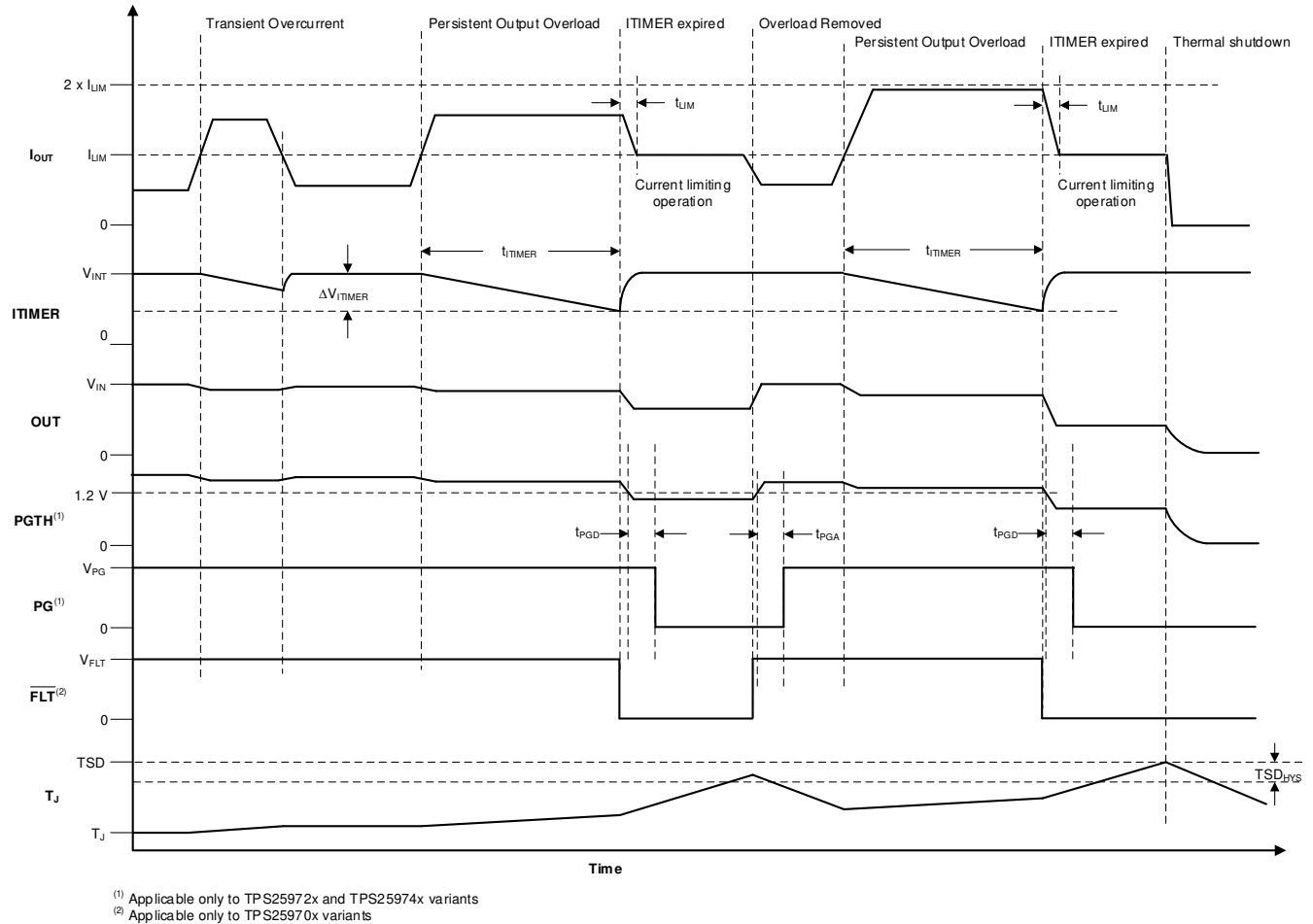
---

**备注**

1. Leaving the ILM pin open sets the current limit to nearly zero and results in the part entering current limit with the slightest amount of loading at the output.
  2. The current limit circuit employs a foldback mechanism. The current limit threshold in the foldback region ( $0 V < V_{OUT} < V_{FB}$ ) is lower than the steady state current limit threshold ( $I_{LIM}$ ).
  3. Shorting the ILM pin to ground at any point during normal operation is detected as a fault and the part shuts down. There's a minimum current ( $I_{FLT}$ ) which the part allows in this condition before the pin short condition is detected.
- 

The duration for which transients are allowed can be adjusted using an appropriate capacitor value from ITIMER pin to ground. Use [方程式 8](#) to calculate the  $C_{ITIMER}$  value needed to set the desired transient overcurrent blanking interval.

$$t_{ITIMER} (ms) = \frac{\Delta V_{ITIMER} (V) \times C_{ITIMER} (nF)}{I_{ITIMER} (\mu A)} \quad (8)$$



**图 8-10. TPS25970x 和 TPS25972x 主动电流限制响应**

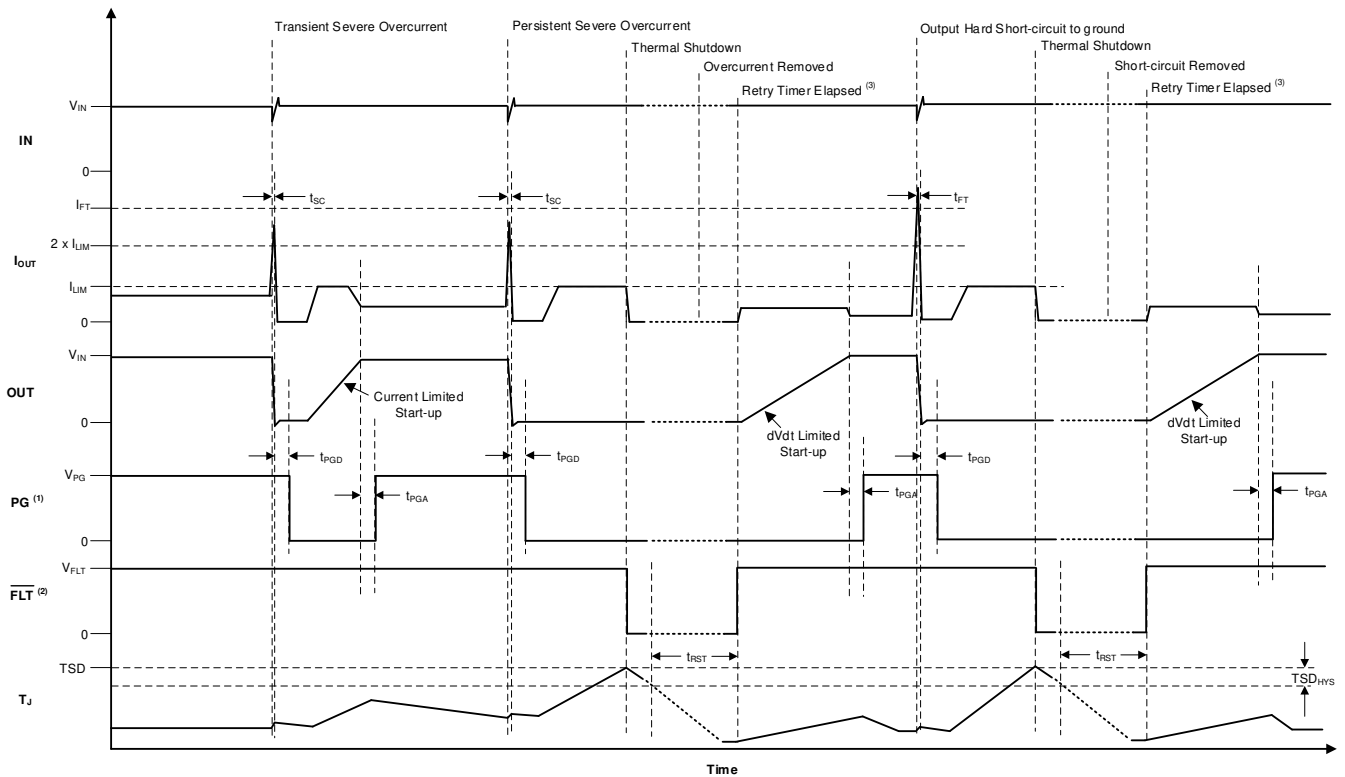
**备注**

1. Leave the ITIMER pin open to allow the part to limit the current with the minimum possible delay.
2. Shorting the ITIMER pin to ground results in minimum overcurrent response delay (similar to ITIMER pin open condition), but increases the device current consumption. This action is not a recommended mode of operation.
3. Active current limiting based on  $R_{ILIM}$  is active during start-up for TPS25970x, TPS25972x (active current limit) as well as TPS25974x (circuit-breaker) variants. In case the start-up current exceeds  $I_{LIM}$ , the device regulates the current to the set limit. However, during start-up the current limit is engaged without waiting for the ITIMER delay.
4. For the TPS25972x variants, during overvoltage clamp condition, if an overcurrent event occurs, the current limit is engaged without waiting for the ITIMER delay.
5. Increasing the  $C_{ITIMER}$  value extends the overcurrent blanking interval, but it also extends the time needed for the  $C_{ITIMER}$  to recharge up to  $V_{INT}$ . If the next overcurrent event occurs before the  $C_{ITIMER}$  is recharged fully, it takes lesser time to discharge to the ITIMER expiry threshold, thereby providing a shorter blanking interval than intended.

During active current limit, the output voltage drops, resulting in increased device power dissipation across the HFET. If the device internal temperature ( $T_J$ ) exceeds the thermal shutdown threshold (TSD), the HFET is turned off. After the part shuts down due to TSD fault, it either stays latched off (TPS2597xL variants) or restarts automatically after a fixed delay (TPS2597xA variants). See [Overtemperature Protection \(OTP\)](#) for more details on device response to overtemperature.

### 8.3.4.4 Short-Circuit Protection

During an output short-circuit event, the current through the device increases very rapidly. When a severe overcurrent condition is detected, the device triggers a fast-trip response to limit the current to a safe level. The internal fast-trip comparator employs a scalable threshold ( $I_{SC}$ ) which is equal to  $2 \times I_{LIM}$ . This action enables the user to adjust the fast-trip threshold rather than using a fixed threshold which can be too high for some low current systems. The device also employs a fixed fast-trip threshold ( $I_{FT}$ ) to protect fast protection against hard short-circuits during steady state. The fixed fast-trip threshold is higher than the maximum recommended user adjustable scalable fast-trip threshold. After the current exceeds  $I_{SC}$  or  $I_{FT}$ , the HFET is turned off completely within  $t_{FT}$ . Thereafter, the device tries to turn the HFET back on after a short de-glitch interval (30  $\mu$ s) in a current limited manner instead of a dVdt limited manner. This action ensures that the HFET has a faster recovery after a transient overcurrent event and minimizes the output voltage droop. However, if the fault is persistent, the device stays in current limit causing the junction temperature to rise and eventually enter thermal shutdown. For details on the device response to overtemperature, see [Overtemperature Protection \(OTP\)](#).



(1) Applicable only to TPS25972x and TPS25974x variants  
(2) Applicable only to TPS25970x variants  
(3) Applicable only to TPS2597xA variants

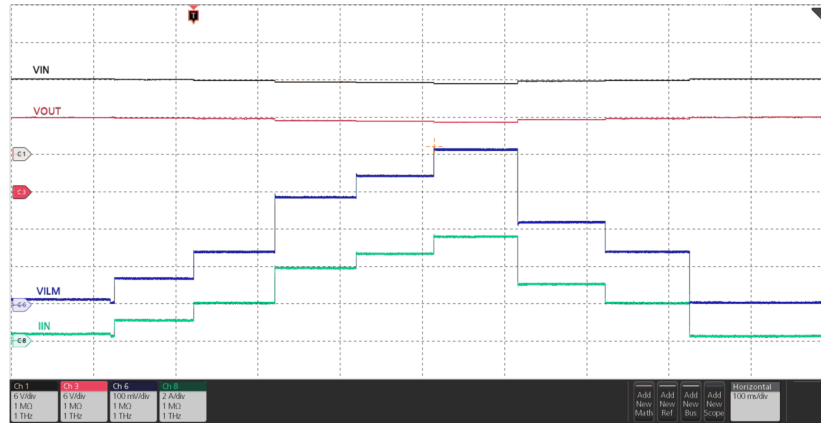
图 8-11. TPS2597xx Short-Circuit Response

### 8.3.5 Analog Load Current Monitor

The device allows the system to accurately monitor the output load current by providing an analog current sense output on the ILM pin, which is proportional to the current through the FET. The user can sense the voltage ( $V_{ILM}$ ) across the  $R_{ILM}$  to get a measure of the output load current.

$$I_{OUT} (A) = \frac{V_{ILM} (\mu V)}{R_{ILM} (\Omega) \times G_{IMON} (\mu A/A)} \quad (9)$$

The waveform below shows the ILM signal response to a load step at the output.



$V_{IN} = 12\text{ V}$ ,  $R_{ILM} = 715\ \Omega$ ,  $I_{OUT}$  varied dynamically between 0 A and 5.5 A

图 8-12. Analog Load Current Monitor Response

### 备注

The ILM pin is sensitive to capacitive loading. Careful design and layout is needed to ensure the parasitic capacitive loading on the ILM pin is  $< 50\text{ pF}$  for stable operation.

### 8.3.6 Overtemperature Protection (OTP)

The device monitors the internal die temperature ( $T_J$ ) at all times and shuts down the part as soon as the temperature exceeds a safe operating level (TSD), thereby protecting the device from damage. The device does not turn back on until the junction cools down sufficiently, that is the die temperature falls below  $(TSD - TSD_{HYS})$ .

When the TPS2597xL (latch-off variant) detects thermal overload, it shuts down and remains latched-off until the device is power cycled or re-enabled. When the TPS2597xA (auto-retry variant) detects thermal overload, it remains off until it has cooled down by  $TSD_{HYS}$ . Thereafter, the device remains off for an additional delay of  $t_{RST}$  after which it automatically retries to turn on if it is still enabled.

表 8-2. Thermal Shutdown

DEVICE	ENTER TSD	EXIT TSD
TPS2597xL (Latch-Off)	$T_J \geq TSD$	$T_J < TSD - TSD_{HYS}$ $V_{IN}$ cycled to 0 V and then above $V_{UVP(R)}$ OR EN/UVLO toggled below $V_{SD(F)}$
TPS2597xA (Auto-Retry)	$T_J \geq TSD$	$T_J < TSD - TSD_{HYS}$ $V_{IN}$ cycled to 0 V and then above $V_{UVP(R)}$ OR EN/UVLO toggled below $V_{SD(F)}$ or $t_{RST}$ timer expired

### 8.3.7 Fault Response and Indication ( $\overline{FLT}$ )

表 8-3 summarizes the device response to various fault conditions. Additionally, an active low external fault indication ( $\overline{FLT}$ ) pin is available on the TPS25970x variants.

表 8-3. Fault Summary

EVENT	PROTECTION RESPONSE	FAULT LATCHED INTERNALLY	$\overline{FLT}$ PIN STATUS <sup>(1)</sup>	$\overline{FLT}$ ASSERTION DELAY <sup>(1)</sup>
Overtemperature	Shutdown	Y	L	
Undervoltage (UVP or UVLO)	Shutdown	N	H	

**表 8-3. Fault Summary (continued)**

EVENT	PROTECTION RESPONSE	FAULT LATCHED INTERNALLY	FLT PIN STATUS <sup>(1)</sup>	FLT ASSERTION DELAY <sup>(1)</sup>
Input Overvoltage	Shutdown <sup>(1) (2)</sup>	N	H	
	Voltage Clamp <sup>(2)</sup>	N	N/A	
Transient Overcurrent ( $I_{LIM} < I_{OUT} < 2 \times I_{LIM}$ )	None	N	N	
Persistent Overcurrent	Circuit Breaker <sup>(3)</sup>	Y	N/A	
Persistent Overcurrent	Current Limit <sup>(4)</sup>	N	L	$t_{TIMER}$
Output Short-Circuit to GND	Circuit Breaker followed by Current Limit	N	H	
ILM Pin Open (During Steady State)	Shutdown	N	L	$t_{TIMER}$
ILM Pin Shorted to GND	Shutdown	Y	L	$t_{TIMER}$

- (1) Applicable to TPS25970x variants only.  
(2) Applicable to TPS25972x variants only.  
(3) Applicable to TPS25974x variants only.  
(4) Applicable to TPS25970x and TPS25972x variants only.

Faults which are latched internally can be cleared either by power cycling the part (pulling  $V_{IN}$  to 0 V) or by pulling the EN/UVLO pin voltage below  $V_{SD}$ . This action also releases the  $\overline{FLT}$  pin for the TPS25970x variants and resets the  $t_{RST}$  timer for the TPS2597xA (auto-retry) variants.

During a latched fault, pulling the EN/UVLO just below the UVLO threshold has no impact on the device. This fact is true for both TPS2597xL (latch-off) and TPS2597xA (auto-retry) variants.

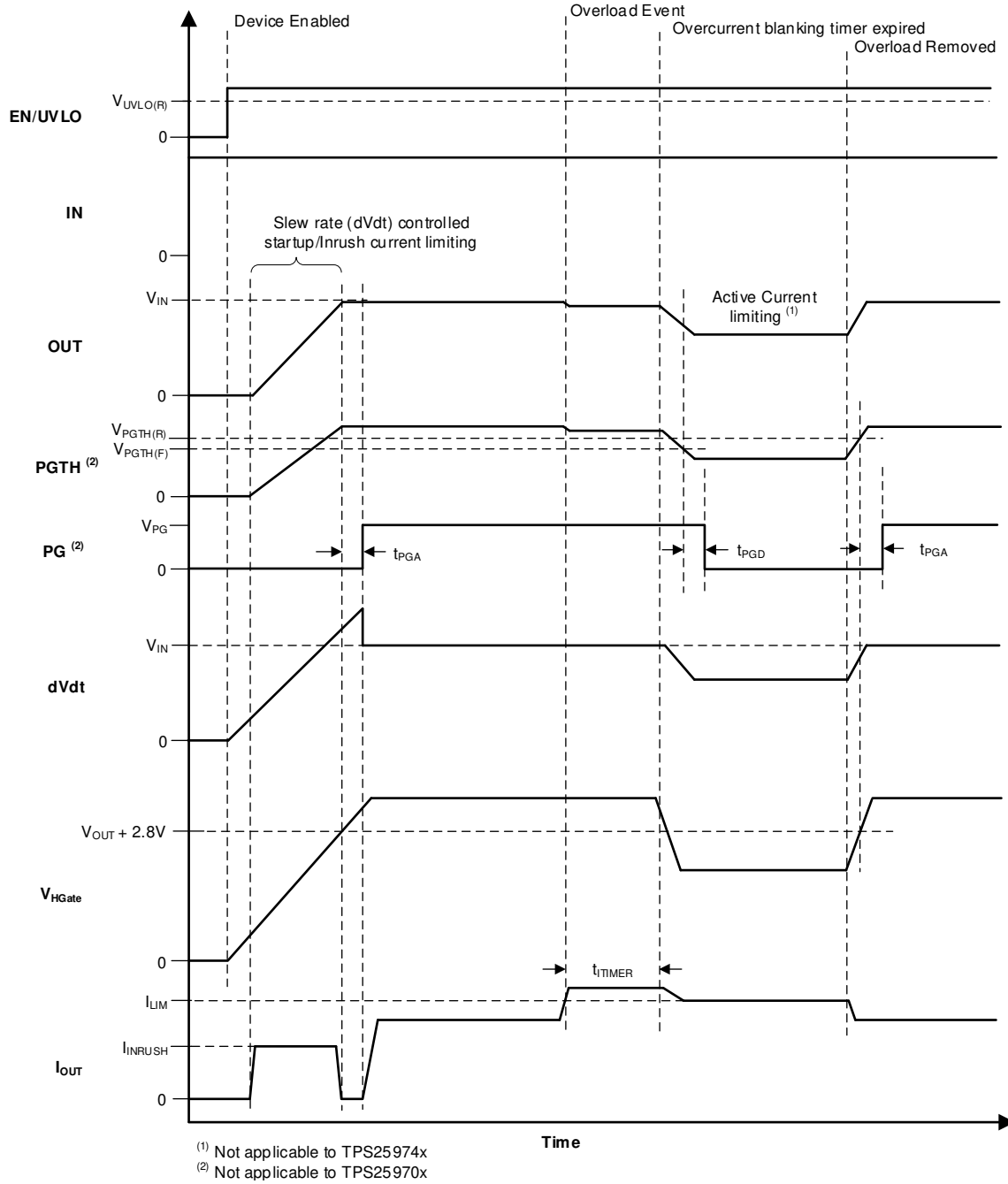
For TPS2597xA (auto-retry) variants, on expiry of the  $t_{RST}$  timer after a fault, the device restarts automatically and the  $\overline{FLT}$  pin is de-asserted (TPS25970A variant).

### 8.3.8 Power-Good Indication (PG)

The TPS25972x and TPS25974x variants provide an active high digital output (PG) which serves as a power-good indication signal and is asserted high depending on the voltage at the PGTH pin along with the device state information. The PG is an open-drain pin and must be pulled up to an external supply.

After power up, PG is pulled low initially. The device initiates a inrush sequence in which the HFET is turned on in a controlled manner. When the HFET gate voltage reaches the full overdrive indicating that the inrush sequence is complete and the voltage at PGTH is above  $V_{PGTH(R)}$ , the PG is asserted after a de-glitch time ( $t_{PGA}$ ).

PG is de-asserted if at any time during normal operation, the voltage at PGTH falls below  $V_{PGTH(F)}$ , or the device detects a fault (except overcurrent). The PG de-assertion de-glitch time is  $t_{PGD}$ .



**图 8-13. TPS25972x, TPS25974x PG Timing Diagram**



**表 8-4. TPS25972x and TPS25974x PG Indication Summary**

EVENT	DEVICE STATUS	PG PIN STATUS	PG PIN TOGGLE DELAY
Undervoltage (UVP or UVLO)	OFF	L	
Oversvoltage (TPS25972x only)	ON (Clamping)	H (If PGTH pin voltage > $V_{PGTH(R)}$ ) L (If PGTH pin voltage < $V_{PGTH(F)}$ )	$t_{PGA}$ $t_{PGD}$
Oversvoltage (TPS25974x only)	OFF	L	$t_{PGD}$
Steady state	ON	H (If PGTH pin voltage > $V_{PGTH(R)}$ ) L (If PGTH pin voltage < $V_{PGTH(F)}$ )	$t_{PGA}$ $t_{PGD}$
Transient overcurrent	ON	H (If PGTH pin voltage > $V_{PGTH(R)}$ ) L (If PGTH pin voltage < $V_{PGTH(F)}$ )	$t_{PGA}$ $t_{PGD}$
Persistent overload (TPS25972x only)	ON (Current Limiting)	H (If PGTH pin voltage > $V_{PGTH(R)}$ ) L (If PGTH pin voltage < $V_{PGTH(F)}$ )	$t_{PGA}$ $t_{PGD}$
Persistent overload (TPS25974x only)	OFF (Circuit-Breaker)	L	$t_{PGD}$
Output short-circuit to GND	Fast-trip followed by Current Limit	H (If PGTH pin voltage > $V_{PGTH(R)}$ ) L (If PGTH pin voltage < $V_{PGTH(F)}$ )	$t_{PGA}$ $t_{PGD}$
ILM pin open	OFF	L (If PGTH < 1.1 V)	$t_{PGD} + t_{TIMER}$
ILM pin shorted to GND	OFF	L	$t_{PGD}$
Overtemperature	OFF	L	$t_{PGD}$

When there is no supply to the device, the PG pin is expected to stay low. However, there is no active pulldown in this condition to drive this pin all the way down to 0 V. If the PG pin is pulled up to an independent supply which is present even if the device is unpowered, there can be a small voltage seen on this pin depending on the pin sink current, which is a function of the pullup supply voltage and resistor. Minimize the sink current to keep this pin voltage low enough not to be detected as a logic HIGH by associated external circuits in this condition.

## 8.4 Device Functional Modes

The TPS25970x and TPS25974x variants have only one functional mode that applies when operated within the recommended operating conditions.

The TPS25972x variants have three different functional modes depending on the OVCSEL pin connection.

**表 8-5. TPS25972x Oversvoltage Clamp Threshold Selection**

OVCSEL PIN CONNECTION	OVERVOLTAGE CLAMP THRESHOLD
Shorted to GND	3.89 V
Open	5.76 V
Connected to GND through a 390-k $\Omega$ resistor	13.88 V

## 9 Application and Implementation

### 备注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 9.1 Application Information

The TPS2597xx is a 2.7-V to 23-V, 7-A eFuse that is typically used for power rail protection applications. The device operates from 2.7 V to 23 V with adjustable overvoltage and undervoltage protection. The device provides ability to control inrush current and protection against overcurrent conditions. The device can be used in a variety of systems such as adapter input protection, server, PC motherboard, add-on cards, enterprise storage – RAID/HBA/SAN/eSSD, retail point-of-sale terminals, smartphones, and tablets. The design procedure explained in the subsequent sections can be used to select the supporting component values based on the application requirement. Additionally, a spreadsheet design tool, [TPS2597xx Design Calculator](#), is available in the web product folder.

#### 9.1.1 Single Device, Self-Controlled

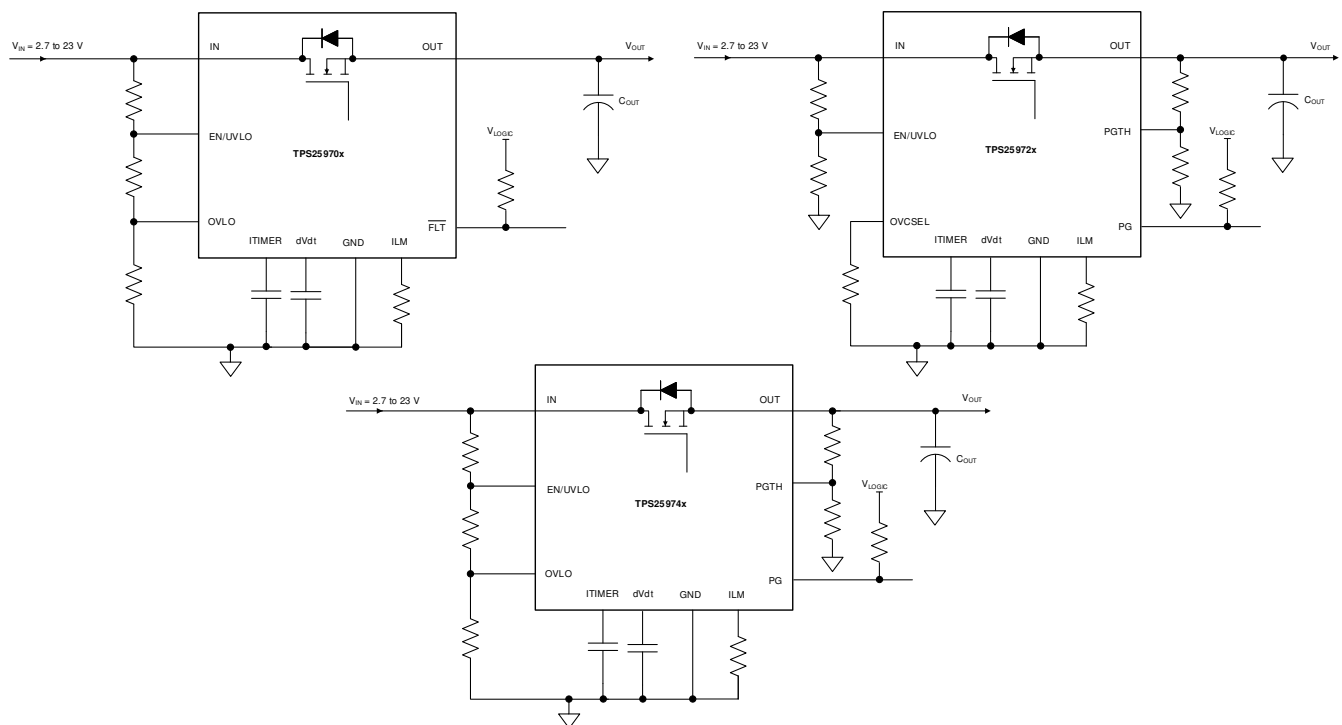


图 9-1. Single Device, Self-Controlled

#### Other variations:

In a Host MCU controlled system, EN/UVLO or OVLO can also be driven from the host GPIO to control the device.

ILM pin can be connected to the MCU ADC input for current monitoring purpose.

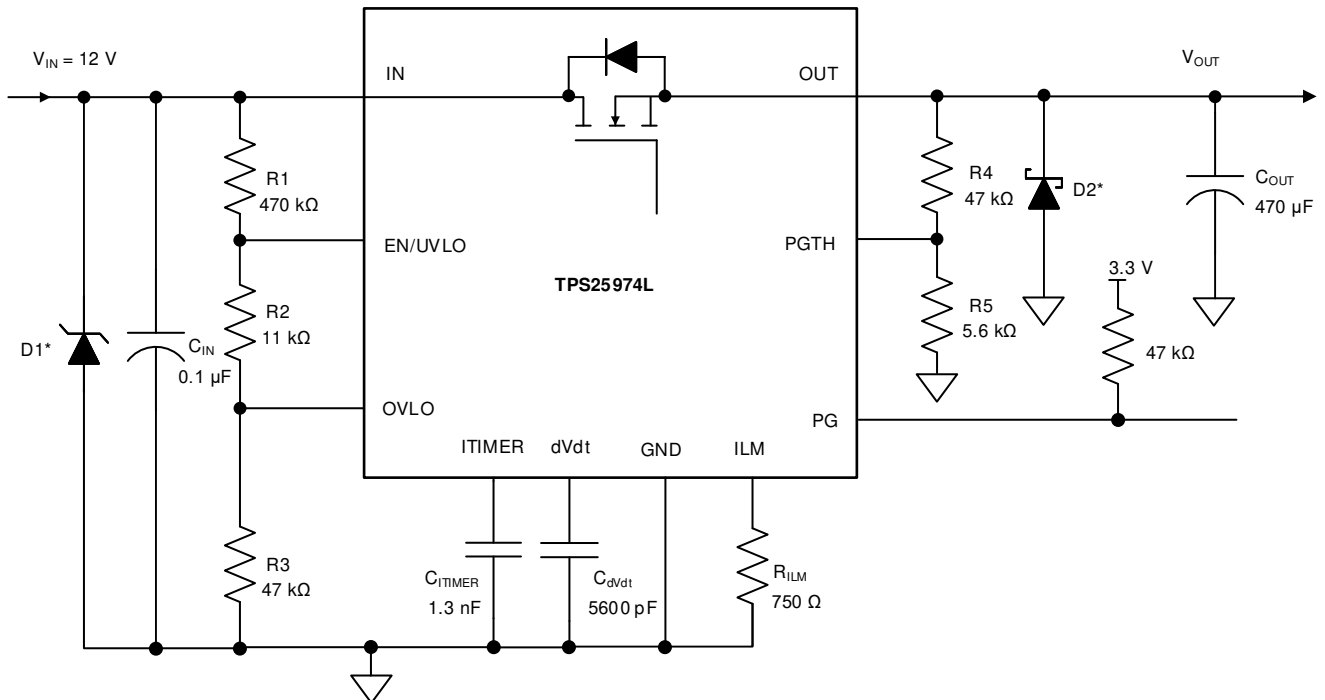
备注

TI recommends to keep parasitic capacitance on ILM pin below 50 pF to ensure stable operation.

For the TPS25972x and TPS25974x variants, either  $V_{IN}$  or  $V_{OUT}$  can be used to drive the PGTH resistor divider depending on which supply must be monitored for Power Good indication.

### 9.2 Typical Application

TPS2597xx can be used for server add-on card input power protection. During overcurrent or short-circuit event at load side, TPS2597xx can quickly respond to this fault event by turning off the device and thus protect the load from damage as well as prevent input supply from drooping. The ITIMER feature allows short duration peak currents to pass through without tripping the eFuse, thereby meeting the transient load current profile of these cards.



\* Optional circuit components needed for transient protection depending on input and output inductance. Please refer to [Transient Protection](#) section for details.

图 9-2. Server Add-on Card Input Power Protection

## 9.2.1 Design Requirements

表 9-1. Design Parameters

PARAMETER	VALUE
Input supply voltage ( $V_{IN}$ )	12 V
Undervoltage threshold ( $V_{IN(UV)}$ )	10.8 V
Overvoltage threshold ( $V_{IN(OV)}$ )	13.2 V
Output Power Good threshold ( $V_{PG}$ )	11.4 V
Maximum continuous current	7 A
Load transient blanking interval ( $t_{TIMER}$ )	1 ms
Output capacitance ( $C_{OUT}$ )	470 $\mu$ F
Output rise time ( $t_R$ )	20 ms
Overcurrent threshold ( $I_{LIM}$ )	7.7 A
Overcurrent response	Circuit breaker
Fault response	Latch-off

## 9.2.2 Detailed Design Procedure

### 9.2.2.1 Device Selection

Because the application requires circuit-breaker response to overcurrent with latch-off response after a fault, the TPS25974L variant is selected after referring to the [Device Comparison Table](#).

### 9.2.2.2 Setting Undervoltage and Overvoltage Thresholds

The supply undervoltage and overvoltage thresholds are set using the resistors R1, R2, and R3, whose values can be calculated using [方程式 10](#) and [方程式 11](#):

$$V_{IN(UV)} = \frac{V_{UVLO(R)} \times (R1 + R2 + R3)}{R2 + R3} \quad (10)$$

$$V_{IN(OV)} = \frac{V_{OV(R)} \times (R1 + R2 + R3)}{R3} \quad (11)$$

Where  $V_{UVLO(R)}$  is the UVLO rising threshold and  $V_{OV(R)}$  is the OVLO rising threshold. Because R1, R2, and R3 leak the current from input supply  $V_{IN}$ , these resistors must be selected based on the acceptable leakage current from input power supply  $V_{IN}$ . The current drawn by R1, R2, and R3 from the power supply is  $I_{R123} = V_{IN} / (R1 + R2 + R3)$ . However, leakage currents due to external active components connected to the resistor string can add error to these calculations. So, the resistor string current,  $I_{R123}$  must be chosen to be 20 times greater than the leakage current expected on the EN/UVLO and OVLO pins.

From the device electrical specifications, both the EN/UVLO and OVLO leakage currents are 0.1  $\mu$ A (maximum),  $V_{OV(R)} = 1.2$  V and  $V_{UVLO(R)} = 1.2$  V. From design requirements,  $V_{IN(OV)} = 13.2$  V and  $V_{IN(UV)} = 10.8$  V. To solve the equation, first choose the value of R1 = 470 k $\Omega$  and use the above equations to solve for R2 = 10.7 k $\Omega$  and R3 = 48 k $\Omega$ .

Using the closest standard 1% resistor values, we get R1 = 470 k $\Omega$ , R2 = 11 k $\Omega$ , and R3 = 47 k $\Omega$ .

### 9.2.2.3 Setting Output Voltage Rise Time ( $t_R$ )

For a successful design, the junction temperature of the device must be kept below the absolute maximum rating during both dynamic (start-up) and steady-state conditions. Dynamic power stresses often are an order of magnitude greater than the static stresses, so it is important to determine the right start-up time and inrush current limit required with system capacitance to avoid thermal shutdown during start-up.

The slew rate (SR) needed to achieve the desired output rise time can be calculated as:

$$SR (V/ms) = \frac{V_{IN} (V)}{t_R (ms)} = \frac{12 V}{20 ms} = 0.6 V/ms \quad (12)$$

The  $C_{dVdt}$  needed to achieve this slew rate can be calculated as:

$$C_{dVdt} \text{ (pF)} = \frac{3300}{SR \text{ (V/ms)}} = \frac{3300}{0.6} = 5500 \text{ pF} \quad (13)$$

Choose the nearest standard capacitor value as 5600 pF.

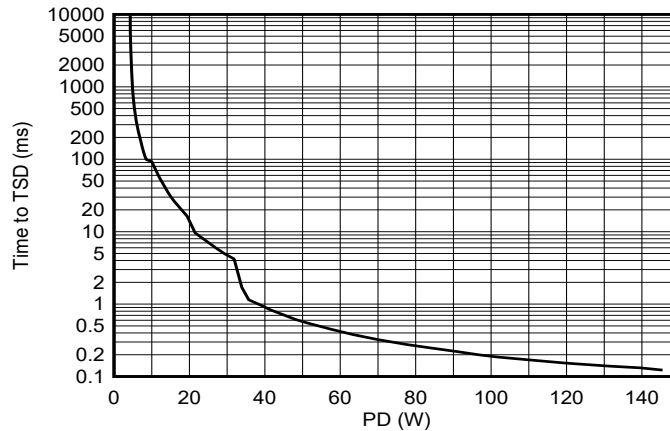
For this slew rate, the inrush current can be calculated as:

$$I_{INRUSH} \text{ (mA)} = SR \text{ (V/ms)} \times C_{OUT} \text{ (}\mu\text{F)} = 0.6 \times 470 = 282 \text{ mA} \quad (14)$$

The average power dissipation inside the part during inrush can be calculated as:

$$P_{DINRUSH} \text{ (W)} = \frac{I_{INRUSH} \text{ (A)} \times V_{IN} \text{ (V)}}{2} = \frac{0.282 \times 12}{2} = 1.69 \text{ W} \quad (15)$$

For the given power dissipation, the thermal shutdown time of the device must be greater than the ramp-up time  $t_R$  to avoid start-up failure. 图 9-3 shows the thermal shutdown limit. For 1.69 W of power, the shutdown time is more than 10 s, which is very large as compared to  $t_R = 20 \text{ ms}$ . Therefore, it is safe to use 20 ms as the start-up time for this application.



**图 9-3. Thermal Shut-Down Plot During Inrush**

**备注**

In some systems, there can be active load circuits (for example, DC-DC converters) with low turn-on threshold voltages which can start drawing power before the eFuse has completed the inrush sequence. This action can cause additional power dissipation inside the eFuse during start-up and can lead to thermal shutdown. TI recommends to use the Power Good (PG) pin of the eFuse to enable and disable the load circuit. This action ensures that the load is turned on only when the eFuse has completed its start-up and is ready to deliver full power without the risk of hitting thermal shutdown.

**9.2.2.4 Setting Power-Good Assertion Threshold**

The Power Good assertion threshold can be set using the resistors R4 and R5 connected to the PGTH pin, whose values can be calculated as:

$$V_{PG} = \frac{V_{PGTH(R)} \times (R4 + R5)}{R5} \quad (16)$$

Because R4 and R5 leak the current from the output rail  $V_{OUT}$ , these resistors must be selected to minimize the leakage current. The current drawn by R4 and R5 from the power supply is  $I_{R45} = V_{OUT} / (R4 + R5)$ . However, leakage currents due to external active components connected to the resistor string can add error to these calculations. So, the resistor string current,  $I_{R123}$  must be chosen to be 20 times greater than the PGTH leakage current expected.

From the device electrical specifications, PGTH leakage current is 1  $\mu\text{A}$  (maximum),  $V_{\text{PGTH(R)}} = 1.2\text{ V}$  and from design requirements,  $V_{\text{PG}} = 11.4\text{ V}$ . To solve the equation, first choose the value of  $R_4 = 47\text{ k}\Omega$  and calculate  $R_5 = 5.52\text{ k}\Omega$ . Choose the nearest 1% standard resistor value as  $R_5 = 5.6\text{ k}\Omega$ .

### 9.2.2.5 Setting Overcurrent Threshold ( $I_{\text{LIM}}$ )

The overcurrent protection (Circuit Breaker) threshold can be set using the  $R_{\text{ILM}}$  resistor whose value can be calculated as:

$$R_{\text{ILM}} (\Omega) = \frac{5747}{I_{\text{LIM}} (\text{A})} = \frac{5747}{7.7\text{ A}} = 746.4\ \Omega \quad (17)$$

Choose nearest 1% standard resistor value as 715  $\Omega$ .

### 9.2.2.6 Setting Overcurrent Blanking Interval ( $t_{\text{TIMER}}$ )

The overcurrent blanking timer interval can be set using the  $C_{\text{TIMER}}$  capacitor whose value can be calculated as:

$$C_{\text{TIMER}} (\text{nF}) = \frac{t_{\text{TIMER}} (\text{ms}) \times I_{\text{TIMER}} (\mu\text{A})}{\Delta V_{\text{TIMER}} (\text{V})} = \frac{1 \times 2}{1.52} = 1.32\text{ nF} \quad (18)$$

Choose nearest standard capacitor value as 1.3 nF.

## 9.2.3 Application Curves

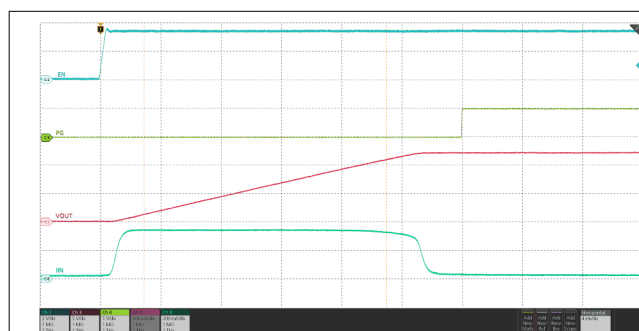


图 9-4. Power Up

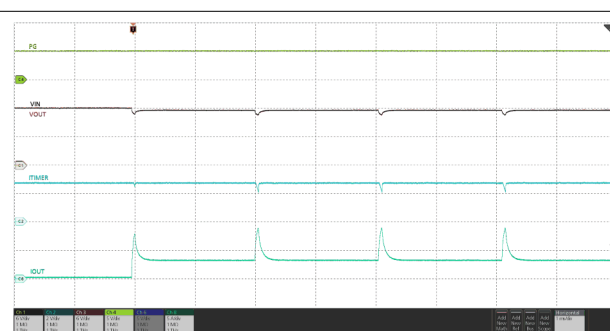


图 9-5. Transient Overload

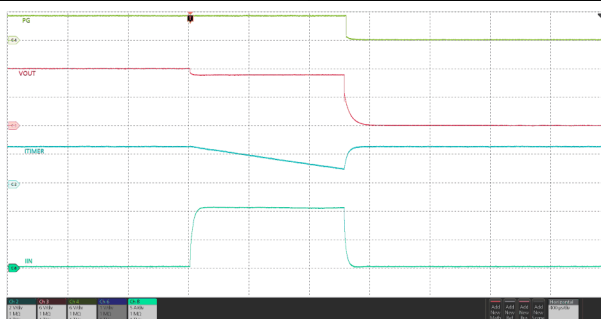
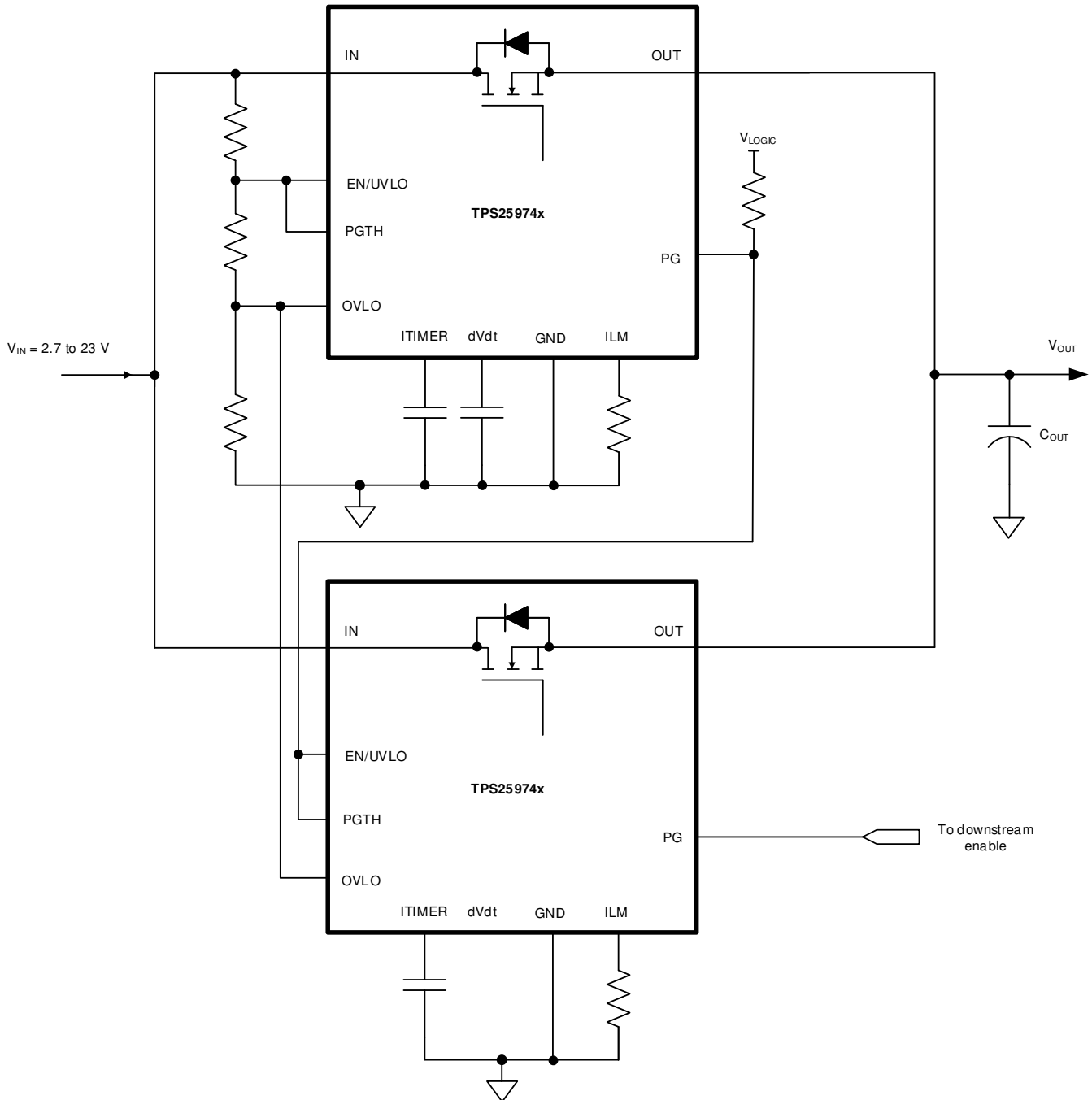


图 9-6. Circuit Breaker Response

## 9.3 Parallel Operation

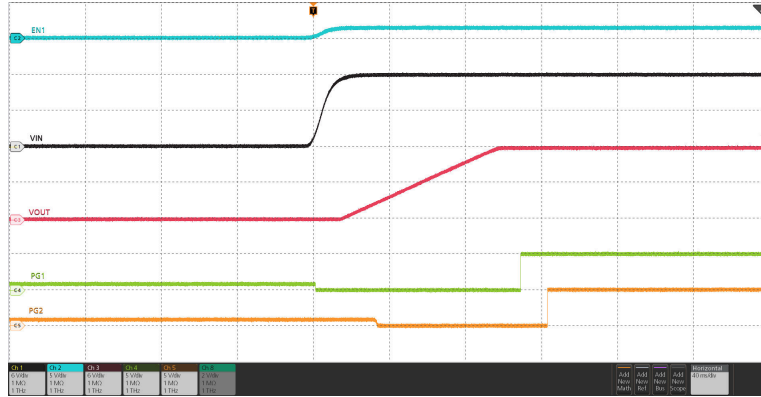
Applications that need higher steady current can use two TPS25974x devices connected in parallel as shown in 图 9-7. In this configuration, the first device turns on initially to provide the inrush current control. The second device is held in an OFF state by driving its EN/UVLO pin low using the PG signal of the first device. After the inrush sequence is complete, the first device asserts its PG pin high and turns on the second device. The second device asserts its PG signal to indicate when it has turned on fully, thereby indicating to the system that the parallel combination is ready to deliver the full steady state current.

After in steady state, both devices share current nearly equally. There can be a slight skew in the currents depending on the part-to-part variation in the  $R_{ON}$  as well as the PCB trace resistance mismatch.

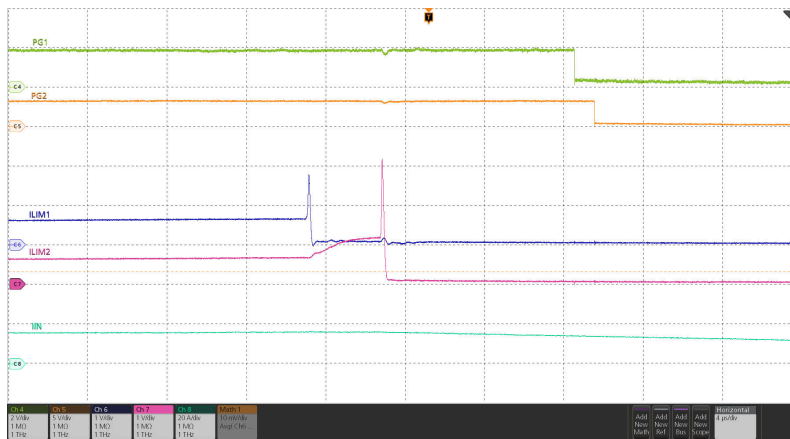


**图 9-7. Two Devices Connected in Parallel for Higher Steady State Current Capability**

The waveforms below illustrate the behavior of the parallel configuration during start-up as well as during steady state.



**图 9-8. Parallel Devices Sequencing During Start-Up**



**图 9-9. Parallel Devices Load Current During Steady State and Overload**



## 10 Power Supply Recommendations

The TPS2597xx devices are designed for a supply voltage range of  $2.7\text{ V} \leq V_{\text{IN}} \leq 23\text{ V}$ . TI recommends an input ceramic bypass capacitor higher than  $0.1\text{ }\mu\text{F}$  if the input supply is located more than a few inches from the device. The power supply must be rated higher than the set current limit to avoid voltage droops during overcurrent and short-circuit conditions.

### 10.1 Transient Protection

In the case of a short-circuit and overload current limit when the device interrupts current flow, the input inductance generates a positive voltage spike on the input, and the output inductance generates a negative voltage spike on the output. The peak amplitude of voltage spikes (transients) is dependent on the value of inductance in series to the input or output of the device. Such transients can exceed the absolute maximum ratings of the device if steps are not taken to address the issue. Typical methods for addressing transients include:

- Minimize lead length and inductance into and out of the device.
- Use a large PCB GND plane.
- Connect a Schottky diode from the OUT pin ground to absorb negative spikes.
- Connect a low ESR capacitor larger than  $1\text{ }\mu\text{F}$  at the OUT pin very close to the device.
- Use a low-value ceramic capacitor  $C_{\text{IN}} = 1\text{ }\mu\text{F}$  to absorb the energy and dampen the transients. The capacitor voltage rating must be at least twice the input supply voltage to be able to withstand the positive voltage excursion during inductive ringing.

Use [方程式 19](#) to estimate the approximate value of input capacitance:

$$V_{\text{SPIKE(Absolute)}} = V_{\text{IN}} + I_{\text{LOAD}} \times \sqrt{\frac{L_{\text{IN}}}{C_{\text{IN}}}} \quad (19)$$

where

- $V_{\text{IN}}$  is the nominal supply voltage.
- $I_{\text{LOAD}}$  is the load current.
- $L_{\text{IN}}$  equals the effective inductance seen looking into the source.
- $C_{\text{IN}}$  is the capacitance present at the input.
- Some applications can require the addition of a Transient Voltage Suppressor (TVS) to prevent transients from exceeding the absolute maximum ratings of the device. In some cases, even if the maximum amplitude of the transients is below the absolute maximum rating of the device, a TVS can help to absorb the excessive energy dump and prevent it from creating very fast transient voltages on the input supply pin of the IC, which can couple to the internal control circuits and cause unexpected behavior.

 [10-1](#) shows the circuit implementation with optional protection components.

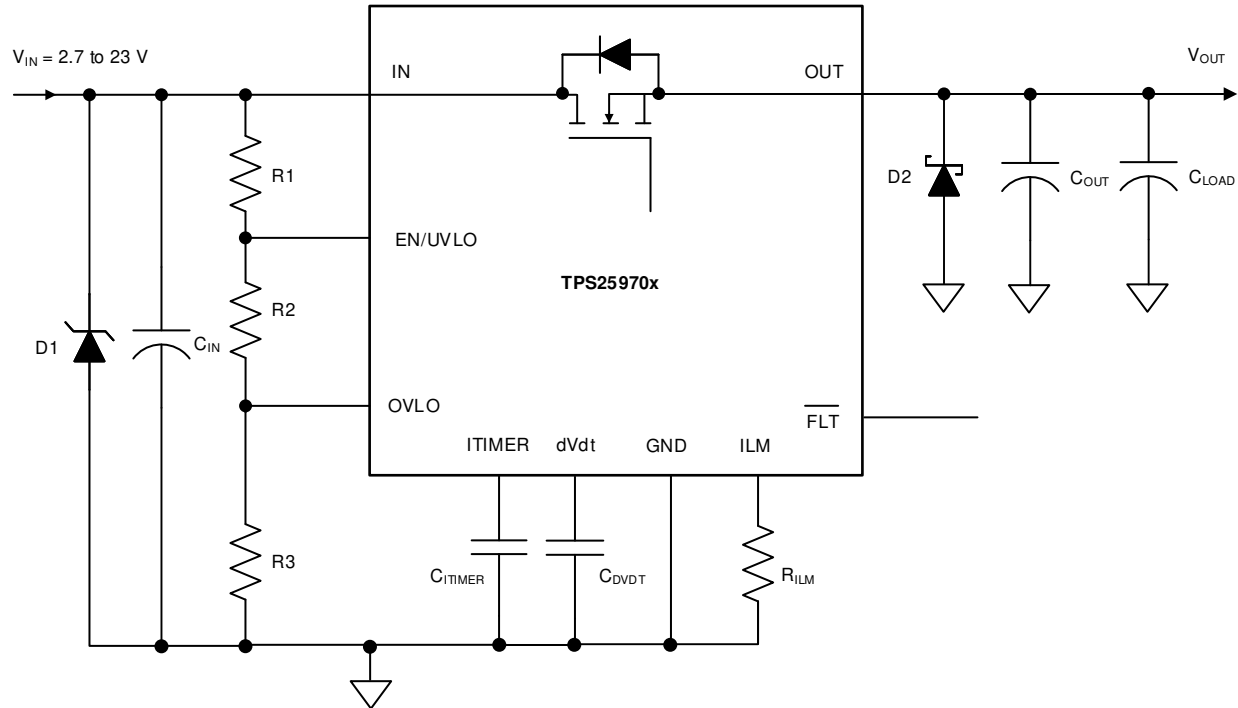


图 10-1. Circuit Implementation With Optional Protection Components

## 10.2 Output Short-Circuit Measurements

It is difficult to obtain repeatable and similar short-circuit testing results. The following contribute to variation in results:

- Source bypassing
- Input leads
- Circuit layout
- Component selection
- Output shorting method
- Relative location of the short
- Instrumentation

The actual short exhibits a certain degree of randomness because it microscopically bounces and arcs. Ensure that configuration and methods are used to obtain realistic results. Do not expect to see waveforms exactly like those in this data sheet because every setup is different.

## 11 Layout

### 11.1 Layout Guidelines

- For all applications, TI recommends a ceramic decoupling capacitor of 0.1  $\mu\text{F}$  or greater between the IN terminal and GND terminal.
- The optimal placement of the decoupling capacitor is closest to the IN and GND terminals of the device. Care must be taken to minimize the loop area formed by the bypass-capacitor connection, the IN terminal, and the GND terminal of the IC.
- High current-carrying power-path connections must be as short as possible and must be sized to carry at least twice the full-load current.
- The GND terminal must be tied to the PCB ground plane at the terminal of the IC with the shortest possible trace. The PCB ground must be a copper plane or island on the board. TI recommends to have a separate ground plane island for the eFuse. This plane does not carry any high currents and serves as a quiet ground reference for all the critical analog signals of the eFuse. The device ground plane must be connected to the system power ground plane using a star connection.
- The IN and OUT pins are used for heat dissipation. Connect to as much copper area on top and bottom PCB layers using as possible with thermal vias. The vias under the device also help to minimize the voltage gradient across the IN and OUT pads and distribute current uniformly through the device, which is essential to achieve the best on-resistance and current sense accuracy.
- Locate the following support components close to their connection pins:
  - $R_{\text{ILM}}$
  - $C_{\text{dVdT}}$
  - $C_{\text{ITIMER}}$
  - Resistors for the EN/UVLO, OVLO/OVCSEL, and PGTH pins
- Connect the other end of the component to the GND pin of the device with shortest trace length. The trace routing for the  $R_{\text{ILM}}$ ,  $C_{\text{ITIMER}}$  and  $C_{\text{dVdT}}$  components to the device must be as short as possible to reduce parasitic effects on the current limit, overcurrent blanking interval and soft start timing. It's recommended to keep parasitic capacitance on ILM pin below 50 pF to ensure stable operation. These traces must not have any coupling to switching signals on the board.
- Because the bias current on ILM pin directly controls the overcurrent protection behavior of the device, the PCB routing of this node must be kept away from any noisy (switching) signals.
- Protection devices such as TVS, snubbers, capacitors, or diodes must be placed physically close to the device they are intended to protect. These protection devices must be routed with short traces to reduce inductance. For example, TI recommends a protection Schottky diode to address negative transients due to switching of inductive loads. TI also recommends to add a ceramic decoupling capacitor of 1  $\mu\text{F}$  or greater between OUT and GND. These components must be physically close to the OUT pins. Care must be taken to minimize the loop area formed by the Schottky diode/bypass-capacitor connection, the OUT pin, and the GND terminal of the IC.

### 11.2 Layout Example

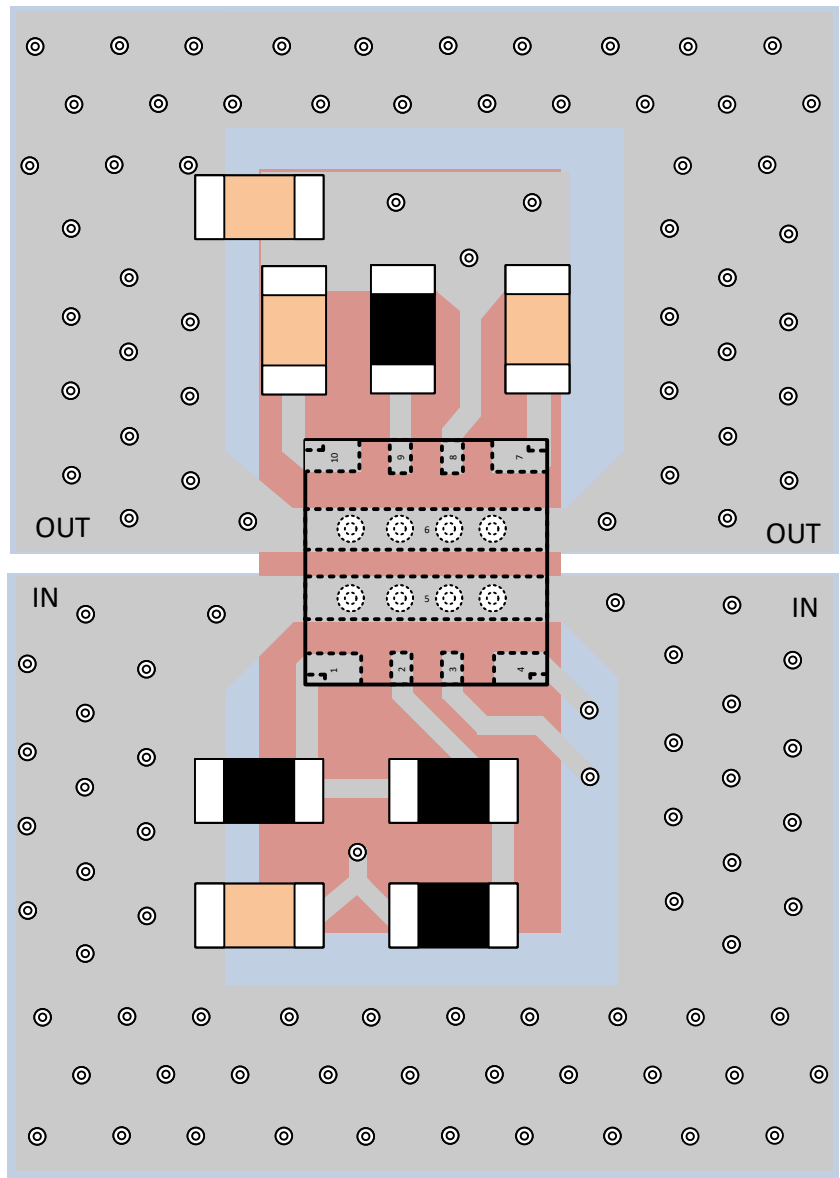
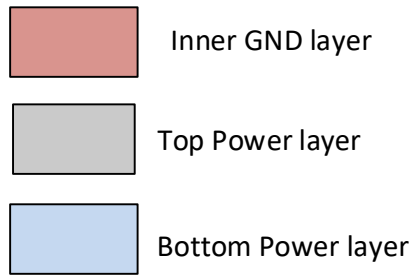


图 11-1. Layout Example - Single TPS25974x With PGTH Referred to OUT

## 12 Device and Documentation Support

TI offers an extensive line of development tools. Tools and software to evaluate the performance of the device, generate code, and develop solutions are listed below.

### 12.1 Device Support

#### 12.1.1 第三方产品免责声明

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### 12.2 Documentation Support

#### 12.2.1 Related Documentation

For related documentation see the following:

- Texas Instruments, [TPS2597EVM eFuse Evaluation Board user's guide](#)
- Texas Instruments, [TPS2597xx Design Calculator](#)

### 12.3 接收文档更新通知

要接收文档更新通知，请导航至 [ti.com](http://ti.com) 上的器件产品文件夹。点击 [订阅更新](#) 进行注册，即可每周接收产品信息更改摘要。有关更改的详细信息，请查看任何已修订文档中包含的修订历史记录。

### 12.4 支持资源

[TI E2E™ 支持论坛](#) 是工程师的重要参考资料，可直接从专家获得快速、经过验证的解答和设计帮助。搜索现有解答或提出自己的问题可获得所需的快速设计帮助。

链接的内容由各个贡献者“按原样”提供。这些内容并不构成 TI 技术规范，并且不一定反映 TI 的观点；请参阅 TI 的 [《使用条款》](#)。

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### 12.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 12.7 术语表

#### TI 术语表

本术语表列出并解释了术语、首字母缩略词和定义。

## 13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS25970ARPWR	ACTIVE	VQFN-HR	RPW	10	3000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	2KNH	<a href="#">Samples</a>
TPS25970LRPWR	ACTIVE	VQFN-HR	RPW	10	3000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	2KOH	<a href="#">Samples</a>
TPS25972ARPWR	ACTIVE	VQFN-HR	RPW	10	3000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	2KPH	<a href="#">Samples</a>
TPS25972LRPWR	ACTIVE	VQFN-HR	RPW	10	3000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	2KQH	<a href="#">Samples</a>
TPS25974ARPWR	ACTIVE	VQFN-HR	RPW	10	3000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	2KRH	<a href="#">Samples</a>
TPS25974LRPWR	ACTIVE	VQFN-HR	RPW	10	3000	RoHS & Green	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	2KSH	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

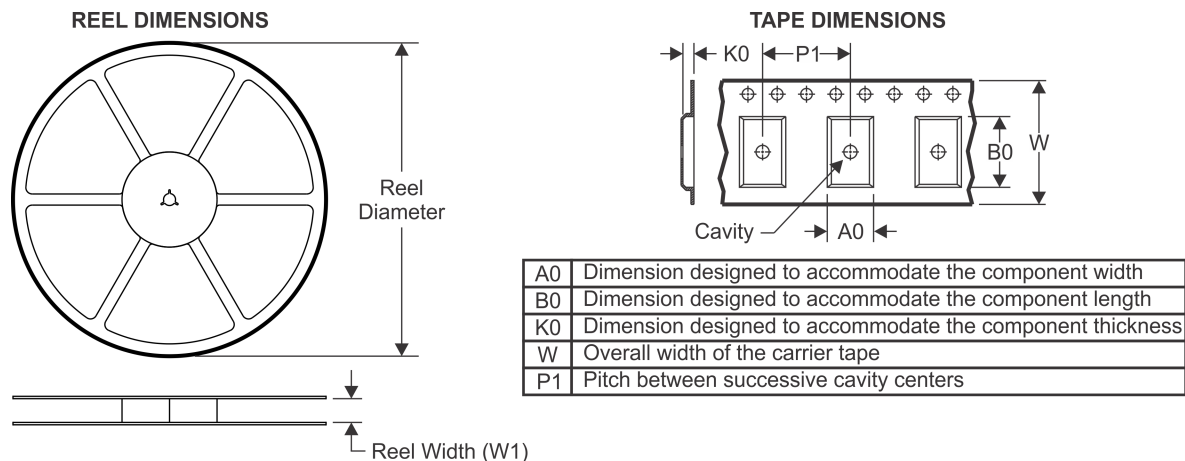
(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

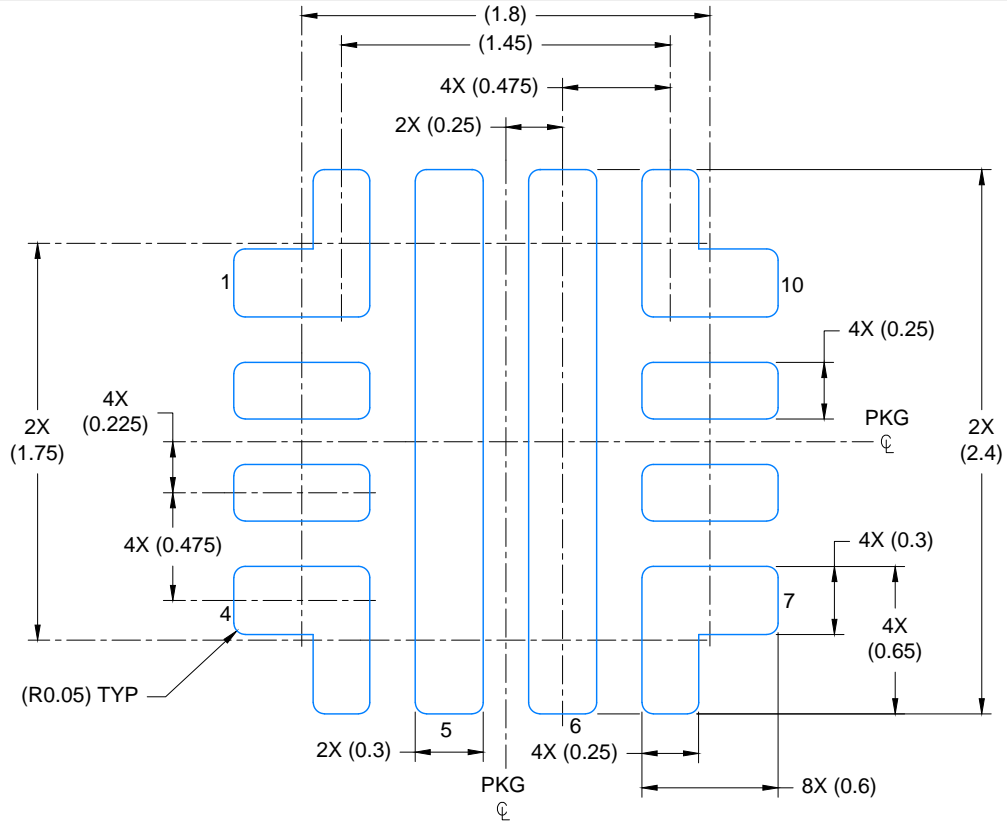
Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS25970ARPWR	VQFN-HR	RPW	10	3000	180.0	8.4	2.3	2.3	1.15	4.0	8.0	Q2
TPS25970LRPWR	VQFN-HR	RPW	10	3000	180.0	8.4	2.3	2.3	1.15	4.0	8.0	Q2
TPS25972ARPWR	VQFN-HR	RPW	10	3000	180.0	8.4	2.3	2.3	1.15	4.0	8.0	Q2
TPS25972LRPWR	VQFN-HR	RPW	10	3000	180.0	8.4	2.3	2.3	1.15	4.0	8.0	Q2
TPS25974ARPWR	VQFN-HR	RPW	10	3000	180.0	8.4	2.3	2.3	1.15	4.0	8.0	Q2
TPS25974LRPWR	VQFN-HR	RPW	10	3000	180.0	8.4	2.3	2.3	1.15	4.0	8.0	Q2

**TAPE AND REEL BOX DIMENSIONS**

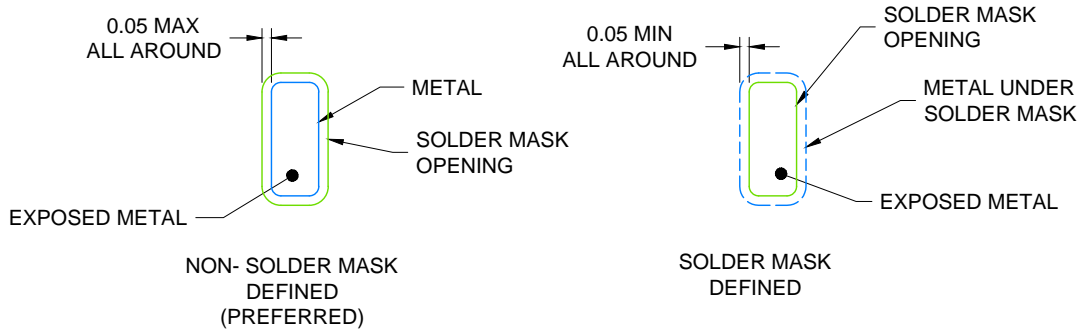

\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS25970ARPWR	VQFN-HR	RPW	10	3000	210.0	185.0	35.0
TPS25970LRPWR	VQFN-HR	RPW	10	3000	210.0	185.0	35.0
TPS25972ARPWR	VQFN-HR	RPW	10	3000	210.0	185.0	35.0
TPS25972LRPWR	VQFN-HR	RPW	10	3000	210.0	185.0	35.0
TPS25974ARPWR	VQFN-HR	RPW	10	3000	210.0	185.0	35.0
TPS25974LRPWR	VQFN-HR	RPW	10	3000	210.0	185.0	35.0





LAND PATTERN EXAMPLE  
SCALE: 30X



SOLDER MASK DETAILS  
NOT TO SCALE

4225183/A 08/2019

NOTES: (continued)

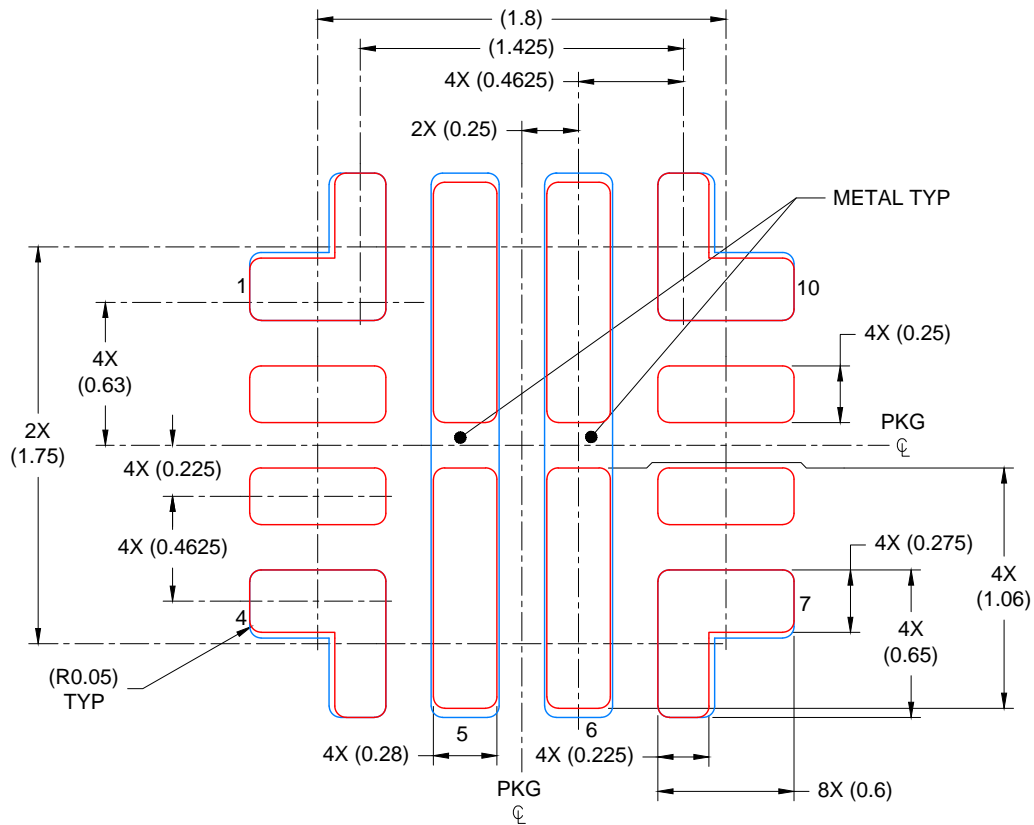
3. For more information, see Texas Instruments literature number SLUA271 ([www.ti.com/lit/sluea271](http://www.ti.com/lit/sluea271)).
4. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

RPW0010A

VQFN-HR - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



SOLDER PASTE EXAMPLE  
BASED ON 0.100 mm THICK STENCIL

PADS 1, 4, 7 & 10: 93%; PADS 5 & 6: 82%  
SCALE: 30X

4225183/A 08/2019

NOTES: (continued)

5. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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