## AFE5812 具有 CW 无源混频器及数字 I／Q 解调器的， $0.75 \mathrm{nV} / \mathrm{rtHz}, ~ 14 / 12$位，65MSPS，180mW／通道全集成 8 通道超声波模拟前端

## 1 特性

- 8 通道完全模拟前端
- LNA，VCAT，PGA，LPF，ADC和连续波（CW）混频器
- 可编程增益低噪音放大器（LNA）
- 24，18，15dB 增益
- $0.25, ~ 0.5, ~ 0.7 \mathrm{~V}_{\mathrm{PP}}$ 线性输入范围
- $0.63,0.7,0.9 \mathrm{nV} / \mathrm{rtHz}$ 输入参考噪音
- 可编程主动终止
- 40 dB 低噪音压控衰减器（VACT）
- $24 / 30 \mathrm{~dB}$ 可编程增益放大器（PGA）
- $3^{\text {rd }}$ 阶线性相位低通滤波器（LPF）
－10，15，20，30，35，50MHz
- 14 位模数转换器，具有 LVDS 输出
- 65MSPS 时为 77dBFS SNR
- 噪声／功率优化（无数字解调器）
- $0.75 \mathrm{nV} / \mathrm{rtHz}, 65 \mathrm{MSPS}$ 时为每通道 180 mW
- $1.1 \mathrm{nV} / \mathrm{rtHz}$ ，40MSPS 时为每通道 109 mW
- 在 CW 模式下为每通道 107 mW
- 出色的器件间增益匹配
$- \pm 0.5 \mathrm{~dB}$（典型值）和 $\pm 1.1 \mathrm{~dB}$（最大值）
- ADC 之后的可编程数字 I／Q 解调器
- 宽范围解调频率
- $<1 \mathrm{KHz}$ 的频率分辨率
- 抽取滤波器因数 $M=1$ 至 32
- $16 x M$ 抽头有限冲击响应（FIR）抽取滤波器
- 解调之后的低压差分信令（LVDS）速率衰减
- 具有 32 个预设定参数的片上 RAM
- 低谐波失真
- 低频声纳信号处理
- 快速且持续的过载恢复
- 针对连续声波多普勒（CWD）的无源混频器
- 低接近相位噪声－在低于 1 KHz 至 2.5 MHz 载波时为 $156 \mathrm{dBc} / \mathrm{Hz}$
- $1 / 16 \lambda$ 的相位分辨率
- 支持 16X， $8 \mathrm{X}, 4 \mathrm{X}$ 和 1 XCW 时钟
- 在 $3^{\text {rd }}$ 和 $5^{\text {th }}$ 谐波上的 12 dB 抑制
- 小型封装： $15 \mathrm{~mm} \times 9 \mathrm{~mm}$ ， $135-\mathrm{BGA}$
- 工作温度范围：$-40^{\circ} \mathrm{C}$ 至 $85^{\circ} \mathrm{C}$

2 应用

- 医疗超声波成像
- 无损检测设备
- 声纳应用
- 多通道高速数据采集


## 3 说明

AFE5812 是一套高度集成的模拟前端（AFE）解决方案，专用于需要高性能和小尺寸的超声波系统。
AFE5812 集成了完整的时间增益控制（TGC）成像路径和连续波多普勒（CWD）路径。借助该器件，用户还可以选择不同的功率／噪声组合来优化系统性能。因此，AFE5812 对于高端系统及便携式系统都是非常理想的超声波 AFE 解决方案。

| 器件信息 ${ }^{(1)}$ |  |  |
| :---: | :---: | :---: |
| 器件型号 | 封装 | 封装尺寸（标称值） |
| AFE5812 | NFBGA（135） | $15.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |

（1）要了解所有可用封装，请见数据表末尾的可订购产品附录。

## 4 简化图表



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## 5 修订历史记录

Changes from Original（March 2015）to Revision A Page
－将器件状态从产品预览更改为量产数据 ..... 1

## 6 器件比较表

| 部件号 | 部件说明 | 封装 | 封装尺寸（标称值） |
| :---: | :---: | :---: | :---: |
| AFE5818，SBAS687 | 具有 $124 \mathrm{~mW} /$ 通道功耗， $0.75 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$ 噪声， 14 位 65MSPS 或 12 位 80MSPS ADC以及 CW 无源混频器的 16 通道超声波模拟前端 | NFBGA（289） | $15.00 \mathrm{~mm} \times 15.00 \mathrm{~mm}$ |
| AFE5816，SBAS688 | 具有 54 mW ／通道功耗， $1.3 \mathrm{nV} / \mathrm{JHz}$ 噪声， 14 位 65 MSPS 或 12 位 80MSPS ADC以及 CW 无源混频器的 16 通道超声波模拟前端 | NFBGA（289） | $15.00 \mathrm{~mm} \times 15.00 \mathrm{~mm}$ |
| AFE5809，SLOS738 | 具有 CW 无源混频器以及数字 I／Q 解调器的 $0.75 \mathrm{nV} / \mathrm{rtHz}$ ， $14 / 12$ 位，65MSPS， $158 \mathrm{~mW} /$ 通道的 8 通道超声波模拟前端 | NFBGA（135） | $15.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |
| AFE5808A，SLOS729 | 具有 CW 无源混频器的， $0.75 \mathrm{nV} / \mathrm{rtHz}, ~ 14 / 12$ 位， $65 \mathrm{MSPS}, ~ 158 \mathrm{~mW} /$ 通道的 8 通道超声波模拟前端 | NFBGA（135） | $15.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |
| AFE5807，SLOS703 | 具有 CW 无源混频器， $1.05 \mathrm{nV} / \mathrm{rtHz}, ~ 12$ 位， $80 \mathrm{MSPS}, ~ 117 \mathrm{~mW} /$ 通道的 8 通道超声波模拟前端 | NFBGA（135） | $15.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |
| AFE5803，SLOS763 | $0.75 \mathrm{nV} / \mathrm{rtHz}, ~ 14 / 12$ 位，65MSPS，158mW／通道的 8 通道超声波模拟前端 | NFBGA（135） | $15.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |
| AFE5805，SBOS421 | $0.85 \mathrm{nV} / \mathrm{rtHz}, ~ 12$ 位，50MSPS，122mW／通道的 8 通道超声波模拟前端 | NFBGA（135） | $15.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |
| AFE5804，SBOS442 | $1.23 \mathrm{nV} / \mathrm{rtHz}, ~ 12$ 位，50MSPS，101mW／通道的 8 通道超声波模拟前端 | NFBGA（135） | $15.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |
| AFE5801，SLOS591 | 具有八路高速 ADC 的 $5.5 \mathrm{nV} / \mathrm{rtHz}, ~ 12$ 位，65MSPS，65mW／通道 8 通道可变增益放大器（VGA） | QFN（64） | $9.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |
| AFE5851，SLOS574 | 具有高速 ADC 的 $5.5 \mathrm{nV} / \mathrm{rtHz}, ~ 12$ 位， $32.5 \mathrm{MSPS}, ~ 39 \mathrm{~mW} /$ 通道 16 通道可变增益放大器（VGA） | QFN（64） | $9.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |
| VCA5807，SLOS727 | 具有 CW 无源混频器的 $0.75 \mathrm{nV} / \mathrm{rtHz}, ~ 99 \mathrm{~mW} /$ 通道 8 通道电压控制放大器 | TQFP（80） | $14.00 \mathrm{~mm} \times 14.00 \mathrm{~mm}$ |
| VCA8500，SBOS390 | 具有低噪声前置放大器的 $0.8 \mathrm{nV} / \mathrm{rtHz}, ~ 65 \mathrm{~mW} /$ 通道 8 通道超低功耗可变增益放大器 | QFN（64） | $9.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |
| ADS5294，SLAS776 | 75 dBFS SNR，77mW／通道八通道 14 位 80MSPS ADC | TQFP（80） | $14.00 \mathrm{~mm} \times 14.00 \mathrm{~mm}$ |
| ADS5292，SLAS788 | 70dBFS SNR，66mW／通道的八通道 12 位 80MSPS ADC | TQFP（80） | $14.00 \mathrm{~mm} \times 14.00 \mathrm{~mm}$ |
| ADS5295，SBAS595 | 70.6 dBFS SNR，80mW／通道的八通道 12 位 100MSPS ADC | TQFP（80） | $14.00 \mathrm{~mm} \times 14.00 \mathrm{~mm}$ |
| ADS5296A，SBAS631 | 10 位，200MSPS，61dBFS SNR，150mW／通道的 4 通道ADC 以及 12 位 80MSPS，70dBFS SNR，65mW／通道的 8 通道 ADC | QFN（64） | $9.00 \mathrm{~mm} \times 9.00 \mathrm{~mm}$ |

7 说明（续）
AFE5812 包含八个具有电压控制放大器（VCA），14 和 12 位 ADC 以及 CW 混频器的通道。VCA 包括
LNA，VCAT，PGA 和 LPF。LNA 增益可以编程，以支持 $250 \mathrm{mV} V_{P P}$ 至 $0.75 \mathrm{~V}_{\mathrm{PP}}$ 的输入信号。 LNA 还支持可编程有源终端。超低噪声 VCAT 提供 40dB 衰减控制范围，可改善整体低增益 SNR，有利于谐波成像和近场成像。 PGA 提供 24 和 30 dB 增益选项。在 ADC 前，可配置 $10 \mathrm{MHz}, ~ 15 \mathrm{MHz}, ~ 20 \mathrm{MHz}, ~ 30 \mathrm{MHz}, ~ 35 \mathrm{MHz}$ 或 50 MHz LPF 来支持不同频率的各种超声波应用。此外，AFE5812 的信号链可以处理频率低于 100 kHz 的信号，因此 AFE5812 适用于声纳和医疗应用。AFE5812的高性能 14 位／65MSPS ADC 可实现 77dBFS SNR。它确保了低链路增益下的出色 SNR。ADC 的 LVDS 输出可实现小型化系统所需的灵活系统集成。

AFE5812 集成了一个低功耗无源混频器和一个低噪声混合放大器，用以生成片上 CWD 波束形成器。16 个可选相位延迟可应用于每个模拟输入信号。同时，器件采用独特的三阶和五阶谐波抑制滤波器来增强 CW 灵敏度。
AFE5812 还包括一个数字同相正交（I／Q）解调器和一个低通抽取滤波器。解调块的主要用途是降低 LVDS 数据传输速率并提升系统总体功率效率。I／Q 解调器可接受高达 65MSPS 采样率和 14 位分辨率的 ADC 输出。例如，当数字解调和 4 倍抽取滤波完成后，同相或正交输出的数据速率降至 16．25MSPS，数据分辨率相应提高到 16 位。因此，总体 LVDS 激励衰减系数可以为 2 。这个解调器可被旁通，如果需要的话，也可将其完全断电。
AFE5812 采用 $15 \mathrm{~mm} \times 9 \mathrm{~mm}, ~ 135$ 引脚的 BGA 封装，额定工作温度范围为 $-40^{\circ} \mathrm{C}$ 至 $85^{\circ} \mathrm{C}$ 。

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## 8 Pin Configuration and Functions

Table 1. ZCF (BGA-135) Top View

|  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | $\mathbf{6}$ | $\mathbf{7}$ | $\mathbf{8}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | AVDD | INP8 | INP7 | INP6 | INP5 | INP4 | INP3 | INP2 |  |
| B | CM_BYP | ACT8 | ACT7 | ACT6 | ACT5 | ACT4 | ACT3 | ACT2 |  |
| C | AVSS | INM8 | INM7 | INM6 | INM5 | INM4 | INM3 | ACT1 |  |
| D | AVSS | AVSS | AVSS | AVSS | AVSS | AVSS | AVSS | INM2 |  |
| E | CW_IP_AMPINP | CW_IP_AMPINM | AVSS | AVSS | AVSS | AVSS | AVSS | INM1 |  |
| F | CW_IP_OUTM | CW_IP_OUTP | AVSS | AVSS | AVSS | AVSS | AVSS | CLKP_16X | CLKM_16X |
| G | AVSS | AVSS | AVSS/DTGC_S | AVSS | AVSS | AVSS | AVSS | CLKP_1X | CLKM_1X |
| H | CW_QP_OUTM | CW_QP_OUTP | AVSS | AVSS | AVSS | AVSS | AVSS | PDN_GLOBAL | RESET |
| J | CW_QP_AMPINP | CW_QP_AMPINM | AVSS | AVSS | AVSS | AVDD_ADC | AVDD_ADC | PDN_VCA | SCLK |
| K | AVDD | AVDD_5V | VCNTLP | VCNTLM | VHIGH | AVSS | DNC | AVDD_ADC | SDATA |
| L | CLKP_ADC | CLKM_ADC | AVDD_ADC | REFM | DNC | LDO_EN | TX_SYNC_IN | PDN_ADC | SEN |
| M | AVDD_ADC | AVDD_ADC | VREF_IN | REFP | DNC | LDO_SETV | SPI_DIG_EN | DNC | SDOUT |
| N | D8P | D8M | DVDD | DVDD_LDO1 | DVSS | DVDD_LDO2 | DVDD | D1M | D1P |
| P | D7M | D6M | D5M | FCLKM | DVSS | DCLKM | D4M | D3M | D2M |
| R | D7P | D6P | D5P | FCLKP | DVSS | DCLKP | D4P | D3P | D2P |

Pin Functions

| PIN |  | DESCRIPTION |
| :---: | :---: | :---: |
| NAME | NO. |  |
| ACT1 to ACT8 | B9 to B2 | Active termination input pins for CH 1 to CH 8 . Bias voltage $=1.5 \mathrm{~V}$ |
| AVDD | A1 | 3.3-V analog supply for LNA, VCAT, PGA, LPF, and CWD blocks |
|  | D8 |  |
|  | D9 |  |
|  | E8 |  |
|  | E9 |  |
|  | K1 |  |
| AVDD_5V | K2 | 5-V analog supply for LNA, VCAT, PGA, LPF, and CWD blocks |
| AVDD_ADC | J6 | 1.8-V analog power supply for ADC |
|  | J7 |  |
|  | K8 |  |
|  | L3 |  |
|  | M1 |  |
|  | M2 |  |
| AVSS | C1 | Analog ground |
|  | D1 to D7 |  |
|  | E3 to E7 |  |
|  | F3 to F7 |  |
|  | G1 to G2 |  |
|  | G4 to G7 |  |
|  | H3 to H7 |  |
|  | J3 to J5 |  |
|  | K6 |  |
| AVSS/DTGC_SW | G3 | Analog ground; or external control pin to switch from ATGC to DTGC. Active high to enable the DTGC mode. Pull down to GND with $20 \mathrm{k} \Omega$. This pin is equivalent to VCA Reg 0x3B[7], DIG_TGC_ATT and图 64. Tie to AVSS if not used. Note: this feature is ensured by design and characterization; NOT production tested. |
| CLKM_ADC | L2 | Negative input of differential ADC clock. In the single-end clock mode, it can be tied to GND directly or through a $0.1-\mu \mathrm{F}$ capacitor. Bias voltage $=1 \mathrm{~V}$ |

## Pin Functions (continued)

| PIN |  | DESCRIPTION |
| :---: | :---: | :---: |
| NAME | NO. |  |
| CLKP_ADC | L1 | Positive input of differential ADC clock. In the single-end clock mode, it can be tied to clock signal directly or through a $0.1-\mu \mathrm{F}$ capacitor. Bias voltage $=1 \mathrm{~V}$ |
| CLKM_16X | F9 | Negative input of differential CW $16 \times$ clock. Tie to GND when the CMOS clock mode is enabled. In the $4 \times$ and $8 \times$ CW clock modes, this pin becomes the $4 \times$ or $8 \times$ CLKM input. In the $1 \times$ CW clock mode, this pin becomes the in-phase $1 \times$ CLKM for the CW mixer. Can be floated if CW mode is not used. See register $0 \times 36[11: 10]$. Bias voltage $=2.5 \mathrm{~V}$ |
| CLKP_16X | F8 | Positive input of differential CW $16 \times$ clock. In $4 \times$ and $8 \times$ clock modes, this pin becomes the $4 \times$ and $8 \times$ CLKP input. In the $1 \times$ CW clock mode, this pin becomes the in-phase $1 \times$ CLKP for the CW mixer. Can be floated if CW mode is not used. See register $0 \times 36[11: 10]$. Bias voltage $=2.5 \mathrm{~V}$ |
| CLKM_1X | G9 | Negative input of differential CW $1 \times$ clock. Tie to GND when the CMOS clock mode is enabled (refer to图 107 for details). In the $1 \times$ clock mode, this pin is the quadrature-phase $1 \times$ CLKM for the CW mixer. Can be floated if CW mode is not used. Bias voltage $=2.5 \mathrm{~V}$ |
| CLKP_1X | G8 | Positive input of differential CW $1 \times$ clock. In the $1 \times$ clock mode, this pin is the quadrature-phase $1 \times$ CLKP for the CW mixer. Can be floated if CW mode is not used. Bias voltage $=2.5 \mathrm{~V}$ |
| CM_BYP | B1 | Bias voltage and bypass to ground. TI recommends $1 \mu \mathrm{~F}$. To suppress the ultra-low frequency noise, the designer can use $10 \mu \mathrm{~F}$. Bias voltage $=1.5 \mathrm{~V}$ |
| CW_IP_AMPINM | E2 | Negative differential input of the in-phase summing amplifier. External LPF capacitor must be connected between CW_IP_AMPINM and CW_IP_OUTP. This pin provides the current output for the CW mixer. This pin becomes the CH7 PGA negative output when PGA test mode is enabled. Can be floated if not used. Bias voltage $=1.5 \mathrm{~V}$ |
| CW_IP_AMPINP | E1 | Positive differential input of the in-phase summing amplifier. External LPF capacitor must be connected between CW_IP_AMPINP and CW_IP_OUTM. This pin provides the current output for the CW mixer. This pin becomes the CH7 PGA positive output when PGA test mode is enabled. Can be floated if not used. Bias voltage $=1.5 \mathrm{~V}$ |
| CW_IP_OUTM | F1 | Negative differential output for the in-phase summing amplifier. External LPF capacitor must be connected between CW_IP_AMPINP and CW_IP_OUTPM. Can be floated if not used. Bias voltage = 1.5 V |
| CW_IP_OUTP | F2 | Positive differential output for the in-phase summing amplifier. External LPF capacitor must be connected between CW_IP_AMPINM and CW_IP_OUTP. Can be floated if not used. Bias voltage $=1.5$ V |
| CW_QP_AMPINM | J2 | Negative differential input of the quadrature-phase summing amplifier. External LPF capacitor must be connected between CW_QP_AMPINM and CW_QP_OUTP. This pin provides the current output for the CW mixer. This pin becomes CH8 PGA negative output when PGA test mode is enabled. Can be floated if not used. Bias voltage $=1.5 \mathrm{~V}$ |
| CW_QP_AMPINP | J1 | Positive differential input of the quadrature-phase summing amplifier. External LPF capacitor must be connected between CW_QP_AMPINP and CW_QP_OUTM. This pin provides the current output for the CW mixer. This pin becomes CH8 PGA positive output when PGA test mode is enabled. Can be floated if not used. Bias voltage $=1.5 \mathrm{~V}$ |
| CW_QP_OUTM | H1 | Negative differential output for the quadrature-phase summing amplifier. External LPF capacitor must be connected between CW_QP_AMPINP and CW_QP_OUTM. Can be floated if not used. Bias voltage = 1.5 V |
| CW_QP_OUTP | H2 | Positive differential output for the quadrature-phase summing amplifier. External LPF capacitor must be connected between CW_QP_AMPINM and CW_QP_OUTP. Can be floated if not used. Bias voltage = 1.5 V |
| D1M to D8M | N8 | ADC CH1 to CH8 LVDS negative data outputs |
|  | P9 to P7 |  |
|  | P3 to P1 |  |
|  | N2 |  |
| D1P to D8P | N9 | ADC CH1 to 8 LVDS positive data outputs |
|  | R9 to R7 |  |
|  | R3 to R1 |  |
|  | N1 |  |
| DCLKM | P6 | LVDS bit clock (7x in 14bit resolution) negative output |
| DCLKP | R6 | LVDS bit clock ( $7 x$ in 14bit resolution) positive output |
| DVDD | N3 | ADC digital and I/O power supply, 1.8 V |
|  | N7 |  |

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Pin Functions (continued)

| PIN |  | DESCRIPTION |
| :---: | :---: | :---: |
| NAME | NO. |  |
| DVSS | N5 | ADC digital ground |
|  | P5 |  |
|  | R5 |  |
| DVDD LDO1, DVDD_LDO2 | N4 | In the internal LDO mode, i.e. LDO_EN=1, these two pins should be separated on PCB and decoupled respectively. Internal LDO output will drive this PIN to 1.2 V or 1.4 V depending on LDO_SETV. In the external LDO mode,i.e. LDO_EN=0 or floating, lower demod power is achieved than the internal LDO mode. $1.4 \mathrm{~V} \sim 1.5 \mathrm{~V}$ should be applied when ADC sampling rate is high, e.g. 50~65MSPS. Demod SPI requires DVDD_LDO1/2. |
|  | N6 |  |
| FCLKM | P4 | LVDS frame clock (1x) negative output |
| FCLKP | R4 | LVDS frame clock (1×) positive output |
| INM1 to INM8 | C9 to C2 | CH 1 to CH 8 complementary analog inputs. Bypass to ground with $\geq 0.015-\mu \mathrm{F}$ capacitors. The HPF response of the LNA depends on the capacitors. Bias voltage $=2.2 \mathrm{~V}$ |
| INP1 to INP8 | A9 to A2 | CH 1 to CH 8 analog inputs. AC couple to inputs with $\geq 0.1-\mu \mathrm{F}$ capacitors. Bias voltage $=2.2 \mathrm{~V}$ |
| LDO_EN | L6 | Enable/Disable AFE's internal LDO regulators. When it is tied to 1.8-V DVDD or Logic "1", AFE's internal LDO is enabled. When it is tied to DVSS or Logic "0", AFE's internal LDO is disabled and external 1.4 V supply can be applied at N4 and N6 pins, i.e. DVDD_LDO1, DVDD_LDO2. Default is pulled down internally through a $150 \mathrm{~K} \Omega$ resistor with input capacitance of 5 pF . Either 1.8 V or 3.3 V logic level can be used. |
| LDO_SETV | M6 | Sets the internal LDO voltage. ' 0 ' is 1.2 V ; ' 1 ' is 1.4 V . Default is pulled down internally through a $150 \mathrm{~K} \Omega$ resistor with input capacitance of 5 pF . Either 1.8 V or 3.3 V logic level can be used. Please note: some voltage drop exists on chip; therefore the measured DVDD_LDO voltage is slightly lower than the sepcified ones. |
| PDN_ADC | L8 | ADC partial (fast) power-down control pin with an internal pulldown resistor of $100 \mathrm{k} \Omega$. Active high. Either 1.8-V or 3.3-V logic level can be used. |
| PDN_VCA | J8 | VCA partial (fast) power-down control pin with an internal pulldown resistor of $20 \mathrm{k} \Omega$. Active high. 3.3-V logic level should be used. |
| PDN_GLOBAL | H8 | Global (complete) power-down control pin for the entire chip with an internal pulldown resistor of $20 \mathrm{k} \Omega$. Active high. 3.3-V logic level should be used. When the complete power-down mode is enabled, the digital demodulator may lose register settings. Therefore, it is required to reconfigure the demodulator registers, filter coefficient memory, and profile memory after existing the complete power-down mode. |
| REFM | L4 | $0.5-\mathrm{V}$ reference output in the internal reference mode. Must leave floated in the internal reference mode. TI recommends adding a test point on the PCB for monitoring the reference output |
| REFP | M4 | $1.5-\mathrm{V}$ reference output in the internal reference mode. Must leave floated in the internal reference mode. TI recommends adding a test point on the PCB for monitoring the reference output |
| RESET | H9 | Hardware reset pin with an internal pulldown resistor of $20 \mathrm{k} \Omega$. Active high. The designer can use 3.3-V logic level. |
| SCLK | J9 | Serial interface clock input with an internal pulldown resistor of $20 \mathrm{k} \Omega$. This pin is connected to both ADC and VCA. The designer should use 3.3-V logic. |
| SDATA | K9 | Serial interface data input with an internal pulldown resistor of $20 \mathrm{k} \Omega$. This pin is connected to both ADC and VCA. The designer should use 3.3-V logic. |
| SDOUT | M9 | Serial interface data readout. High impedance when readout is disabled. This pin is connected to ADC only. The designer can use $1.8-\mathrm{V}$ logic. |
| SEN | L9 | Serial interface enable with an internal pullup resistor of $20 \mathrm{k} \Omega$. Active low. This pin is connected to both ADC and VCA. The designer should use 3.3-V logic. |
| SPI_DIG_EN | M7 | Serial interface enable for the digital demodulator memory space. SPI_DIG_EN pin is required to be set to 0 during SPI transactions to demodulator registers. Each transaction starts by setting SEN as 0 and terminates by setting it back to 1 (similar to other register transactions). Pull up internally through a 20$\mathrm{k} \Omega$ resistor. This pin is connected to both ADC and VCA. The designer should use 3.3-V logic. |
| TX_SYNC_IN | L7 | System trig signal input. It indicates the start of signal transmission. Either 3.3-V or 1.8-V logic level can be used. Note: TX_SYNC signal must be synchronized with ADC CLK. Typically, pulse repetition frequency (PRF) signal can be used for TX_SYNC_IN. |
| VCNTLM | K4 | Negative differential attenuation control pin |
| VCNTLP | K3 | Positive differential attenuation control pin |
| VHIGH | K5 | Bias voltage; bypass to ground with $\geq 1 \mu \mathrm{~F}$. Bias voltage $=1 \mathrm{~V}$ |

## Pin Functions (continued)

| PIN |  | DESCRIPTION |
| :---: | :---: | :---: |
| NAME | NO. |  |
| VREF_IN | M3 | ADC 1.4-V reference input in the external reference mode; bypass to ground with $0.1 \mu \mathrm{~F}$. |
| DNC | L5 | Do not connect. Must leave floated |
|  | K7 |  |
|  | M5 |  |
|  | M8 |  |

## 9 Specifications

### 9.1 Absolute Maximum Ratings

over operating free-air temperature (unless otherwise noted) ${ }^{(1)}$

|  |  | MIN | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: |
|  | AVDD | -0.3 | 3.9 | V |
|  | AVDD_ADC | -0.3 | 2.2 | V |
| Supply voltage | AVDD_5V | -0.3 | 6 | V |
|  | DVDD | -0.3 | 2.2 | V |
|  | DVDD_LDO | -0.3 | 1.6 | V |
| Voltage betwee | and LVSS | -0.3 | 0.3 | V |
| Voltage at CLKM | , CLKP_ADC ${ }^{(2)}$ | -0.3 | min[2.2, AVDD_ADC+0.3] | V |
| Voltage at CLKM | CLKP_16X, CLKM_1X, and CLKP_1X ${ }^{(2)}$ | -0.3 | $\min [5.5 \mathrm{~V}, \mathrm{AVDD}$ _5V+0.3] | V |
| Voltage at anal | s and digital inputs | -0.3 | $\min [3.6$, AVDD + 0.3] | V |
| Voltage at digita |  | -0.3 | min[2.2, DVDD +0.3 ] | V |
| Peak solder tem | $\mathrm{e}^{(3)}$ |  | 260 | ${ }^{\circ} \mathrm{C}$ |
| Maximum junctio | perature ( $\mathrm{T}_{\mathrm{J}}$ ), any condition |  | 105 | ${ }^{\circ} \mathrm{C}$ |
| Operating temp |  | -40 | 85 | ${ }^{\circ} \mathrm{C}$ |
| Storage temper |  | -55 | 150 | ${ }^{\circ} \mathrm{C}$ |

(1) Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions is not implied Exposure to absolute maximum rated conditions for extended periods may degrade device reliability.
(2) When AVDD_ADC or AVDD_5V is turned off, TI recommends to switch off the input clock (or ensure the voltage on CLKP_ADC, CLKM_ADC is $<|0.3 V|)$. This prevents the ESD protection diodes at the clock input pins from turning on. CLKM/P_16X and CLKM/P_1X CLKs should follow the similar recommendations as well.
(3) Device complies with JSTD-020D.

### 9.2 ESD Ratings

| V $_{(\text {(ESD })}$ |  | Electrostatic <br> discharge | Human body model (HBM), per ANSI/ESDA/JEDEC JS-001 ${ }^{(1)}$ | VALUE |
| :--- | :--- | :--- | :---: | :---: |
|  | Charged device model (CDM), per JEDEC specification JESD22-C101 ${ }^{(2)}$ | $\pm 1000$ | UNIT |  |

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 9.3 Recommended Operating Conditions

|  | MIN | MAX |
| :--- | :---: | :---: |
| UNIT |  |  |
| AVDD | 3.15 |  |
| AVDD_ADC | 3.6 | V |
| DVDD | 1.7 |  |
| DVDD_LDO1/2 (External LDO mode) | 1.9 | V |
| AVDD_5V | 1.7 |  |
| $T_{\text {A }}$ Ambient temperature | 1.9 | V |

### 9.4 Thermal Information

| THERMAL METRIC ${ }^{(1)}$ | AFE5812 | UNIT |
| :---: | :---: | :---: |
|  | BGA |  |
|  | 135 PINS |  |
| $\mathrm{R}_{\theta \mathrm{JA}}$ Junction-to-ambient thermal resistance | 34.1 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\theta \mathrm{JC} \text { (top) }}$ Junction-to-case (top) thermal resistance | 5 |  |
| $\mathrm{R}_{\theta \mathrm{JB}}$ Junction-to-board thermal resistance | 11.5 |  |
| $\Psi_{\text {JT }} \quad$ Junction-to-top characterization parameter | 0.2 |  |
| $\Psi_{\text {JB }} \quad$ Junction-to-board characterization parameter | 10.8 |  |
| $\mathrm{R}_{\text {өJC(bot) }}$ ( Junction-to-case (bottom) thermal resistance | N/A |  |

(1) For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, SPRA953.

### 9.5 Electrical Characteristics

AVDD_5V = $5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$, DVDD $=1.8 \mathrm{~V}$, AC-coupled with $0.1 \mu \mathrm{~F}$ at INP and bypassed to ground with 15 nF at INM, No active termination, $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, f_{I N}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit, sample rate $=65$ MSPS, LPF Filter $=15 \mathrm{MHz}$, low-noise mode, $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$, Single-ended $\mathrm{V}_{\text {CNTL }}$ mode, VCNTLM = GND, ADC configured in internal reference mode, internal $500-\Omega \mathrm{CW}$ feedback resistor, CMOS CW clocks, at ambient temperature, $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, Digital demodulator is disabled unless otherwise noted. Min and max values are specified across full-temperature range with AVDD_5 V = 5 V, AVDD $=3.3 \mathrm{~V}, \mathrm{AVDD} \mathrm{\_ADC}=1.8 \mathrm{~V}$, $\mathrm{DVDD}=1.8 \mathrm{~V}$.

| PARAMETER |  | TEST CONDITIONS | MIN TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TGC FULL SIGNAL CHANNEL (LNA + VCAT + LPF + ADC) |  |  |  |  |  |
| en (RTI) | Input voltage noise over LNA gain (lownoise mode) | Rs $=0 \Omega, f=2 \mathrm{MHz}, \mathrm{LNA}=24,18,15 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}$ | 0.76, 0.83, 1.16 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
|  |  | Rs $=0 \Omega, f=2 \mathrm{MHz}, \mathrm{LNA}=24,18,15 \mathrm{~dB}, \mathrm{PGA}=30 \mathrm{~dB}$ | 0.75, 0.86, 1.12 |  |  |
|  | Input voltage noise over LNA gain (lowpower mode) | Rs $=0 \Omega, f=2 \mathrm{MHz}, \mathrm{LNA}=24,18,15 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}$ | 1.1, 1.2, 1.45 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
|  |  | Rs $=0 \Omega, f=2 \mathrm{MHz}, \mathrm{LNA}=24,18,15 \mathrm{~dB}, \mathrm{PGA}=30 \mathrm{~dB}$ | 1.1, 1.2, 1.45 |  |  |
|  | Input voltage noise over LNA gain (medium-power mode) | Rs $=0 \Omega, f=2 \mathrm{MHz}, \mathrm{LNA}=24,18,15 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}$ | 1, 1.05, 1.25 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
|  |  | Rs $=0 \Omega, f=2 \mathrm{MHz}, \mathrm{LNA}=24,18,15 \mathrm{~dB}, \mathrm{PGA}=30 \mathrm{~dB}$ | 0.95, 1, 1.2 |  |  |
| en (RTI) | Input voltage noise at low frequency | $f=100 \mathrm{kHz}$, INM capacitor $=1 \mu \mathrm{~F}$, PGA integrator disabled | 0.9 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
|  | Input referred current noise | Low-noise mode/medium-power mode/low-power mode | 2.7, 2.1, 2 |  | $\mathrm{pA} / \mathrm{rtHz}$ |
| NF | Noise figure | Rs $=200 \Omega, 200-\Omega$ active termination, PGA $=24 \mathrm{~dB}, \mathrm{LNA}=15,18,24 \mathrm{~dB}$ | 3.85, 2.4, 1.8 |  | dB |
|  |  | Rs $=100 \Omega, 100-\Omega$ active termination, PGA $=24 \mathrm{~dB}, \mathrm{LNA}=15,18,24 \mathrm{~dB}$ | 5.3, 3.1, 2.3 |  | dB |
| NF | Noise figure | Rs $=500 \Omega, 1 \mathrm{k} \Omega$, no termination, low-NF mode is enabled (Reg53[9] = 1) | 1.08, 0.94 |  | dB |
| NF | Noise figure | Rs $=50 \Omega / 200 \Omega$, no termination, low-noise mode (Reg53[9] = 0) | 2.35, 1.05 |  | dB |
| $\mathrm{V}_{\text {MAX }}$ | Maximum linear input voltage | LNA gain $=24,18,15 \mathrm{~dB}$ | 250, 500, 700 |  | mVpp |
| $\mathrm{V}_{\text {CLAMP }}$ | Clamp voltage | Reg52[10:9] $=0, \mathrm{LNA}=24,18,15 \mathrm{~dB}$ | 350, 600, 825 |  |  |
|  | PGA gain | Low-noise mode | 24, 30 |  | dB |
|  |  | Medium-power/low-power mode | 24, 28.5 |  |  |
|  | Total gain | LNA $=24 \mathrm{~dB}, \mathrm{PGA}=30 \mathrm{~dB}$, low-noise mode | 54 |  | dB |
|  |  | LNA $=24 \mathrm{~dB}, \mathrm{PGA}=30 \mathrm{~dB}$, medium-power mode | 52.5 |  |  |
|  |  | LNA $=24 \mathrm{~dB}, \mathrm{PGA}=30 \mathrm{~dB}$, low-power mode | 52.5 |  |  |
|  | Ch-CH noise correlation factor without signal ${ }^{(1)}$ | Summing of 8 channels | 0 |  |  |
|  | Ch-CH noise correlation factor with signal ${ }^{(1)}$ | Full band ( $\mathrm{V}_{\text {CNTL }}=0,0.8$ ) | 0.15, 0.17 |  |  |
|  |  | $1-\mathrm{MHz}$ band over carrier ( $\left.\mathrm{V}_{\text {CNTL }}=0,0.8\right)$ | 0.18, 0.75 |  |  |
|  | Signal-to-noise ratio (SNR) | $\mathrm{V}_{\text {CNTL }}=0.6 \mathrm{~V}$ (22-dB total channel gain) | 68 70 |  | dBFS |
|  |  | $\mathrm{V}_{\text {CNTL }}=0, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}$ | 58.3 63 |  |  |
|  |  | $\mathrm{V}_{\text {CNTL }}=0, \mathrm{LNA}=24 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}$ | 58 |  |  |
|  | Narrow-band SNR | SNR over 2-MHz band around carrier at $\mathrm{V}_{\text {CNTL }}=0.6 \mathrm{~V}$ (22-dB total gain) | $75 \quad 77$ |  | dBFS |
|  | Input common-mode voltage | At INP and INM pins | 2.2 |  | V |
|  | Input resistance |  | 8 |  | k $\Omega$ |
|  |  | Preset active termination enabled | 50,100,200,400 |  | $\Omega$ |
|  | Input capacitance |  | 20 |  | pF |
|  | Input control voltage | $\mathrm{V}_{\text {CNTLP }}-\mathrm{V}_{\text {CNTLM }}$ | 0 | 1.5 | V |
|  | Common-mode voltage | $\mathrm{V}_{\text {CNTLP }}$ and $\mathrm{V}_{\text {CNTLM }}$ | 0.75 |  | V |
|  | Gain range |  | -40 |  | dB |
|  | Gain slope | $\mathrm{V}_{\text {CNTL }}=0.1$ to 1.1 V | 35 |  | dB/V |
|  | Input resistance | Between $\mathrm{V}_{\text {CNTLP }}$ and $\mathrm{V}_{\text {CNTLM }}$ | 200 |  | k $\Omega$ |
|  | Input capacitance | Between $\mathrm{V}_{\text {CNTLP }}$ and $\mathrm{V}_{\text {CNTLM }}$ | 1 |  | pF |
|  | TGC response time | $\mathrm{V}_{\text {CNTL }}=0-$ to $1.5-\mathrm{V}$ step function | 1.5 |  | $\mu \mathrm{s}$ |
|  | Third-order LPF |  | $\begin{array}{r} \hline 10,15,20,30, \\ 35,50 \\ \hline \end{array}$ |  | MHz |
|  | Settling time for change in LNA gain |  | 14 |  | $\mu \mathrm{s}$ |
|  | Settling time for change in active termination setting |  | 1 |  | $\mu \mathrm{s}$ |

(1) Noise correlation factor is defined as $\mathrm{Nc} /(\mathrm{Nu}+\mathrm{Nc})$, where Nc is the correlated noise power in single channel; and Nu is the uncorrelated noise power in single channel. Its measurement follows the below equation, in which the SNR of single-channel signal and the SNR of summed eight-channel signal are measured.
$\frac{\mathrm{N}_{\mathrm{C}}}{\mathrm{Nu}+\mathrm{N}_{\mathrm{C}}}=\frac{10-\frac{8 \mathrm{CH} \mathrm{C}_{2} \mathrm{SNR}}{10}}{-\frac{1 \mathrm{CH} \text { _SNR }}{10}} \times \frac{1}{56}-\frac{1}{7}$

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## Electrical Characteristics（接下页）

AVDD＿5V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}$, AVDD＿ADC $=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ，AC－coupled with $0.1 \mu \mathrm{~F}$ at INP and bypassed to ground with 15 nF at INM，No active termination， $\mathrm{V}_{\text {CNTL }}=0 \mathrm{~V}, f_{\mathrm{IN}}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF Filter $=15 \mathrm{MHz}$ ，low－noise mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ ，Single－ended $\mathrm{V}_{\text {CNTL }}$ mode，VCNTLM $=$ GND，ADC configured in internal reference mode，internal $500-\Omega \mathrm{CW}$ feedback resistor，CMOS CW clocks，at ambient temperature， $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ， Digital demodulator is disabled unless otherwise noted．Min and max values are specified across full－temperature range with AVDD＿5 V $=5 \mathrm{~V}$, AVDD $=3.3 \mathrm{~V}$, AVDD＿ADC $=1.8 \mathrm{~V}, \mathrm{DVDD}=1.8 \mathrm{~V}$ ．

| PARAMETER | TEST CONDITIONS | MIN TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: |
| AC ACCURACY |  |  |  |  |
| LPF bandwidth tolerance |  | $\pm 5 \%$ |  |  |
| $\mathrm{CH}-\mathrm{CH}$ group delay variation | 2 to 15 MHz | 2 |  | ns |
| $\mathrm{CH}-\mathrm{CH}$ phase variation | $15-\mathrm{MHz}$ signal | 11 |  | 。 |
| Gain matching | $0 \mathrm{~V}<\mathrm{V}_{\text {CNTL }}<0.1 \mathrm{~V}$（Dev－to－Dev） | $\pm 0.5$ |  | dB |
|  | $0.1 \mathrm{~V}<\mathrm{V}_{\text {CNTL }}<1.1 \mathrm{~V}$（Dev－to－Dev） | －1．1 $\pm 0.5$ | 1.1 |  |
|  | $1.1 \mathrm{~V}<\mathrm{V}_{\text {CNTL }}<1.5 \mathrm{~V}$（Dev－to－Dev） | $\pm 0.5$ |  |  |
| Gain matching | Channel－to－channel | $\pm 0.25$ |  | dB |
| Output offset | $\mathrm{V}_{\text {CNTL }}=0, \mathrm{PGA}=24 \mathrm{~dB}, \mathrm{LNA}=18 \mathrm{~dB}$ | －100 | 100 | LSB |
| AC PERFORMANCE |  |  |  |  |
| HD2 Second－harmonic distortion | $\mathrm{F}_{\text {IN }}=2 \mathrm{MHz} ; \mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ | －60 |  | dBc |
|  | $\mathrm{F}_{\text {IN }}=5 \mathrm{MHz} ; \mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ | －60 |  |  |
|  | $\begin{aligned} & \mathrm{F}_{\text {IN }}=5 \mathrm{MHz} ; \mathrm{V}_{\text {IN }}=500 \mathrm{mV}_{\mathrm{PP}}, \\ & \mathrm{~V}_{\text {OUT }}=-1 \mathrm{dBFS}, \text { LNA }=18 \mathrm{~dB}, \mathrm{~V}_{\text {CNTL }}=0.88 \mathrm{~V} \end{aligned}$ | －55 |  |  |
|  | $\begin{aligned} & \mathrm{F}_{\text {IN }}=5 \mathrm{MHz} ; \mathrm{V}_{\text {IN }}=250 \mathrm{mV}_{\text {PP }}, \\ & \mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, \text { LNA }=24 \mathrm{~dB}, \mathrm{~V}_{\text {CNTL }}=0.88 \mathrm{~V} \end{aligned}$ | －55 |  |  |
| HD3 Third－harmonic distortion | $\mathrm{F}_{\text {IN }}=2 \mathrm{MHz} ; \mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ | －50 |  | dBc |
|  | $\mathrm{F}_{\text {IN }}=5 \mathrm{MHz} ; \mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ | －50 |  |  |
|  | $\begin{aligned} & \mathrm{F}_{\text {IN }}=5 \mathrm{MHz} ; \mathrm{V}_{\text {IN }}=500 \mathrm{mV}_{\text {PP }}, \\ & \mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, \text { LNA }=18 \mathrm{~dB}, \mathrm{~V}_{\text {CNTL }}=0.88 \mathrm{~V} \end{aligned}$ | －50 |  |  |
|  | $\begin{aligned} & \mathrm{F}_{\text {IN }}=5 \mathrm{MHz} ; \mathrm{V}_{\text {IN }}=250 \mathrm{mV}_{\mathrm{PP}}, \\ & \mathrm{~V}_{\text {OUT }}=-1 \mathrm{dBFS}, \text { LNA }=24 \mathrm{~dB}, \mathrm{~V}_{\text {CNTL }}=0.88 \mathrm{~V} \end{aligned}$ | －50 |  |  |
| Total harmonic distortion | $\mathrm{F}_{\text {IN }}=2 \mathrm{MHz} ; \mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ | －50 |  | dBc |
|  | $\mathrm{F}_{\text {IN }}=5 \mathrm{MHz} ; \mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ | －50 |  |  |
| IMD3 Intermodulation distortion | $\begin{aligned} & f_{1}=5 \mathrm{MHz} \text { at }-1 \mathrm{dBFS}, \\ & f_{2}=5.01 \mathrm{MHz} \text { at }-27 \mathrm{dBFS} \end{aligned}$ | －60 |  | dBc |
| XTALK Cross－talk | $\mathrm{F}_{\text {IN }}=5 \mathrm{MHz}$ ； $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ | －65 |  | dB |
| Phase noise | kHz off $5 \mathrm{MHz}\left(\mathrm{V}_{\text {CNTL }}=0 \mathrm{~V}\right)$ | －132 |  | $\mathrm{dBc} / \mathrm{Hz}$ |
| LNA |  |  |  |  |
| Input referred voltage noise | Rs $=0 \Omega, f=2 \mathrm{MHz}$ ，Rin $=$ High Z，Gain $=24,18,15 \mathrm{~dB}$ | 0．63，0．70， 0.9 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
| High－pass filter（HPF） | －3 dB cut－off frequency | $\begin{array}{r} \hline 50,100,150, \\ 200 \end{array}$ |  | kHz |
| LNA linear output |  | 4 |  | Vpp |
| VCAT＋PGA |  |  |  |  |
| VCAT input noise | 0－dB，$-40-\mathrm{dB}$ attenuation | 2， 10.5 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
| PGA input noise | $24 \mathrm{~dB}, 30 \mathrm{~dB}$ | 1.75 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
| -3 dB HPF cut－off frequency |  | 80 |  | kHz |

## Electrical Characteristics（接下页）

AVDD＿5V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}$, AVDD＿ADC $=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ，AC－coupled with $0.1 \mu \mathrm{~F}$ at INP and bypassed to ground with 15 nF at INM，No active termination， $\mathrm{V}_{\text {CNTL }}=0 \mathrm{~V}, f_{\mathrm{IN}}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF Filter $=15 \mathrm{MHz}$ ，low－noise mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ ，Single－ended $\mathrm{V}_{\mathrm{CNTL}}$ mode，VCNTLM $=$ GND，ADC configured in internal reference mode，internal $500-\Omega \mathrm{CW}$ feedback resistor，CMOS CW clocks，at ambient temperature， $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ， Digital demodulator is disabled unless otherwise noted．Min and max values are specified across full－temperature range with AVDD＿5 V＝ 5 V, AVDD $=3.3 \mathrm{~V}$, AVDD＿ADC $=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ．

| PARAMETER |  | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CW DOPPLER |  |  |  |  |  |  |
| en（RTI） | Input voltage noise（CW） | 1－channel mixer，LNA $=24 \mathrm{~dB}, 500-\Omega$ feedback resistor |  | 0.8 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
|  |  | 8 －channel mixer，LNA $=24 \mathrm{~dB}, 62.5-\Omega$ feedback resistor |  | 0.33 |  |  |
| en（RTO） | Output voltage noise（CW） | 1－channel mixer，LNA $=24 \mathrm{~dB}, 500-\Omega$ feedback resistor |  | 12 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
|  |  | 8 －channel mixer，LNA $=24 \mathrm{~dB}, 62.5-\Omega$ feedback resistor |  | 5 |  |  |
| en（RTI） | Input voltage noise（CW） | 1－channel mixer，LNA $=18 \mathrm{~dB}, 500-\Omega$ feedback resistor |  | 1.1 |  | nV／rtHz |
|  |  | 8 －channel mixer，LNA $=18 \mathrm{~dB}, 62.5-\Omega$ feedback resistor |  | 0.5 |  |  |
| en（RTO） | Output voltage noise（CW） | 1－channel mixer，LNA $=18 \mathrm{~dB}, 500-\Omega$ feedback resistor |  | 8.1 |  | nV／rtHz |
|  |  | 8 －channel mixer，LNA $=18 \mathrm{~dB}, 62.5-\Omega$ feedback resistor |  | 4.0 |  |  |
| NF | Noise figure | Rs $=100 \Omega, R_{\text {IN }}=$ High $Z, F_{I N}=2 \mathrm{MHz}$（LNA，I／Q mixer and summing amplifier／filter） |  | 1.8 |  | dB |
| $\mathrm{f}_{\mathrm{CW}}$ | CW operation range ${ }^{(2)}$ | CW signal carrier frequency |  | 8 |  | MHz |
|  | CW clock frequency | $1 \times$ CLK（16x mode） |  |  | 8 | MHz |
|  |  | 16× CLK（ $16 \times$ mode） |  |  | 128 |  |
|  |  | $4 \times$ CLK（ $4 \times$ mode） |  | 32 |  |  |
|  | AC coupled differential clock amplitude ${ }^{(3)}$ | CLKM＿16X－CLKP＿16X；CLKM＿1X－CLKP＿1X；LVDS，LVPECL | 0.4 | 0.7 |  | Vpp |
|  | CLK duty cycle | $1 \times$ and $16 \times$ CLKs | 35\％ |  | 65\％ |  |
|  | Common－mode voltage | Internal provided |  | 2.5 |  | V |
| $\mathrm{V}_{\text {CMOS }}$ | CMOS input clock amplitude |  | 4 |  | 5 | V |
|  | CW mixer conversion loss |  |  | 4 |  | dB |
|  | CW mixer phase noise | 1 kHz off 2－MHz carrier |  | 156 |  | $\mathrm{dBc} / \mathrm{Hz}$ |
| DR | Input dynamic range | $\mathrm{F}_{\text {IN }}=2 \mathrm{MHz}, \mathrm{LNA}=24 / 18 / 15 \mathrm{~dB}$ |  | 160，164， 165 |  | dBFS／Hz |
| IMD3 | Intermodulation distortion | $f_{1}=5.00 \mathrm{MHz}, f_{2}=5.01 \mathrm{MHz}$ ，both tones at $-8.5-\mathrm{dBm}$ amplitude， 8 channels summed up in－phase，CW feedback resistor $=87 \Omega$ |  | －50 |  | dBc |
|  |  | $f_{1}=5 \mathrm{MHz}, f_{2}=5.01 \mathrm{MHz}$ ，both tones at $-8.5-\mathrm{dBm}$ amplitude，single－ channel case，CW feedback resistor $=500 \Omega$ |  | －60 |  | dBc |
|  | I／Q channel gain matching | $16 \times$ mode |  | $\pm 0.04$ |  | dB |
|  | I／Q channel phase matching | $16 \times$ mode |  | $\pm 0.1$ |  | 。 |
|  | I／Q channel gain matching | $4 \times$ mode |  | $\pm 0.04$ |  | dB |
|  | I／Q channel phase matching | $4 \times$ mode |  | $\pm 0.1$ |  | － |
|  | Image rejection ratio | $\mathrm{F}_{\text {IN }}=2.01 \mathrm{MHz}, 300-\mathrm{mV}$ input amplitude， CW clock frequency $=2 \mathrm{MHz}$ |  | －50 |  | dBc |
| CW SUMMING AMPLIFIER |  |  |  |  |  |  |
| $\mathrm{V}_{\text {Смо }}$ | Common－mode voltage | Summing amplifier inputs／outputs |  | 1.5 |  | V |
|  | Summing amplifier output |  |  | 4 |  | Vpp |
| Input referred voltage noise |  | 100 Hz |  | 2 |  | nV／rtHz |
|  |  | 1 kHz |  | 1.2 |  | nV／rtHz |
|  |  | 2 kHz to 100 MHz |  | 1 |  | $\mathrm{nV} / \mathrm{rtHz}$ |
|  | Input referred current noise |  |  | 2.5 |  | $\mathrm{pA} / \mathrm{ttHz}$ |
|  | Unit gain bandwidth |  |  | 200 |  | MHz |
|  | Max output current | Linear operation range |  | 20 |  | mApp |
| ADC SPECIFICATIONS |  |  |  |  |  |  |
|  | Sample rate |  | 10 |  | 65 | MSPS |
| SNR | Signal－to－noise ratio | Idle channel SNR of ADC 14b |  | 77 |  | dBFS |
| Internal reference mode |  | REFP |  | 1.5 |  | V |
|  |  | REFM |  | 0.5 |  | V |

（2）In the $16 \times$ operation mode，the CW operation range is limited to 8 MHz due to the $16 \times$ CLK．The maximum clock frequency for the $16 \times$ CLK is 128 MHz ．In the $8 \times, 4 \times$ ，and $1 \times$ modes，higher CW signal frequencies up to 15 MHz can be supported with small degradation in performance，see application information：CW Clock Selection．
（3）Clocks with fast slew rate achieves desired phase noise．5V CMOS clock achieves the best performance in terms of phase noise．See CW Clock Selection

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## Electrical Characteristics（接下页）

AVDD＿5V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}$, AVDD＿ADC $=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ，AC－coupled with $0.1 \mu \mathrm{~F}$ at INP and bypassed to ground with 15 nF at INM，No active termination， $\mathrm{V}_{\text {CNTL }}=0 \mathrm{~V}, f_{\mathrm{IN}}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF Filter $=15 \mathrm{MHz}$ ，low－noise mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ ，Single－ended $\mathrm{V}_{\text {CNTL }}$ mode，VCNTLM $=$ GND，ADC configured in internal reference mode，internal $500-\Omega \mathrm{CW}$ feedback resistor，CMOS CW clocks，at ambient temperature， $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ， Digital demodulator is disabled unless otherwise noted．Min and max values are specified across full－temperature range with AVDD＿5 V $=5 \mathrm{~V}$, AVDD $=3.3 \mathrm{~V}$, AVDD＿ADC $=1.8 \mathrm{~V}, \mathrm{DVDD}=1.8 \mathrm{~V}$ ．

| PARAMETER | TEST CONDITIONS | MIN TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: |
| External reference mode | VREF＿IN voltage | 1.4 |  | V |
|  | VREF＿IN current | 50 |  | $\mu \mathrm{A}$ |
| ADC input full－scale range |  | 2 |  | Vpp |
| LVDS rate | 65 MSPS at 14 bit | 910 |  | Mbps |
| POWER DISSIPATION |  |  |  |  |
| AVDD voltage |  | 3.15 3．3 | 3.6 | V |
| AVDD＿ADC voltage |  | 1.7 1．8 | 1.9 | V |
| AVDD＿5V voltage |  | 4.75 5 | 5.5 | V |
| DVDD voltage |  | 1.7 1．8 | 1.9 | V |
| Total power dissipation per channel | TGC low－noise mode， 65 MSPS | 180 | 214 | mW／CH |
|  | TGC low－noise mode， 40 MSPS | 163 |  |  |
|  | TGC medium－power mode， 40 MSPS | 125 |  |  |
|  | TGC low－power mode， 40 MSPS | 109 |  |  |
| AVDD（3．3－V）current | TGC low－noise mode，no signal | 108 | 130 | mA |
|  | TGC medium－power mode，no signal | 68 |  |  |
|  | TGC low－power mode，no signal | 59 |  |  |
|  | CW－mode，no signal， 16 x clock $=80 \mathrm{MHz}$ | 49 |  |  |
|  | TGC low－noise mode， $500 \mathrm{mV} \mathrm{V}_{\text {PP }}$ Input， $1 \%$ duty cycle | 116 |  |  |
|  | TGC medium－power mode， $500 \mathrm{mV}_{\mathrm{PP}}$ Input， $1 \%$ duty cycle | 75 |  |  |
|  | TGC low power， $500 \mathrm{mV} \mathrm{V}_{\text {PP }}$ Input， $1 \%$ duty cycle | 65 |  |  |
|  | CW－mode， $500 \mathrm{mV} \mathrm{V}_{\text {PP }}$ Input to all 8 channels | 281 |  |  |
| AVDD＿5V current | TGC mode no signal | 116 | 140 | mA |
|  | CW mode no signal， $16 \times$ clock $=80 \mathrm{MHz}$ | 139 |  |  |
|  | TGC mode， 500 mVpp Input， $1 \%$ duty cycle | 116.5 |  |  |
|  | CW－mode， 500 mV pp input | 148 |  |  |
| VCA power dissipation | TGC low－noise mode，no signal | 117 | 142 | $\mathrm{mW} / \mathrm{CH}$ |
|  | TGC medium－power mode，no signal | 79 |  |  |
|  | TGC low－power mode，no signal | 63 |  |  |
|  | TGC low－noise mode， $500 \mathrm{mV} \mathrm{V}_{\text {P }}$ input， $1 \%$ duty cycle | 121 |  |  |
|  | TGC medium－power mode， 500 mV VPP Input， $1 \%$ duty cycle | 82 |  |  |
|  | TGC low－power mode， 500 mVpp input， $1 \%$ duty cycle | 67 |  |  |
| CW power dissipation | No signal，ADC shutdown CW mode no signal，16× clock $=80 \mathrm{MHz}$ | 107 |  | mW／CH |
|  | 500 mV PP input， ADC shutdown， $16 \times$ clock $=80 \mathrm{MHz}$ | 209 |  |  |
| AVDD＿ADC（1．8－V）current | 65MSPS | 187 | 220 | mA |
| DVDD（1．8－V）current | 65 MSPS | 90 | 110 | mA |
| ADC power dissipation／CH | 65 MSPS | 59 | 69 | mW／CH |
|  | 50 MSPS | 51 |  |  |
|  | 40 MSPS | 46 |  |  |
|  | 20 MSPS | 35 |  |  |
| Power dissipation in power down mode | PDN＿VCA $=$ High，PDN＿ADC＝High | 25 |  | mW／CH |
|  | Complete power－down PDN＿Global＝High | 0.675 |  |  |
| Power－down response time | Time taken to enter power down | 1 |  | $\mu \mathrm{s}$ |
| Power－up response time | VCA power down | $2 \mu \mathrm{~s}+1 \%$ of PDN time |  | $\mu \mathrm{s}$ |
|  | ADC power down | 1 |  |  |
|  | Complete power down | 2.5 |  | ms |
| Power supply modulation ratio，AVDD and AVDD＿5V | $\mathrm{F}_{\mathrm{IN}}=5 \mathrm{MHz}$ ，at $50 \mathrm{mV}_{\text {PP }}$ noise at 1 kHz on supply ${ }^{(4)}$ | －65 |  | dBc |
|  | $\mathrm{F}_{\text {IN }}=5 \mathrm{MHz}$ ，at 50 mVpp noise at 50 kHz on supply ${ }^{(4)}$ | －65 |  |  |

（4）PSMR specification is with respect to carrier signal amplitude．

## Electrical Characteristics（接下页）

AVDD＿5V $=5 \mathrm{~V}$, AVDD $=3.3 \mathrm{~V}$, AVDD＿ADC $=1.8 \mathrm{~V}, \operatorname{DVDD}=1.8 \mathrm{~V}, \mathrm{AC}$－coupled with $0.1 \mu \mathrm{~F}$ at INP and bypassed to ground with 15 nF at INM ，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, f_{\mathrm{IN}}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF Filter $=15 \mathrm{MHz}$ ，low－noise mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}$ ，Single－ended $\mathrm{V}_{\text {CNTL }}$ mode，VCNTLM $=$ GND，ADC configured in internal reference mode，internal $500-\Omega \mathrm{CW}$ feedback resistor，CMOS CW clocks，at ambient temperature， $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ， Digital demodulator is disabled unless otherwise noted．Min and max values are specified across full－temperature range with AVDD＿5 V $=5 \mathrm{~V}$, AVDD $=3.3 \mathrm{~V}$, AVDD＿ADC $=1.8 \mathrm{~V}, \mathrm{DVDD}=1.8 \mathrm{~V}$ ．

| PARAMETER | TEST CONDITIONS | MIN | TYP |
| :---: | :--- | :---: | :---: |
| Power supply rejection ratio | $f=10 \mathrm{kHz}, \mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}$（high gain），AVDD | MAX | -40 |
|  | $f=10 \mathrm{kHz}, \mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}$（high gain），AVDD＿5 V | dBc |  |
|  | $f=10 \mathrm{kHz}, \mathrm{V}_{\mathrm{CNTL}}=1 \mathrm{~V}$（low gain），AVDD | -55 |  |

## 9．6 Digital Demodulator Electrical Characteristics

AVDD＿5 V＝ 5 V, AVDD $=3.3 \mathrm{~V}$, AVDD＿ADC $=1.8 \mathrm{~V}, \mathrm{DVDD}=1.8 \mathrm{~V}$, DVDD＿LDO $=1.4 \mathrm{~V}$（internal generated）， 14 bit／65 MSPS， $4 \times$ decimation factor，at ambient temperature $T_{A}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．

|  | PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Additional power consumption on DVDD（1．8 V） | 65 MSPS， $4 \times$ decimation factor |  | 92 |  | $\mathrm{mW} / \mathrm{CH}$ |
|  | Additional current on DVDD（1．8V） | 65 MSPS， $4 \times$ decimation factor |  | 410 |  | mA／AFE |
|  | Additional power consumption on DVDD（1．8 V） | 40 MSPS， $4 \times$ decimation factor |  | 61 |  | $\mathrm{mW} / \mathrm{CH}$ |
|  | Additional power consumption on DVDD（1．8 V） | 65 MSPS， $32 \times$ decimation factor，half LVDS pairs are powered down |  | 79 |  | $\mathrm{mW} / \mathrm{CH}$ |
|  | Additional power consumption on DVDD（1．8 V） | 40 MSPS， $32 \times$ decimation factor，half LVDS pairs are powered down |  | 55 |  | $\mathrm{mW} / \mathrm{CH}$ |
|  | External DVDD＿LDO1，DVDD＿LDO2 | 65 MSPS， $4 \times$ decimation factor | 1.4 | 1.45 | 1.5 | V |
|  | Additional current on external DVDD＿LDO1＋DVDD＿LDO2 | 65 MSPS， $4 \times$ decimation factor |  | 300 |  | mA／AFE |
| $\mathrm{V}_{\mathrm{IH}}$ | Logic high input voltage，TX＿SYNC pin | Support 1．8－V and 3．3－V CMOS logic | 1.3 |  | 3.3 | V |
| $\mathrm{V}_{\text {IL }}$ | Logic low input voltage，TX＿SYNC pin | Support 1．8－V and 3．3－V CMOS logic | 0 |  | 0.3 | V |
| $\mathrm{I}_{\mathrm{H}}$ | Logic high input current，TX＿SYNC pin | $\mathrm{V}_{\text {HIGH }}=1.8 \mathrm{~V}$ |  | 11 |  | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {IL }}$ | Logic low input current，TX＿SYNC pin | $\mathrm{V}_{\text {LOW }}=0 \mathrm{~V}$ |  | ＜ 0.1 |  | $\mu \mathrm{A}$ |

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### 9.7 Digital Characteristics

Typical values are at $25^{\circ} \mathrm{C}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_5=5 \mathrm{~V}$ and $\mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$, $\mathrm{DVDD}=1.8 \mathrm{~V}$ unless otherwise noted. Minimum and maximum values are across the full temperature range: $\mathrm{T}_{\text {MIN }}=-40^{\circ} \mathrm{C}$ to $\mathrm{T}_{\text {MAX }}=85^{\circ} \mathrm{C}$.

| PARAMETER | TEST CONDITIONS | MIN | TYP MAX | UNIT ${ }^{(1)}$ |
| :---: | :---: | :---: | :---: | :---: |
| DIGITAL INPUTS/OUTPUTS |  |  |  |  |
| $\mathrm{V}_{\mathrm{IH}} \quad$ Logic high input voltage |  | 2 | 3.3 | V |
| $\mathrm{V}_{\text {IL }} \quad$ Logic low input voltage |  | 0 | 0.3 | V |
| Logic high input current |  |  | 200 | $\mu \mathrm{A}$ |
| Logic low input current |  |  | 200 | $\mu \mathrm{A}$ |
| Input capacitance |  |  | 5 | pF |
| $\mathrm{V}_{\mathrm{OH}} \quad$ Logic high output voltage | SDOUT pin |  | DVDD | V |
| $\mathrm{V}_{\text {OL }}$ Logic low output voltage | SDOUT pin |  | 0 | V |
| LVDS OUTPUTS |  |  |  |  |
| Output differential voltage | With $100-\Omega$ external differential termination |  | 400 | mV |
| Output offset voltage | Common-mode voltage |  | 1100 | mV |
| FCLKP and FCLKM | $1 \times$ clock rate | 10 | 65 | MHz |
| DCLKP and DCLKM | $7 \times$ clock rate | 70 | 455 | MHz |
|  | $6 \times$ clock rate | 60 | 390 | MHz |
| $\mathrm{t}_{\text {su }} \quad$ Data setup time ${ }^{(2)}$ |  |  | 350 | ps |
| $\mathrm{th}_{\mathrm{h}} \quad$ Data hold time ${ }^{(2)}$ |  |  | 350 | ps |
| ADC INPUT CLOCK |  |  |  |  |
| Clock frequency |  | 10 | 65 | MSPS |
| Clock duty cycle |  | 45\% | 50\% 55\% |  |
| Clock input amplitude, differential( $\left.\mathrm{V}_{\text {CLKP_ADC }}-\mathrm{V}_{\text {CLKM_ADC }}\right)$ | Sine-wave, AC-coupled | 0.5 |  | Vpp |
|  | LVPECL, LVDS, AC-coupled |  | >0.3 | Vpp |
| Common-mode voltage | Biased internally |  | 1 | V |
| Clock input amplitude VCLKP_ADC (singleended) | CMOS clock |  | 1.8 | Vpp |

(1) The DC specifications refer to the condition where the LVDS outputs are not switching, but are permanently at a valid logic level 0 or 1 with $100-\Omega$ external termination.
(2) Setup and hold time specifications take into account the effect of jitter on the output data and clock. These specifications also assume that the data and clock paths are perfectly matched within the receiver. Any mismatch in these paths within the receiver would appear as reduced timing margins

## 9．8 Timing Characteristics ${ }^{(1)}$

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD}$＿ADC $=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ．Typical values are at $25^{\circ} \mathrm{C}$ ，Differential clock， $\mathrm{C}_{\text {LOAD }}=$ $5 \mathrm{pF}, \mathrm{R}_{\text {LOAD }}=100 \Omega$ ， 14 bit，sample rate $=65 \mathrm{MSPS}$ ，digital demodulator is disabled，unless otherwise noted．Minimum and maximum values are across the full temperature range $\mathrm{T}_{\mathrm{MIN}}=-40^{\circ} \mathrm{C}$ to $\mathrm{T}_{\mathrm{MAX}}=85^{\circ} \mathrm{C}$ ．

| PARAMETER |  | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{ta}_{\mathrm{a}}$ | Aperture delay | The delay in time between the rising edge of the input sampling clock and the actual time at which the sampling occurs． | 0.7 | 3 |  | ns |
|  | Aperture delay matching | Across channels within the same device |  | $\pm 150$ |  | ps |
| $t_{j}$ | Aperture jitter |  |  | 450 |  | Fs rms |
|  | ADC latency | Default，after reset，or／ $0 \times 2$［12］＝1，LOW＿LATENCY＝ 1 |  | 11／8 |  | Input clock cycles |
| $t_{\text {delay }}$ | Data and frame clock delay | Input clock rising edge（zero cross）to frame clock rising edge（zero cross）minus $3 / 7$ of the input clock period（T） | 3 | 5.4 | 7 | ns |
| $\Delta t_{\text {delay }}$ | Delay variation | At fixed supply and $20^{\circ} \mathrm{C}$ T difference；device to device | －1 |  | 1 | ns |
| $\mathrm{t}_{\text {RISE }}$ | Data rise time | Rise time measured from -100 to 100 mV |  | 0.14 |  | ns |
| $\mathrm{t}_{\text {FALL }}$ | Data fall time | Fall time measured from 100 to $-100 \mathrm{mV} 10 \mathrm{MHz}<f_{\text {CLKIN }}<65$ MHz |  | 0.15 |  |  |
| $\mathrm{t}_{\text {FCLKRISE }}$ | Frame clock rise time | Rise time measured from -100 to 100 mV |  | 0.14 |  | ns |
| $\mathrm{t}_{\text {FCLKFALL }}$ | Frame clock fall time | Fall time measured from 100 to $-100 \mathrm{mV} 10 \mathrm{MHz}<f_{\text {CLKIN }}<65$ MHz |  | 0.15 |  |  |
|  | Frame clock duty cycle | Zero crossing of the rising edge to zero crossing of the falling edge | 48\％ | 50\％ | 52\％ |  |
| $\mathrm{t}_{\text {DCLKRISE }}$ | Bit clock rise time | Rise time measured from－100 to 100 mV |  | 0.13 |  | ns |
| $t_{\text {DCLKFALL }}$ | Bit clock fall time | Fall time measured from 100 to $-100 \mathrm{mV} 10 \mathrm{MHz}<f_{\text {CLKIN }}<65$ MHz | 0.12 |  |  |  |
|  | Bit clock duty cycle | Zero crossing of the rising edge to zero crossing of the falling edge $10 \mathrm{MHz}<f_{\text {CLKIN }}<65 \mathrm{MHz}$ | 46\％ |  | 54\％ |  |

（1）Timing parameters are ensured by design and characterization；not production tested．

## 9．9 Output Interface Timing（14－bit）

| fCLKIN， Input Clock Frequency | Setup Time（ $\mathrm{t}_{\text {sul }}$ ），ns |  |  | Hold Time（ $\mathrm{t}_{\mathrm{h}}$ ），ns |  |  | $\mathrm{t}_{\text {PROG }}=(3 / 7) \times \mathrm{T}+\mathrm{t}_{\text {delay }}, \mathrm{ns}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Data Valid to Bit Clock Zero－ Crossing |  |  | Bit Clock Zero－Crossing to Data Invalid |  |  | Input Clock Zero－Cross（Rising Edge）to Frame Clock Zero－Cross（Rising Edge） |  |  |
| MHz | MIN | TYP | MAX | MIN | TYP | MAX | MIN | TYP | MAX |
| 65 | 0.24 | 0.37 |  | 0.24 | 0.38 |  | 11 | 12 | 12.5 |
| 50 | 0.41 | 0.54 |  | 0.46 | 0.57 |  | 13 | 13.9 | 14.4 |
| 40 | 0.55 | 0.70 |  | 0.61 | 0.73 |  | 15 | 16 | 16.7 |
| 30 | 0.87 | 1.10 |  | 0.94 | 1.1 |  | 18.5 | 19.5 | 20.1 |
| 20 | 1.30 | 1.56 |  | 1.46 | 1.6 |  | 25.7 | 26.7 | 27.3 |

（1）FCLK timing is the same as for the output data lines．It has the same relation to DCLK as the data pins．Setup and hold are the same for the data and frame clock．
（2）Data valid is logic high $=100 \mathrm{mV}$ and logic low $=-100 \mathrm{mV}$
（3）Timing parameters are ensured by design and characterization；not production tested．

## 注

The above timing data can be applied to 12 －bit or 16 －bit LVDS rates as well．For example， the maximum LVDS output rate at 65 MHz and 14－bit is equal to 910 MSPS ，which is approximately equivalent to the rate at 56 MHz and 16 bits．


图 1．LVDS Timing Diagrams

## 9．10 SPI Timing Characteristics

Minimum values across full temperature range $\mathrm{T}_{\mathrm{MIN}}=-40^{\circ} \mathrm{C}$ to $\mathrm{T}_{\mathrm{MAX}}=85^{\circ} \mathrm{C}$ ，AVDD＿5V $=5 \mathrm{~V}$ ，AVDD $=3.3 \mathrm{~V}, \mathrm{AVDD} \_A D C=$ $1.8 \mathrm{~V}, \mathrm{DVDD}=1.8 \mathrm{~V}$

|  |  | PARAMETER | MIN |
| :--- | :--- | :---: | :---: |
| $\mathrm{t}_{1}$ | SCLK period | 50 |  |
| $\mathrm{t}_{2}$ | SCLK high time | MAX | UNIT |
| $\mathrm{t}_{3}$ | SCLK low time | 20 |  |
| $\mathrm{t}_{4}$ | Data setup time | ns |  |
| $\mathrm{t}_{5}$ | Data hold time | 5 |  |
| $\mathrm{t}_{6}$ | SEN fall to SCLK rise | ns |  |
| $\mathrm{t}_{7}$ | Time between last SCLK rising edge to $\overline{\text { SEN }}$ rising edge | 5 |  |
| $\mathrm{t}_{8}$ | SDOUT delay | ns |  |

## 9．11 Typical Characteristics

AVDD＿5 V $=5 \mathrm{~V}$ ，AVDD $=3.3 \mathrm{~V}$ ，AVDD＿ADC $=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ，AC－coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter $=15 \mathrm{MHz}$ ，low－noise mode，Single－ended $\mathrm{V}_{\mathrm{CNTL}}$ mode， $\mathrm{V}_{\mathrm{CNTLM}}=\mathrm{GND}$ ，$A D C$ is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


图 2．Gain vs $\mathrm{V}_{\mathrm{CNTL}}$ ，$L N A=18 \mathrm{~dB}$ and $P G A=24 \mathrm{~dB}$


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图 4．Gain Matching Histogram， $\mathrm{V}_{\mathrm{CNTL}}=0.3 \mathrm{~V}$（34951 Channels）


图 3．Gain Variation vs Temperature，LNA $=18 \mathrm{~dB}$ and PGA $=24 \mathrm{~dB}$


图 5．Gain Matching Histogram， $\mathrm{V}_{\mathrm{CNTL}}=0.6 \mathrm{~V}$（34951 Channels）

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## Typical Characteristics（接下页）

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ， $\mathrm{AC}-$ coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}$ ，LNA $=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter $=15 \mathrm{MHz}$ ，low－noise mode，Single－ended $\mathrm{V}_{\mathrm{CNTL}}$ mode， $\mathrm{V}_{\text {CNTLM }}=\mathrm{GND}$ ，ADC is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


图 6．Gain Matching Histogram， $\mathrm{V}_{\mathrm{CNTL}}=0.9 \mathrm{~V}$（34951 Channels）


图 8．Input Impedance Without Active Termination
（Magnitude）


图 10．Input Impedance With Active Termination（Magnitude）


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图 7．Output Offset Histogram， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}$（1247 Channels）


图 9．Input Impedance Without Active Termination（Phase）


图 11．Input Impedance With Active Termination（Phase）

## Typical Characteristics（接下页）

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ， AC －coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM ，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter $=15 \mathrm{MHz}$ ，low－noise mode，Single－ended $\mathrm{V}_{\text {CNTL }}$ mode， $\mathrm{V}_{\text {CNTLM }}=\mathrm{GND}$ ，ADC is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


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## Typical Characteristics（接下页）

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ， $\mathrm{AC}-$ coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}$ ，LNA $=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter $=15 \mathrm{MHz}$ ，low－noise mode，Single－ended $\mathrm{V}_{\text {CNTL }}$ mode， $\mathrm{V}_{\text {CNTLM }}=\mathrm{GND}$ ，ADC is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


图 18．IRN，PGA＝ $\mathbf{2 4} \mathrm{dB}$ and Low Noise Mode


图 20．IRN，PGA＝ $\mathbf{2 4}$ dB and Medium－Power Mode


图 22．IRN，PGA＝ 24 dB and Low－Power Mode


图 19．IRN，PGA＝ $\mathbf{2 4}$ dB and Low Noise Mode


图 21．IRN，PGA＝ $\mathbf{2 4}$ dB and Medium－Power Mode


图 23．IRN，PGA＝ $\mathbf{2 4} \mathrm{dB}$ and Low－Power Mode

## Typical Characteristics（接下页）

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ， AC －coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM ，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter $=15 \mathrm{MHz}$ ，low－noise mode，Single－ended $\mathrm{V}_{\mathrm{CNTL}}$ mode， $\mathrm{V}_{\text {CNTLM }}=\mathrm{GND}$ ，ADC is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


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## Typical Characteristics（接下页）

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ， $\mathrm{AC}-$ coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}$ ，LNA $=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter $=15 \mathrm{MHz}$ ，low－noise mode，Single－ended $\mathrm{V}_{\text {CNTL }}$ mode， $\mathrm{V}_{\text {CNTLM }}=\mathrm{GND}$ ，ADC is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


图 30．SNR，LNA＝ 18 dB and Low－Power Mode


图 32．Noise Figure，LNA＝ 15 dB and Low Noise Mode


图 34．Noise Figure，LNA＝ 24 dB and Low Noise Mode


图 31．SNR vs Different Power Modes


图 33．Noise Figure，LNA＝ 18 dB and Low Noise Mode


图 35．Noise Figure vs Power Modes With 400－$\Omega$ Termination

## Typical Characteristics（接下页）

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ， AC －coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM ，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter $=15 \mathrm{MHz}$ ，low－noise mode，Single－ended $\mathrm{V}_{\text {CNTL }}$ mode， $\mathrm{V}_{\text {CNTLM }}=\mathrm{GND}$ ，ADC is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


图 36．Noise Figure vs Power Modes Without Termination


图 38．HD3 vs Frequency， $\mathrm{V}_{\mathrm{IN}}=500 \mathrm{mVpp}$ and $\mathrm{V}_{\mathrm{OUT}}=\mathbf{- 1}$ dBFS


图 40．HD3 vs Gain，LNA $=15 \mathrm{~dB}$ and $P G A=24 \mathrm{~dB}$ and $\mathrm{V}_{\text {OUT }}$ $=-1 \mathrm{dBFS}$


图 37． HD 2 vs Frequency， $\mathrm{V}_{\mathrm{IN}}=500 \mathrm{mVpp}$ and $\mathrm{V}_{\text {OUT }}=-1$ dBFS


图 39．HD2 vs Gain，LNA＝ 15 dB and $P G A=24 \mathrm{~dB}$ and $\mathrm{V}_{\text {OUT }}$ $=-1 \mathrm{dBFS}$


图 41．HD2 vs Gain，LNA＝ 18 dB and $P G A=24 \mathrm{~dB}$ and $\mathrm{V}_{\text {OUT }}$ $=-1 \mathrm{dBFS}$

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## Typical Characteristics（接下页）

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ， $\mathrm{AC}-$ coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}$ ，LNA $=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter $=15 \mathrm{MHz}$ ，low－noise mode，Single－ended $\mathrm{V}_{\mathrm{CNTL}}$ mode， $\mathrm{V}_{\text {CNTLM }}=\mathrm{GND}$ ，ADC is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


## Typical Characteristics（接下页）

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}, \mathrm{DVDD}=1.8 \mathrm{~V}$ ， AC －coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM ，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}, \mathrm{LNA}=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter＝ 15 MHz ，low－noise mode，Single－ended $\mathrm{V}_{\text {CNTL }}$ mode， $\mathrm{V}_{\text {CNTLM }}=\mathrm{GND}$ ，ADC is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


图 48．AVDD＿5V Power Supply Modulation Ratio， 100 mVpp Supply Noise With Different Frequencies


图 50．AVDD＿5V Power Supply Rejection Ratio， 100 mVpp Supply Noise With Different Frequencies


图 52． $\mathrm{V}_{\text {CNTL }}$ Response Time，LNA $=18 \mathrm{~dB}$ and PGA $=\mathbf{2 4} \mathrm{dB}$


图 49．AVDD Power Supply Rejection Ratio， 100 mVpp Supply Noise With Different Frequencies


图 51． $\mathrm{V}_{\mathrm{CNTL}}$ Response Time，LNA $=\mathbf{1 8} \mathrm{dB}$ and PGA $=\mathbf{2 4} \mathrm{dB}$


图 53．Pulse Inversion Asymmetrical Positive Input

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## Typical Characteristics（接下页）

AVDD＿5 V $=5 \mathrm{~V}, \mathrm{AVDD}=3.3 \mathrm{~V}, \mathrm{AVDD} \_\mathrm{ADC}=1.8 \mathrm{~V}$ ，DVDD $=1.8 \mathrm{~V}$ ， $\mathrm{AC}-$ coupled with $0.1-\mu \mathrm{F}$ capacitors at INP and $15-\mathrm{nF}$ capacitors at INM，No active termination， $\mathrm{V}_{\mathrm{CNTL}}=0 \mathrm{~V}, \mathrm{~F}_{\mathrm{IN}}=5 \mathrm{MHz}$ ，LNA $=18 \mathrm{~dB}, \mathrm{PGA}=24 \mathrm{~dB}, 14$ bit，sample rate $=65$ MSPS，LPF filter $=15 \mathrm{MHz}$ ，low－noise mode，Single－ended $\mathrm{V}_{\mathrm{CNTL}}$ mode， $\mathrm{V}_{\text {CNTLM }}=\mathrm{GND}$ ，ADC is configured in internal reference mode， $\mathrm{V}_{\text {OUT }}=-1 \mathrm{dBFS}, 500-\Omega \mathrm{CW}$ feedback resistor，CMOS $16 \times$ clock，digital demodulator is disabled，at ambient temperature $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ ，unless otherwise noted．


图 54．Pulse Inversion Asymmetrical Negative Input


图 56．Overload Recovery Response vs INM Capacitor， $\mathrm{V}_{\mathrm{IN}}=$ $50 \mathrm{mVpp} / 100 \mu \mathrm{Vpp}$, Max Gain


图 58．Digital HPF Response

图 55．Pulse Inversion， $\mathrm{V}_{\mathrm{IN}}=2 \mathrm{Vpp}, \mathrm{PRF}=1 \mathrm{kHz}$ ，Gain＝ 21 dB


图 57．Overload Recovery Response vs INM Capacitor （Zoomed）， $\mathrm{V}_{\mathrm{IN}}=50 \mathrm{mVpp} / 100 \mu \mathrm{Vpp}$ ，Max Gain


图 59．Signal Chain Low Frequency Response With INM Capacitor $=1 \mu \mathrm{~F}$

## 10 Detailed Description

## 10．1 Overview

The AFE5812 is a highly－integrated AFE solution specifically designed for ultrasound systems in which high performance and small size are required．The AFE5812 integrates a complete TGC imaging path and a CWD path．It also enables users to select one of various power／noise combinations to optimize system performance． The AFE5812 contains eight channels；each channel includes a LNA，VCAT，PGA，LPF，14－bit ADC，digital I／Q demodulator，and CW mixer．

Multiple features in the AFE5812 are suitable for ultrasound applications，such as active termination，individual channel control，fast power－up and power－down response，programmable clamp voltage control，and fast and consistent overload recovery．Therefore，the AFE5812 brings premium image quality to ultraportable，handheld systems all the way up to high－end ultrasound systems．

In addition，the signal chain of the AFE5812 can handle ultrasound systems or tranducers with a center frequency from 50 kHz to 50 MHz ．This enables the AFE5812 to be used in both sonar and medical applications．
图 60 shows a simplified functional block diagram．

## 10．2 Functional Block Diagram



图 60．Simplified Functional Block Diagram

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## Functional Block Diagram（接下页）



图 61．Digital Demodulator Block Diagram，M＝4

## 10．3 Feature Description

## 10．3．1 LNA

In many high－gain systems，a LNA is critical to achieve overall performance．Using a new proprietary architecture，the LNA in the AFE5812 delivers exceptional low－noise performance，while operating on a low－ quiescent current compared to CMOS－based architectures with similar noise performance．The LNA performs single－ended input to differential output voltage conversion．It is configurable for a programmable gain of 24，18， or 15 dB and its input－referred noise is only $0.63,0.7$ ，or $0.9 \mathrm{nV} / \mathrm{VHz}$ ，respectively．Programmable gain settings result in a flexible linear input range up to 0.70 Vpp ，realizing high－signal handling capability demanded by new transducer technologies．A larger input signal can be accepted by the LNA；however，the signal can be distorted because it exceeds the LNA＇s linear operation region．Combining the low noise and high－input range，the device consequently achieves a wide－input dynamic range for supporting the high demands from various ultrasound imaging modes．

## Feature Description（接下页）

The LNA input is internally biased at approximately 2.2 V ；the signal source should be AC－coupled to the LNA input by an adequately－sized capacitor，for example $\geq 0.1 \mu \mathrm{~F}$ ．To achieve low DC offset drift，the AFE5812 incorporates a DC offset correction circuit for each amplifier stage．To improve the overload recovery，an integrator circuit is used to extract the DC component of the LNA output and then fed back to the LNA＇s complementary input for DC offset correction．This DC offset correction circuit has a high－pass response and can be treated as a HPF．The effective corner frequency is determined by the capacitor $\mathrm{C}_{\text {BYPAss }}$ connected at INM． With larger capacitors，the corner frequency is lower．For stable operation at the highest HP filter cut－off frequency，a $\geq 15-\mathrm{nF}$ capacitor can be selected．This corner frequency scales almost linearly with the value of the $C_{\text {BYPASs．}}$ ．For example， 15 nF gives a corner frequency of approximately 100 kHz ，while 47 nF can give an effective corner frequency of 33 kHz ．The DC offset correction circuit can also be disabled or enabled through register 52［12］．A large capacitor like $1 \mu \mathrm{~F}$ can be used for setting low corner frequency（ $<2 \mathrm{kHz}$ ）of the LNA DC offset correction circuit．图 59 shows the frequency responses for low－frequency applications．
The AFE5812 can be terminated passively or actively．Active termination is preferred in ultrasound applications for reducing reflection from mismatches and achieving better axial resolution without degrading noise figure too much．Active termination values can be preset to $50,100,200$ ，and $400 \Omega$ ；other values also can be programmed by users through register 52［4：0］．A feedback capacitor is required between ACTx and the signal source as 图 62 shows．On the active termination path，a clamping circuit is also used to create a low－impedance path when overload signal is seen by the AFE5812．The clamp circuit limits large input signals at the LNA inputs and improves the overload recovery performance of the AFE5812．The clamp level can be set to $350 \mathrm{mVpp}, 600$ mVpp ，or 0.825 Vpp automatically depending on the LNA gain settings when register $52[10: 9]=0$ ．Other clamp voltages，such as $0.825 \mathrm{Vpp}, 0.6 \mathrm{Vpp}$ ，and 1.5 Vpp ，are also achievable by setting register 52［10：9］．This clamping circuit is also designed to obtain good pulse inversion performance and reduce the impact from asymmetric inputs．


图 62．AFE5812 LNA With DC Offset Correction Circuit

## 10．3．2 Voltage－Controlled Attenuator

The voltage－controlled attenuator is designed to have a linear－in－dB attenuation characteristic；that is，the average gain loss in dB （refer to 图 2）is constant for each equal increment of the control voltage（VCNTL）as shown in 图63．A differential control structure is used to reduce common mode noise．图 63 and 图 64 show a simplified attenuator structure．
The attenuator is essentially a variable voltage divider that consists of the series input resistor（RS）and seven shunt FETs placed in parallel and controlled by sequentially activated clipping amplifiers（A1 through A7）．VCNTL is the effective difference between VCNTLP and VCNTLM．Each clipping amplifier can be understood as a specialized voltage comparator with a soft transfer characteristic and well－controlled output limit voltage． Reference voltages V1 through V7 are equally spaced over the 0 －to $1.5-\mathrm{V}$ control voltage range．As the control voltage increases through the input range of each clipping amplifier，the amplifier output rises from a voltage where the FET is nearly OFF to VHIGH where the FET is completely ON．As each FET approaches its ON state

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## Feature Description（接下页）

and the control voltage continues to rise，the next clipping amplifier／FET combination takes over for the next portion of the piecewise－linear attenuation characteristic．Thus，low control voltages have most of the FETs turned OFF，producing minimum signal attenuation．Similarly，high control voltages turn the FETs ON，leading to maximum signal attenuation．Therefore，each FET acts to decrease the shunt resistance of the voltage divider formed by RS and the parallel FET network．
Additionally，a digitally－controlled TGC（DTGC）mode is implemented to achieve better phase－noise performance in the AFE5812．The attenuator can be controlled digitally instead of the analog control voltage， $\mathrm{V}_{\text {CNTL }}$ ．This mode can be set by the register bit 59［7］．The variable voltage divider is implemented as a fixed series resistance and FET as the shunt resistance．Each FET can be turned on by connecting the switches SW1 through SW7． Turning on each of the switches can give approximately 6 dB of attenuation．This can be controlled by the register bits 59［6：4］．This digital control feature can eliminate the noise from the $\mathrm{V}_{\text {CNTL }}$ circuit and ensure better SNR and phase noise for the TGC path．


图 63．Simplified Voltage－Controlled Attenuator（Analog Structure）


图 64．Simplified Voltage－Controlled Attenuator（Digital Structure，DTGC）
The voltage－controlled attenuator＇s noise follows a monotonic relationship to the attenuation coefficient．At higher attenuation，the input－referred noise is higher and vice－versa．The attenuator＇s noise is then amplified by the PGA and becomes the noise floor at ADC input．In the attenuator＇s high－attenuation operating range，that is $\mathrm{V}_{\text {CNTL }}$ is high，the attenuator＇s input noise may exceed the LNA output noise；the attenuator then becomes the dominant noise source for the following PGA stage and ADC．Therefore，the attenuator noise should be minimized compared to the LNA output noise．The AFE5812 attenuator is designed for achieving very－low noise even at high attenuation（low channel gain）and realizing better SNR in near field．表 2 lists the input referred noise for different attenuations．

表 2．Voltage－Controlled－Attenuator Noise versus Attenuation

| Attenuation（dB） | Attenuator Input Referred Noise（nV／rtHz） |
| :---: | :---: |
| -40 | 10.5 |
| -36 | 10 |
| -30 | 9 |

表 2．Voltage－Controlled－Attenuator Noise versus Attenuation（接下页）

| Attenuation（dB） | Attenuator Input Referred Noise（nV／rtHz） |
| :---: | :---: |
| -24 | 8.5 |
| -18 | 6 |
| -12 | 4 |
| -6 | 3 |
| 0 | 2 |

## 10．3．3 PGA

After the voltage－controlled attenuator，a PGA can be configured as 24 or 30 dB with a constant－input referred noise of $1.75 \mathrm{nV} / \mathrm{rtHz}$ ．The PGA structure consists of a differential voltage－to－current converter with programmable gain，clamping circuits，a transimpedance amplifier with a programmable LPF，and a DC offset correction circuit．图 65 shows its simplified block diagram．


图 65．Simplified Block Diagram of PGA
Low input noise is always preferred in a PGA，and its noise contribution should not degrade the ADC SNR too much after the attenuator．At the minimum attenuation（used for small input signals），the LNA noise dominates；at the maximum attenuation（large input signals），the PGA and ADC noise dominates．Thus，24－dB gain of PGA achieves better SNR as long as the amplified signals can exceed the noise floor of the ADC．

The PGA clamping circuit can be enabled（register 51）to improve the overload recovery performance of the AFE．If the user measures the standard deviation of the output just after overload，for $0.5 \mathrm{~V} \mathrm{~V}_{\text {CNTL }}$ ，it is about 3.2 LSBs in normal case，that is，the output is stable in about 1 clock cycle after overload．With the clamp disabled， the value approaches 4 LSBs meaning a longer time duration before the output stabilizes；however，with the clamp enabled，there will be degradation in HD3 for PGA output levels $>-2$ dBFS．For example，for a $-2-d B F S$ output level，the HD3 degrades by approximately 3 dB ．To maximize the output dynamic range，the maximum PGA output level can be above 2 Vpp even with the clamp circuit enabled；the ADC in the AFE5812 has excellent overload recovery performance to detect small signals right after the overload．

注
In the low－power and medium－power modes，PGA＿CLAMP is disabled for saving power if $51[7]=0$ ．

The AFE5812 integrates an anti－aliasing filter in the form of a programmable LPF in the transimpedance amplifier．The LPF is designed as a differential，active，third－order filter with Butterworth characteristics and a typical 18 dB per octave roll－off．Programmable through the serial interface，the -1 －dB frequency corner can be set to one of $10,15,20,30,35$ and 50 MHz ．The filter bandwidth is set for all channels simultaneously．
A selectable DC offset correction circuit is implemented in the PGA as well．This correction circuit is similar to the one used in the LNA．It extracts the DC component of the PGA outputs and feeds back to the PGA complementary inputs for DC offset correction．This DC offset correction circuit also has a high－pass response with a cut－off frequency of 80 kHz ．

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## 10．3．4 ADC

The ADC of the AFE5812 employs a pipelined converter architecture that consists of a combination of multi－bit and single－bit internal stages．Each stage feeds its data into the digital error correction logic，ensuring excellent differential linearity and no missing codes at the 14－bit level．The 14 bits given out by each channel are serialized and sent out on a single pair of pins in LVDS format．All eight channels of the AFE5812 operate from a common input clock（CLKP／M）．The sampling clocks for each of the eight channels are generated from the input clock using a carefully matched clock buffer tree．The $14 \times$ clock required for the serializer is generated internally from the CLKP／M pins．A $7 \times$ and $1 \times$ clock are also given out in LVDS format，along with the data，to enable easy data capture．The AFE5812 operates from internally－generated reference voltages that are trimmed to improve the gain matching across devices．The nominal values of REFP and REFM are 1.5 and 0.5 V ，respectively． Alternatively，the device also supports an external reference mode that can be enabled using the serial interface．

Using serialized LVDS transmission has multiple advantages，such as a reduced number of output pins（saving routing space on the board），reduced power consumption，and reduced effects of digital－noise coupling to the analog circuit inside the AFE5812．

## 10．3．5 Continuous－Wave（CW）Beamformer

CWD is a key function in mid－end to high－end ultrasound systems．Compared to the TGC mode，the CW path needs to handle high dynamic range along with strict phase－noise performance．CW beamforming is often implemented in analog domain due to the strict requirements．Multiple beamforming methods are implemented in ultrasound systems，including passive delay line，active mixer，and passive mixer．Among all of them，the passive mixer approach achieves optimized power and noise．It satisfies the CW processing requirements，such as wide dynamic range，low phase noise，accurate gain and phase matching．
图 66 and 图 67 show a simplified CW path block diagram and an in－phase or quadrature（I／Q）channel block diagram，respectively．Each CW channel includes a LNA，a voltage－to－current converter，a switch－based mixer，a shared summing amplifier with a LPF，and clocking circuits．

## 注

The local oscillator inputs of the passive mixer are $\cos (\omega t)$ for $\mathrm{I}-\mathrm{CH}$ and $\sin (\omega t)$ for Q－CH respectively．Depending on the users＇CW Doppler complex FFT processing，swapping I／Q channels in FPGA or DSP may be needed to get correct blood flow directions．

All blocks include well－matched in－phase and quadrature channels to achieve good image frequency rejection as well as beamforming accuracy．As a result，the image rejection ratio from an I／Q channel is better than -46 dBc ， which is desired in ultrasound systems．


图 66．Simplified Block Diagram of CW Path


Note：The approximately 10 －to $15-\Omega$ resistors at CW＿AMPINM／P are due to internal IC routing and can create slight attenuation．

## 图 67．Complete In－Phase or Quadrature－Phase Channel

The CW mixer in the AFE5812 is passive and switch based；a passive mixer adds less noise than an active mixer．It achieves good performance at low power．图 68 and the equations describe the principles of mixer operation，where $\mathrm{Vi}(\mathrm{t})$ ， $\mathrm{Vo}(\mathrm{t})$ ，and $\mathrm{LO}(\mathrm{t})$ are input，output，and local oscillator（LO）signals for a mixer respectively． The LO（t）is square－wave based and includes odd harmonic components，as shown in 公式 1.

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图 68．Block Diagram of Mixer Operation

$$
\begin{align*}
& V i(t)=\sin \left(\omega_{0} t+\omega_{d} t+\varphi\right)+f\left(\omega_{0} t\right) \\
& L O(t)=\frac{4}{\pi}\left[\sin \left(\omega_{0} t\right)+\frac{1}{3} \sin \left(3 \omega_{0} t\right)+\frac{1}{5} \sin \left(5 \omega_{0} t\right) \ldots\right] \\
& \operatorname{Vo}(t)=\frac{2}{\pi}\left[\cos \left(\omega_{d} t+\phi\right)-\cos \left(2 \omega_{0} t-\omega_{d} t+\phi\right) \ldots\right] \tag{1}
\end{align*}
$$

From 公式 1，the third－order and fifth－order harmonics from the LO can interface with the third－order and fifth－ order harmonic signals in the $\mathrm{Vi}(\mathrm{t})$ ，or the noise around the third－order and fifth－order harmonics in the $\mathrm{Vi}(\mathrm{t})$ ． Therefore，the mixer＇s performance is degraded．To eliminate this side effect due to the square－wave demodulation，a proprietary harmonic－suppression circuit is implemented in the AFE5812．The third－and fifth－ harmonic components from the LO can be suppressed by over 12 dB ．Thus，the LNA output noise around the third－order and fifth－order harmonic bands is not down－converted to base band．Hence，the device achieves

The mixed current outputs of the eight channels are summed together internally．An internal low－noise operational amplifier is used to convert the summed current to a voltage output．The internal summing amplifier is designed to accomplish low－power consumption，low noise，and ease of use．CW outputs from multiple AFE5812s can be further combined on system board to implement a CW beamformer with more than eight channels．See Typical Application for more detailed information．
Multiple clock options are supported in the AFE5812 CW path．Two CW clock inputs are required： $\mathrm{N} \times \mathrm{f}_{\mathrm{cw}}$ clock and $1 \times f_{\mathrm{cw}}$ clock，where $f_{\mathrm{cw}}$ is the CW transmitting frequency and N could be $16,8,4$ ，or 1 ．Users have the flexibility to select the most convenient system clock solution for the AFE5812．In the $16 \times f_{\mathrm{cw}}$ and $8 \times f_{\mathrm{cw}}$ modes，the third－and fifth－harmonic suppression feature can be supported．Thus，the $16 \times f_{\mathrm{cw}}$ and $8 \times f_{\mathrm{cw}}$ modes achieve better performance than the $4 \times f_{\mathrm{cw}}$ and $1 \times f_{\mathrm{cw}}$ modes．

## 10．3．5．1 $16 \times f_{c w}$ Mode

The $16 \times f_{\mathrm{cw}}$ mode achieves the best phase accuracy compared to other modes．It is the default mode for CW operation．In this mode， $16 \times f_{\mathrm{cw}}$ and $1 \times f_{\mathrm{cw}}$ clocks are required． $16 \times f_{\mathrm{cw}}$ generates LO signals with 16 accurate phases．Multiple AFE5812s can be synchronized by the $1 \times f_{\mathrm{cw}}$ ，that is LO signals in multiple AFEs can have the same starting phase．The phase noise specification is critical only for $16 \times$ clock．The $1 \times$ clock is for synchronization only and does not require low phase noise．See the phase noise requirement in Typical Application．
图 69 shows the top－level clock distribution diagram．Each mixer＇s clock is distributed through a $16 \times 8$ cross－ point switch．The inputs of the cross－point switch are 16 different phases of the $1 \times$ clock．TI recommends to align the rising edges of the $1 \times f_{\mathrm{cw}}$ and $16 \times f_{\mathrm{cw}}$ clocks．
The cross－point switch distributes the clocks with appropriate phase delay to each mixer．For example， $\mathrm{Vi}(\mathrm{t})$ is a received signal with a delay of $\frac{1}{16}^{\top}$ ，a delayed $L O(t)$ should be applied to the mixer to compensate for the $\frac{1}{16} T$ delay．Thus a $22.5^{\circ}$ delayed clock，that is $\frac{2 \pi}{16}$ ，is selected for this channel．The mathematic calculation is expressed in the following equations：

$$
\begin{align*}
& \operatorname{Vi}(\mathrm{t})=\sin \left[\omega_{0}\left(\mathrm{t}+\frac{1}{16 f_{0}}\right)+\omega_{\mathrm{d}} \mathrm{t}\right]=\sin \left[\omega_{0} \mathrm{t}+22.5^{\circ}+\omega_{\mathrm{d}} \mathrm{t}\right] \\
& \operatorname{LO}(\mathrm{t})=\frac{4}{\pi} \sin \left[\omega_{0}\left(\mathrm{t}+\frac{1}{16 f_{0}}\right)\right]=\frac{4}{\pi} \sin \left[\omega_{0} \mathrm{t}+22.5^{\circ}\right] \\
& \operatorname{Vo}(\mathrm{t})=\frac{2}{\pi} \cos \left(\omega_{\mathrm{d}} \mathrm{t}\right)+f\left(\omega_{\mathrm{n}} \mathrm{t}\right) \tag{2}
\end{align*}
$$

Vo（t）represents the demodulated Doppler signal of each channel．When the Doppler signals from N channels are summed，the signal－to－noise ratio improves．


图 69.

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图 70． $1 \times$ and $16 \times$ CW Clock Timing

## 10．3．5．2 $8 \times f_{c w}$ and $4 \times f_{c w}$ Modes

$8 \times f_{\mathrm{cw}}$ and $4 \times f_{\mathrm{cw}}$ modes are alternative modes when a higher frequency clock solution（that is $16 \times f_{\mathrm{cw}}$ clock） is not available in system．图 71 shows a block diagram of these two modes．

Good phase accuracy and matching are also maintained．Quadrature clock generator is used to create in－phase and quadrature clocks with exactly $90^{\circ}$ phase difference．The only difference between $8 \times f_{\mathrm{cw}}$ and $4 \times f_{\mathrm{cw}}$ modes is the accessibility of the third－and fifth－harmonic suppression filter．In the $8 \times f_{c w}$ mode，the suppression filter can be supported．In both modes，$\frac{1}{16}^{\top}$ phase delay resolution is achieved by weighting the in－phase and quadrature paths correspondingly．For example，if a delay of $\frac{1}{16}^{\top}$ or $22.5^{\circ}$ is targeted，the weighting coefficients should follow 公式 3，assuming $l_{\text {in }}$ and $Q_{\text {in }}$ are $\sin \left(\omega_{0} t\right)$ and $\cos \left(\omega_{0} t\right)$ respectively．

$$
\begin{align*}
& I_{\text {delayed }}(t)=I_{\text {in }} \cos \left(\frac{2 \pi}{16}\right)+Q_{\text {in }} \sin \left(\frac{2 \pi}{16}\right)=I_{\text {in }}\left(t+\frac{1}{16 f_{0}}\right) \\
& Q_{\text {delayed }}(t)=Q_{\text {in }} \cos \left(\frac{2 \pi}{16}\right)-I_{\text {in }} \sin \left(\frac{2 \pi}{16}\right)=Q_{\text {in }}\left(t+\frac{1}{16 f_{0}}\right) \tag{3}
\end{align*}
$$

Therefore，after I／Q mixers，phase delay in the received signals is compensated．The mixers＇outputs from all channels are aligned and added linearly to improve the signal－to－noise ratio．It is preferred to have the $4 \times f_{\mathrm{cw}}$ or $8 \times f_{c w}$ and $1 \times f_{c w}$ clocks both aligned at the rising edge．


图 71． $8 \times f_{\mathrm{cw}}$ and $4 \times f_{\mathrm{cw}}$ Block Diagram


图 72． $8 \times f_{\text {cw }}$ and $4 \times f_{c w}$ Timing Diagram

## 10．3．5．3 $1 \times f_{c w}$ Mode

The $1 \times f_{\mathrm{cw}}$ mode requires in－phase and quadrature clocks with low phase noise specifications．The ${ }^{\frac{1}{16}} \mathrm{~T}$ phase delay resolution is also achieved by weighting the in－phase and quadrature signals as described in the $8 \times f_{\mathrm{cw}}$ and $4 \times f_{\text {cw }}$ modes．


图 73．Block Diagram of $1 \times f_{c w}$ mode

## 10．3．6 Digital I／Q Demodulator

AFE5812 also includes a digital in－phase and quadrature（I／Q）demodulator and a low－pass decimation filter．The main purpose of the demodulation block is to reduce the LVDS data rate and improve overall system power efficiency．The I／Q demodulator accepts ADC output with up to 65 MSPS sampling rate and 14 －bit resolution．For example，after digital demodulation and $4 \times$ decimation filtering，the data rate for either in－phase or quadrature output is reduced to 16.25 MSPS ，and the data resolution is improved to 16 bits consequently．Hence，the overall LVDS trace reduction can be a factor of 2 ．This demodulator can be bypassed and powered down completely if it is not needed．

The digital demodulator block given in AFE5812 is designed to do down－conversion followed by decimation．The top－level block is divided into two exactly similar blocks：（1）subchip0 and（2）subchip1．Both subchips share four channels each，that is，subchip0（ADC．1，ADC．2，ADC．3，and ADC．4）and subchip1（ADC．5，ADC．6，ADC．7，and ADC．8）．


图 74．Subchip
The following four functioning blocks are given in each demodulator．Every block can be bypassed．
－DC removal block
－Down conversion
－Decimator
－Channel multiplexing InsTRUMENTS

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图 75．Digital Demodulator Block
1．DC removal block is used to remove DC offset．An offset value can be given to a specific register．
2．Down conversion or demodulation of signal is done by multiplying signal by $\cos \left(\omega_{0} t\right)$ and by $-\sin \left(\omega_{0} t\right)$ to give out I phase and $Q$ phase，respectively． $\cos (\omega t)$ and $-\sin (\omega t)$ are 14 －bit wide plus a sign bit．$\omega=2 \pi f, f$ can be set with resolution $\mathrm{Fs} / 2^{16}$ ，where Fs is the ADC sampling frequency．

注
The digital demodulator is based on a conventional down converter，that is，$-\sin \left(\omega_{0} t\right)$ is used for Q phase．

3．The decimator block has two functions：decimation filter and down sampler．Decimation filter is a variable coefficient symmetric FIR filter and its coefficients can be given using coefficient RAM．Number of taps of FIR filter is $16 \times$ decimation factor $(M)$ ．For decimation factor of $M, 8 M$ coefficients have to be stored in the coefficient bank．Each coefficient is 14 －bit wide．Down－sampler gives out 1 sample followed by M－ 1 samples zeros．
4．In 图 76，channel multiplexing is implemented for flexible data routing：


图 76．Channel Multiplexing

## 10．3．7 Equivalent Circuits



图 77．Equivalent Circuits of LNA Inputs


图 78．Equivalent Circuits of $\mathrm{V}_{\text {CNTLP／M }}$

（a）CW 1X and 16X Clocks

（b）ADC Input Clocks

图 79．Equivalent Circuits of Clock Inputs

（a）CW＿OUTP／M

（b）CW＿AMPINP／M


图 80．Equivalent Circuits of CW Summing Amplifier Inputs and Outputs


图 81．Equivalent Circuits of LVDS Outputs

## 10．3．8 LVDS Output Interface Description

AFE5812 has a LVDS output interface，which supports multiple output formats．The ADC resolutions can be configured as 12 bit or 14 bit as shown in the LVDS timing diagrams（图1）．The ADCs in the AFE5812 are running at 14 bits； 2 LSBs are removed when 12－bit output is selected；and two zeros are added at LSBs when 16 －bit output is selected．Appropriate ADC resolutions can be selected for optimizing system－performance cost effectiveness．When the devices run at 16－bit mode，higher－end FPGAs are required to process the higher rate of LVDS data．Corresponding register settings are listed in 表 5.

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## 10．4 Device Functional Modes

## 10．4．1 TGC Mode

By default，after reset the AFE is configured in TGC mode．Depending upon the system requirements，the device can be programmed in a suitable power mode using the register bits shown in VCA Register Map．In the TGC mode，the digital demodulator after ADC can be enabled as well for further digital processing．

## 10．4．2 CW Mode

To configure the device in CW mode，set the CW＿TGC＿SEL（ $0 \times 36[8]$ ）register bit to 1 ．To save power，the voltage－controlled attenuator and programmable gain amplifier in the TGC path can be disabled by setting the $0 \times 35[12$ ］to 1 ．Also，the ADC can be powered down completely using the $0 \times 1[0]$ ．Usually only half the number of channels in a system are active in the CW mode．Thus，the individual channel control can power－down unused channels and save power；see register $0 \times 1[9: 2]$ and $0 \times 35[7: 0]$ and Power Saving in CW Mode．

## 10．4．3 TGC＋CW Mode

In systems that require fast switching between the TGC and CW modes，either mode can be selected simply by setting the CW＿TGC＿SEL register bit．

## 10．4．4 Test Modes

The AFE5812 includes multiple test modes to accelerate system development．

## 10．4．4．1 ADC Test Modes

The AFE5812 can output a variety of test patterns on the LVDS outputs．These test patterns replace the normal ADC data output．The device may also be made to output 6 preset patterns：
1．Ramp：Setting Register $2[15: 13]=111$ causes all the channels to output a repeating full－scale ramp pattern． The ramp increments from zero code to full－scale code in steps of 1 LSB every clock cycle．After hitting the full－scale code，it returns back to zero code and ramps again．
2．Zeros：The device can be programmed to output all Os by setting Register 2［15：13］＝ 110 ．
3．Ones：The device can be programmed to output all 1 s by setting Register $2[15: 13]=100$.
4．Deskew Pattern：When $2[15: 13]=010$ ；this mode replaces the 14 －bit ADC output with the 01010101010101 word．
5．Sync Pattern：When $2[15: 13]=001$ ，the normal ADC output is replaced by a fixed 11111110000000 word．
6．Toggle：When $2[15: 13]=101$ ，the normal ADC output is alternating between 1 s and 0 s ．The start state of ADC word can be either 1 s or 0 s ．
7．Custom Pattern：It can be enabled when $2[15: 13]=011$ ．Users can write the required VALUE into register bits＜CUSTOM PATTERN＞，which is Register 5［13：0］．Then，the device will output VALUE at its outputs， about 3 to 4 ADC clock cycles after the $24^{\text {th }}$ rising edge of SCLK．So，the time taken to write one value is 24 SCLK clock cycles＋ 4 ADC clock cycles．To change the customer pattern value，users can repeat writing Register 5［13：0］with a new value．Due to the speed limit of SPI，the refresh rate of the custom pattern may not be high．For example， 128 points custom pattern takes approximately $128 \times(24$ SCLK clock cycles +4 ADC clock cycles）．

## 注

Only one of the above ADC patterns can be active at any given instant．
Digital demodulator should be disabled，i．e．0x16＝1．

## Device Functional Modes（接下页）

## 10．4．4．2 VCA Test Mode

The VCA has a test mode in which the CH7 and CH8 PGA outputs can be brought to the CW pins．By monitoring these PGA outputs，the functionality of VCA operation can be verified．The PGA outputs are connected to the virtual ground pins of the summing amplifier（CW＿IP＿AMPINM／P，CW＿QP＿AMPINM／P）through 5－k $\Omega$ resistors． The PGA outputs can be monitored at the summing amplifier outputs when the LPF capacitors $\mathrm{C}_{\mathrm{EXT}}$ are removed．Note that the signals at the summing amplifier outputs are attenuated due to the $5-\mathrm{k} \Omega$ resistors．The attenuation coefficient is $\mathrm{R}_{\text {INT／EXT }} / 5 \mathrm{k} \Omega$ ．

If users would like to check the PGA outputs without removing $\mathrm{C}_{\mathrm{EXT}}$ ，an alternative way is to measure the PGA outputs directly at the CW＿IP＿AMPINM／P and CW＿QP＿AMPINM／P when the CW summing amplifier is powered down．

Some registers are related to this test mode，PGA Test Mode Enable：Reg59［9］；Buffer Amplifier Power Down Reg59［8］；and Buffer Amplifier Gain Control Reg54［4：0］．Based on the buffer amplifier configuration，the registers can be set in different ways：
－Configuration 1
－In this configuration，the test outputs can be monitored at CW＿AMPINP／M．
－Reg59［9］＝1；test mode enabled
－Reg59［8］＝0；buffer amplifier powered－down
－Configuration 2
－In this configuration，the test outputs can be monitored at CW＿OUTP／M．
－Reg59［9］＝1；test mode enabled
－Reg59［8］＝1；buffer amplifier powered on
－Reg54［4：0］＝10H；internal feedback 2－k $\Omega$ resistor enabled．Different values can be used as well．


图 82．AFE5812 PGA Test Mode

## 10．5 Programming

## 10．5．1 Serial Peripheral Interface（SPI）Operation



图 83．SPI Interface in the AFE5812
图 83 shows the block diagram of SPI inerface in the AFE5812．SPI＿DIG＿EN and SEN are used to access ADC／VCA SPI or Demod SPI．After reset and SPI＿DIG＿EN pin is floating or SPI＿DIG＿EN＝1，the ADC／VCA SPI is accessiable．When SEN and SPI＿DIG＿EN are pulled down simultaneously，the demod SPI is accessiable．

## 10．5．1．1 Serial Register Write Description

Programming of different modes can be done through the serial interface formed by pins SEN（serial interface enable），SCLK（serial interface clock），SDATA（serial interface data），and RESET．All these pins have a pulldown resistor to GND of $20 \mathrm{k} \Omega$ ．Serial shift of bits into the device is enabled when SEN is low．Serial data，SDATA，is latched at every rising edge of SCLK when SEN is active（low）．The serial data is loaded into the register at every $24^{\text {th }}$ SCLK rising edge when SEN is low．If the word length exceeds a multiple of 24 bits，the excess bits are ignored．Data can be loaded in multiple of 24－bit words within a single active SEN pulse（an internal counter counts groups of 24 clocks after the falling edge of SEN）．The interface can work with the SCLK frequency from 20 MHz to low speeds（of a few Hertz）and even with non－ $50 \%$ duty cycle SCLK．The data is divided into two main portions：a register address（ 8 bits）and the data itself（ 16 bits），to load on the addressed register．When writing to a register with unused bits，set these to 0 ．图 84 shows this process．

## Programming（接下页）



图 84．SPI Timing


#### Abstract

注 TI recommends to synchronize SCLK to ADC CLK．Typically，SCLK can be generated by dividing ADC CLK by an integer factor of N ．In a system with multiple AFEs，SCLKs may not reach all AFEs simultaneously due to routing．To compensate routing differences and ensure AFEs＇outputs are aligned，SCLK can be adjusted to toggle on either the falling edge of ADCLK or the rising edge of ADC CLK（ensuring new register settings are loaded before next ADC sampling clock）．


ADC CLK is required to access the demodulation registers．
Refer to SPI Timing Characteristics for the timing characteristics of t1～t8．

## 10．5．1．2 Serial Register Readout

The device includes an option where the contents of the internal registers can be read back．This may be useful as a diagnostic test to verify the serial interface communication between the external controller and the AFE． First，the＜REGISTER READOUT ENABLE＞bit（RegO［1］）needs to be set to 1 ．Then，the user should initiate a serial interface cycle specifying the address of the register（A7 through A0）whose content has to be read．The data bits are don＇t care．The device outputs the contents（D15 through D0）of the selected register on the SDOUT pin．SDOUT has a typical delay， $\mathrm{t}_{8}$ ，of 20 ns from the falling edge of the SCLK．For lower speed SCLK， SDOUT can be latched on the rising edge of SCLK．For higher speed SCLK，for example，if the SCLK period is less than 60 ns ，it is better to latch the SDOUT at the next falling edge of SCLK．图 85 shows this operation．In the readout mode，users still can access the＜REGISTER READOUT ENABLE＞through SDATA／SCLK／SEN．To enable serial register writes，set the＜REGISTER READOUT ENABLE＞bit back to 0 ．

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## Programming（接下页）



图 85．Serial Interface Register Read
The AFE5812 SDOUT buffer is tri－stated and gets enabled only when 0［1］（REGISTER READOUT ENABLE）is enabled．SDOUT pins from multiple AFE5812s can be tied together without any pullup resistors．Level shifter SN74AUP1T04 can be used to convert $1.8-\mathrm{V}$ logic to $2.5-\mathrm{V} / 3.3-\mathrm{V}$ logics if needed．

## 10．5．1．3 SPI for Demodulator

Demodulator is enabled after a software or hardware reset．It can be disabled by setting the LSB of register $0 \times 16$ as 1．This is done using the ADC SPI interface，that is，SPI＿DIG＿EN＝1．The demodulator SPI interface is independent from the ADC／VCA SPI interface as shown in 图 83.

To access the specific demodulator registers：
1．SPI＿DIG＿EN pin is required to be set as 0 during SPI transactions to demodulator registers．Meanwhile， ADC SEN needs to be set as 0 during demodulator SPI programming．
2．The SPI register address is 8 bits and is made of 2 subchip select bits and 6 register address bits．SPI register data is 16 bits．
3．ADC CLK and DVDD＿LDO1／2 are required to access the demodulation registers．
表 3．Register Address Bit Description

| Bit7 | Bit6 | Bit 5：0 |
| :--- | :--- | :--- |
| SCID1＿SEL | SCID0＿SEL | Register address＜5：0＞ |

4．SCID0＿SEL enables configuration of channels 1 through 4．SCID1＿SEL enables configuration of channels 5 through 7．When performing demodulator SPI write transactions，these SCID bits can be individually or mutually used with a specific register address．
5．Register configuration is normally shared by both subchips（both SCID bits should be set as 1）．An exception to this rule would be the DC OFFSET registers（ $0 \times 14$ through $0 \times 17$ ）for which specific channel access is expected．


A．Each of two subchips supports four channels．
B．Each of two demodulators has four channels named as A，B，C，and D．

## 图 86．Subchip 0 and Subchip 1

6．Demodulator register readout follows these procedures：
－Write 1 to register $0 \times 0[1]$ ；pin SPI＿DIG＿EN should be 0 while writing．This is the readout enable register for demodulator．
－Write 1 to register $0 \times 0[1]$ ；pin SPI＿DIG＿EN should be 1 while writing．This is the readout enable register for ADC and VCA．
－Set SPI＿DIG＿EN as 0 and write anything to the register whose stored data needs to be known．Device finds the address of the register and sends its stored data at the SDOUT pin serially．

## 注

After enabling the register 0x0［1］REGISTER＿READOUT＿ENABLE，data cannot be written to the register（whose data needs to be known），but stored data would come serially at the SDOUT pin．
－To disable the register readout，first write 0 to register $0 \times 0[1]$ while SPI＿DIG＿EN is 1 ；then write 0 to register $0 \times 0$［1］while SPI＿DIG＿EN is 0 ．

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## 10．5．2 POWER UP SEQUENCE



A． $10 \mu \mathrm{~s}<\mathrm{t}_{1}<50 \mathrm{~ms}, 10 \mu \mathrm{~s}<\mathrm{t}_{2}<50 \mathrm{~ms},-10 \mathrm{~ms}<\mathrm{t}_{3}<10 \mathrm{~ms}, \mathrm{t}_{4}>10 \mathrm{~ms}, \mathrm{t}_{5}>100 \mathrm{~ns}, \mathrm{t}_{6}>100 \mathrm{~ns}, \mathrm{t}_{7}>10 \mathrm{~ms}$ ，and $\mathrm{t}_{8}>$ $100 \mu \mathrm{~s}$ ．When the demodulator power DVDD＿LDO1 and DVDD＿LDO2 are supplied externally，it should be powered up 1ms after DVDD．LDOs for external DVDD＿LDO1 and DVDD＿LDO2 can be powered down if the demodualtor is not used．
B．The AVDDx and DVDD power－on sequence does not matter as long as $-10 \mathrm{~ms}<\mathrm{t}_{3}<10 \mathrm{~ms}$ ．Similar considerations apply while shutting down the device．
图 87．Recommended Power－Up Sequencing with Internally Generated 1．4V Demod Supply

## 10．6 Register Maps

## 10．6．1 ADC and VCA Register Description

A reset process is required at the AFE5812 initialization stage．Initialization can be done in one of two ways：
－Through a hardware reset，by applying a positive pulse in the RESET pin．
－Through a software reset，using the serial interface，by setting the SOFTWARE RESET bit to high．Setting this bit initializes the internal registers to the respective default values（all zeros），and then self－resets the SOFTWARE RESET bit to low．In this case，the RESET pin can stay low（inactive）．

## 注

After reset，all ADC and VCA registers are set to 0 ，that is default setting．During register programming，all unlisted register bits need to be set as 0 ．
Some demodulator registers are set as 1 after reset．During register programming，all unlisted register bits need to be set as 0 ．In addition，the demodulator registers can be reset when $0 \times 16[0]$ is set as 0 ．Thus，it is required to reconfigure the demodulator registers after toggling the $0 \times 16[0]$ from 1 to 0 ．

## 10．6．1．1 ADC Register Map

| Address （DEC） | Address （HEX） | Default Value | Function | Description |
| :---: | :---: | :---: | :---: | :---: |
| O［0］ | 0x0［0］ | 0 | SOFTWARE＿RESET | 0：Normal operation <br> 1：Resets the device and self－clears the bit to 0 ．Note：Register 0 is a write only register． |
| 0 ［1］ | $0 \times 0$［1］ | 0 | REGISTER＿READOUT＿ENABLE | 0 ：Disables readout <br> 1：Enables readout of register at SDOUT pin．Note：When this bit is set to 0 ， the device always operates in write mode and when it is set to 1 ，device will be in read mode．Multiple reading or writing events can be performed when this bit is set to 1 or 0 correspondingly．Register 0 is a write－only register． |
| 1［0］ | 0x1［0］ | 0 | ADC＿COMPLETE＿PDN | 0 ：Normal <br> 1：Complete power down．Note：When the complete power－down mode is enabled，the digital demodulator may lose register settings．Therefore，it is required to reconfigure the demodulator registers，filter coefficient memory， and profile memory after exiting the complete power－down mode． |
| 1［1］ | 0x1［1］ | 0 | LVDS＿OUTPUT＿DISABLE | 0 ：Output enabled <br> 1：Output disabled |
| 1［9：2］ | 0x1［9：2］ | 0 | ADC＿PDN＿CH＜7：0＞ | 0：Normal operation <br> 1：Power down．Power down individual ADC channels． $1[9] \rightarrow \mathrm{CH} 8 \ldots 1[2] \rightarrow \mathrm{CH} 1$ |
| 1［10］ | 0x1［10］ | 0 | PARTIAL＿PDN | 0：Normal operation <br> 1：Partial power down ADC |
| 1［11］ | 0x1［11］ | 0 | LOW＿FREQUENCY NOISE＿SUPPRESSION | 0：No suppression <br> 1：Suppression enabled |
| 1［13］ | 0x1［13］ | 0 | EXT＿REF | 0 ：Internal reference <br> 1：External reference．VREF＿IN is used．Both 3［15］and 1［13］should be set as <br> 1 in the external reference mode |
| 1［14］ | 0x1［14］ | 0 | LVDS＿OUTPUT＿RATE＿2X | 0 ： $1 \times$ rate <br> 1： $2 \times$ rate．Combines data from 2 channels on 1 LVDS pair．When ADC clock rate is low，this feature can be used． |
| 1［15］ | 0x1［15］ | 0 | SINGLE－ENDED＿CLK＿MODE | 0 ：Differential clock input <br> 1：Single－ended clock input |
| 2［2：0］ | 0x2［2：0］ | 0 | RESERVED | Set to 0 |
| 2［10：3］ | 0x2［10：3］ | 0 | POWER－DOWN＿LVDS | 0：Normal operation <br> 1：PDN individual LVDS outputs．2［10］$\rightarrow$ CH8．．．2［3］$\rightarrow \mathrm{CH} 1$ |
| 2［11］ | 0x2［11］ | 0 | AVERAGING＿ENABLE | 0 ：No averaging <br> 1：Average two channels to increase SNR |
| 2［12］ | 0x2［12］ | 0 | LOW＿LATENCY | 0 ：Default latency with digital features supported <br> 1：Low latency with digital features bypassed |

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## Register Maps（接下页）

| Address （DEC） | Address （HEX） | Default Value | Function | Description |
| :---: | :---: | :---: | :---: | :---: |
| 2［15：13］ | 0x2［15：13］ | 0 | TEST＿PATTERN＿MODES | 000：Normal operation <br> 001：Sync <br> 010：De－skew <br> 011：Custom <br> 100：All 1＇s <br> 101：Toggle <br> 110：All O＇s <br> 111：Ramp．Note：Reg． $0 \times 16$ should be set as 1，i．e．demodulator is disabled． |
| 3［7：0］ | 0x3［7：0］ | 0 | INVERT＿CHANNELS | 0 ：No inverting <br> 1：Invert channel digital output．3［7］$\rightarrow \mathrm{CH8} ; 3[0] \rightarrow \mathrm{CH} 1$ ．Note：Suppose that the device is giving digital output of 11001100001111 ．After enabling this bit， output of device becomes 00110011110000 ．Note：This function is not applicable for ADC test patterns and in demod mode． |
| 3［8］ | 0x3［8］ | 0 | CHANNEL OFFSET SUBSTRACTION＿ENABLE | 0 ：No offset subtraction <br> 1：Offset value subtract enabled |
| 3［9：11］ | 0x3［9：11］ | 0 | RESERVED | Set to 0 |
| 3［12］ | 0x3［12］ | 0 | DIGITAL＿GAIN＿ENABLE | 0 ：No digital gain <br> 1：Digital gain enabled |
| 3［14：13］ | $0 \times 3$［14：13］ | 0 | SERIALIZED＿DATA＿RATE | Serialization factor <br> 00：14× <br> 01： $16 \times$ <br> 10：Reserved <br> 11：12× <br> When $4[1]=1$ ，in the $16 \times$ serialization rate，two zeros are filled at two LSBs （see 表 5）．Note：Make sure the settings aligning with the demod register $0 \times 3[14: 13]$ ．Be aware that the same setting，for example， 00 ，in these two registers can represent different LVDS data rates respectively． |
| 3［15］ | 0x3［15］ | 0 | ENABLE＿EXTERNAL REFERENCE＿MODE | 0 ：Internal reference mode <br> 1：Set to external reference mode <br> Note：Both $3[15]$ and $1[13]$ should be set as 1 when configuring the device in the external reference mode． |
| 4［1］ | 0x4［1］ | 0 | ADC＿RESOLUTION＿SELECT | $\begin{aligned} & 0: 14 \text { bit } \\ & 1: 12 \text { bit } \end{aligned}$ |
| 4［3］ | 0x4［3］ | 0 | ADC＿OUTPUT＿FORMAT | 0：2＇s complement <br> 1：Offset binary <br> Note：When the demodulation feature is enabled，only 2＇s complement format can be selected． |
| 4［4］ | 0x4［4］ | 0 | LSB＿MSB＿FIRST | 0：LSB first <br> 1：MSB first |
| 5［13：0］ | 0x5［13：0］ | 0 | CUSTOM＿PATTERN | Custom pattern data for LVDS output（2［15：13］＝011） |
| 10［8］ | 0xA［8］ | 0 | SYNC＿PATTERN | 0 ：Test pattern outputs of 8 channels are not synchronized． <br> 1：Test pattern outputs of 8 channels are synchronized． |
| 13［9：0］ | 0xD［9：0］ | 0 | OFFSET＿CH1 | Value to be subtracted from channel 1 code |
| 13［15：11］ | 0xD［15：11］ | 0 | DIGITAL＿GAIN＿CH1 | 0 to 6 dB in 0．2－dB steps |
| 15［9：0］ | 0xF［9：0］ | 0 | OFFSET＿CH2 | Value to be subtracted from channel 2 code |
| 15［15：11］ | 0xF［15：11］ | 0 | DIGITAL＿GAIN＿CH2 | 0 to 6 dB in 0．2－dB steps |
| 17［9：0］ | 0x11［9：0］ | 0 | OFFSET＿CH3 | Value to be subtracted from channel 3 code |
| 17［15：11］ | 0x11［15：11］ | 0 | DIGITAL＿GAIN＿CH3 | 0 to 6 dB in 0．2－dB steps |
| 19［9：0］ | 0x13［9：0］ | 0 | OFFSET＿CH4 | Value to be subtracted from channel 4 code |
| 19［15：11］ | 0x13［15：11］ | 0 | DIGITAL＿GAIN＿CH4 | 0 to 6 dB in 0．2－dB steps |
| 21［0］ | 0x15［0］ | 0 | $\begin{aligned} & \text { DIGITAL_HPF_FILTER_ENABLE } \\ & -\mathrm{CH} 1-4 \end{aligned}$ | 0 ：Disable the digital HPF filter； <br> 1：Enable for 1 to 4 channels <br> Note：This HPF feature is only available when the demodulation block is disabled． |
| 21［4：1］ | 0x15［4：1］ | 0 | DIGITAL＿HPF＿FILTER＿K＿CH1－4 | Set $K$ for the HPF（ $k$ from 2 to 10，that is 0010B to 1010B）． <br> This group of four registers controls the characteristics of a digital high－pass transfer function applied to the output data，following the formula： $y(n)=2^{k} /\left(2^{k}+1\right)[x(n)-x(n-1)+y(n-1)] \text { (see 表 4) }$ |

## Register Maps（接下页）

| Address （DEC） | Address （HEX） | Default Value | Function | Description |
| :---: | :---: | :---: | :---: | :---: |
| 22［0］ | 0x16［0］ | 0 | DIS＿DEMOD | 0 ：Digital demodulator is enabled <br> 1：Digital demodulator is disabled <br> Note：The demodulator registers can be reset when $0 \times 16[0]$ is set as 0 ．Thus， it is required to reconfigure the demodulator registers after toggling the $0 \times 16[0]$ ． |
| 25［9：0］ | 0x19［9：0］ | 0 | OFFSET＿CH8 | Value to be subtracted from channel 8 code |
| 25［15：11］ | 0x19［15：11］ | 0 | DIGITAL＿GAIN＿CH8 | 0 to 6－dB in 0．2－dB steps |
| 27［9：0］ | 0x1B［9：0］ | 0 | OFFSET＿CH7 | Value to be subtracted from channel 7 code |
| 27［15：11］ | 0x1B［15：11］ | 0 | DIGITAL＿GAIN＿CH7 | 0 to 6－dB in 0．2－dB steps |
| 29［9：0］ | 0x1D［9：0］ | 0 | OFFSET＿CH6 | Value to be subtracted from channel 6 code |
| 29［15：11］ | 0x1D［15：11］ | 0 | DIGITAL＿GAIN＿CH6 | 0 to 6－dB in 0．2－dB steps |
| 31［9：0］ | 0x1F［9：0］ | 0 | OFFSET＿CH5 | Value to be subtracted from channel 5 code |
| 31［15：11］ | 0x1F［15：11］ | 0 | DIGITAL＿GAIN＿CH5 | 0 to 6－dB in 0．2－dB steps |
| 33［0］ | 0x21［0］ | 0 | DIGITAL＿HPF＿FILTER＿ENABLE ＿ $\mathrm{CH} 5-8$ | 0 ：Disable the digital HPF filter <br> 1：Enable for 5 to 8 channels <br> Note：This HPF feature is only available when the demodulation block is disabled． |
| 33［4：1］ | 0x21［4：1］ | 0 | DIGITAL＿HPF＿FILTER＿K＿CH5－8 | Set $K$ for the HPF（ $k$ from 2 to 10，0010B to 1010B） <br> This group of four registers controls the characteristics of a digital high－pass transfer function applied to the output data，following the formula： $y(n)=2^{k} /\left(2^{k}+1\right)[x(n)-x(n-1)+y(n-1)](\text { see 表 } 4)$ |

## 10．6．1．2 AFE5812 ADC Register／Digital Processing Description

The ADC in the AFE5812 has extensive digital processing functionality，which can be used to enhance ultrasound system performance．The digital processing blocks are arranged as in 图 88.


图 88．ADC Digital Block Diagram
These digital processing features are only available when the demodulation block is
disabled．ADC output data directly enter the digital demodulator when the demod is
enabled．

## 10．6．1．2．1 AVERAGING＿ENABLE：Address：2［11］

When set to 1 ，two samples，corresponding to two consecutive channels，are averaged（channel 1 with 2,3 with 4,5 with 6 ，and 7 with 8 ）．If both channels receive the same input，the net effect is an improvement in SNR．The averaging is performed as：
－Channel $1+$ channel 2 comes out on channel 3
－Channel $3+$ channel 4 comes out on channel 4
－Channel $5+$ channel 6 comes out on channel 5
－Channel $7+$ channel 8 comes out on channel 6

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## 10．6．1．2．2 ADC＿OUTPUT＿FORMAT：Address：4［3］

The ADC output，by default，is in 2＇s－complement mode．Programming the ADC＿OUTPUT＿FORMAT bit to 1 inverts the MSB，and the output becomes straight－offset binary mode．When the demodulation feature is enabled，only 2＇s complement format can be selected．

## 10．6．1．2．3 ADC Reference Mode：Address 1［13］and 3［15］

The following shows the register settings for the ADC internal reference mode and external reference mode．
－ $0 \times 1[13] 0 \times 3[15]=00$ ：ADC internal reference mode，VREF＿IN floating（pin M3）
－ $0 \times 1[13] 0 \times 3[15]=01: N / A$
－ $0 \times 1[13] 0 \times 3[15]=10$ ：N／A
－ $0 \times 1[13] 0 \times 3[15]=11$ ：ADC external reference mode，VREF＿IN＝ 1.4 V （pin M3）

## 10．6．1．2．4 DIGITAL＿GAIN＿ENABLE：Address：3［12］

Setting this bit to 1 applies to each channel $i$ the corresponding gain given by DIGTAL＿GAIN＿CHi $<15: 11>$ ．The gain is given as $0 \mathrm{~dB}+0.2 \mathrm{~dB} \times$ DIGTAL＿GAIN＿CHi＜15：11＞．For instance，if DIGTAL＿GAIN＿CH5＜15：11＞$=3$ ， channel 5 is increased by $0.6-\mathrm{dB}$ gain．DIGTAL＿GAIN＿CHi＜15：11＞$=31$ produces the same effect as DIGTAL＿GAIN＿CHi＜15：11＞＝30，setting the gain of channel ito 6 dB ．

## 10．6．1．2．5 DIGITAL＿HPF＿ENABLE

－ CH 1 to CH 4 ：Address $21[0]$
－CH5 to CH8：Address 33［0］

## 10．6．1．2．6 DIGITAL＿HPF＿FILTER＿K＿CHX

－ CH 1 to CH4：Address 21［4：1］
－ CH 5 to CH 8 ：Address 33［4：1］
This group of registers controls the characteristics of a digital high－pass transfer function applied to the output data，following 公式 4.
$y(n)=\frac{2^{k}}{2^{k}+1}[x(n)-x(n-1)+y(n-1)]$
These digital HPF registers（one for the first four channels and one for the second group of four channels） describe the setting of K．The digital HPF can be used to suppress low frequency noise，which commonly exists in ultrasound echo signals．The digital filter can significantly benefit near－field recovery time due to T／R switch low－frequency response．表 4 shows the cut－off frequency versus K ．

表 4．Digital HPF－1－dB Corner Frequency versus $K$ and Fs

| $\mathbf{k}$ | $\mathbf{4 0} \mathbf{~ M S P S}$ | $\mathbf{5 0} \mathbf{~ M S P S}$ | $\mathbf{6 5} \mathbf{~ M S P S}$ |
| :---: | :---: | :---: | :---: |
| 2 | 2780 kHz | 3480 kHz | 4520 kHz |
| 3 | 1490 kHz | 1860 kHz | 2420 kHz |
| 4 | 770 kHz | 960 kHz | 1250 kHz |

## 10．6．1．2．7 LOW＿FREQUENCY＿NOISE＿SUPPRESSION：Address：1［11］

The low－frequency noise suppression mode is especially useful in applications where good noise performance is desired in the frequency band of 0 to 1 MHz （around dc）．Setting this mode shifts the low－frequency noise of the AFE5812 to approximately Fs／2，thereby moving the noise floor around dc to a much lower value．Register bit $1[11]$ is used for enabling or disabling this feature．When this feature is enabled，power consumption of the device is increased slightly by approximately $1 \mathrm{~mW} / \mathrm{CH}$ ．

## 10．6．1．2．8 LVDS＿OUTPUT＿RATE＿2X：Address：1［14］

The output data always uses a DDR format，with valid／different bits on the positive as well as the negative edges of the LVDS bit clock，DCLK．The output rate is set by default to $1 \times$（LVDS＿OUTPUT＿RATE＿2X＝0），where each ADC has one LVDS stream associated with it．If the sampling rate is low enough，two ADCs can share one LVDS stream，in this way lowering the power consumption devoted to the interface．The unused outputs will output zero．To avoid consumption from those outputs，no termination should be connected to them．The distribution on the used output pairs is done in the following way：
－Channel 1 and channel 2 come out on channel 3 ．Channel 1 comes out first．
－Channel 3 and channel 4 come out on channel 4 ．Channel 3 comes out first．
－Channel 5 and channel 6 come out on channel 5 ．Channel 5 comes out first．
－Channel 7 and channel 8 come out on channel 6 ．Channel 7 comes out first．

## 10．6．1．2．9 CHANNEL＿OFFSET＿SUBSTRACTION＿ENABLE：Address：3［8］

Setting this bit to 1 enables the subtraction of the value on the corresponding OFFSET＿CHx＜9：0＞（offset for channel i）from the ADC output．The number is specified in 2 ＇s complement format．For example， OFFSET＿CHx＜9：0＞＝ 1110000000 means subtract -128 ．For OFFSET＿CHx＜9：0＞$=0001111111$ the effect is to subtract 127．In effect，both addition and subtraction can be performed．Note that the offset is applied before the digital gain（see DIGITAL＿GAIN＿ENABLE）．The whole data path is 2＇s complement throughout internally， with digital gain being the last step．Only when ADC＿OUTPUT＿FORMAT $=1$（straight binary output format）is the 2＇s complement word translated into offset binary at the end．

## 10．6．1．2．10 SERIALIZED＿DATA＿RATE：Address：3［14：13］

See 表 5 for detailed description．
表 5．Corresponding Register Settings

| LVDS Rate | 12 bit（6× DCLK） | $\mathbf{1 4}$ bit（7× DCLK） | 16 bit（8× DCLK） |
| :---: | :---: | :---: | :---: |
| Register 3［14：13］ | 11 | 00 | 01 |
| Register 4［2：0］ | 010 | 000 | 000 |
| Description | 2 LSBs removed | N／A | 2 zeroes added at LSBs |

## 10．6．1．2．11 TEST＿PATTERN＿MODES：Address：2［15：13］

The AFE5812 can output a variety of test patterns on the LVDS outputs．These test patterns replace the normal ADC data output．The device may also be made to output 6 preset patterns：
1．Ramp：Setting Register $2[15: 13]=111$ causes all the channels to output a repeating full－scale ramp pattern． The ramp increments from zero code to full－scale code in steps of 1 LSB every clock cycle．After hitting the full－scale code，it returns back to zero code and ramps again．
2．Zeros：The device can be programmed to output all 0 s by setting Register 2［15：13］＝ 110.
3．Ones：The device can be programmed to output all 1 s by setting Register 2［15：13］＝ 100.
4．Deskew Pattern：When $2[15: 13]=010$ ；this mode replaces the 14 －bit ADC output with the 01010101010101 word．
5．Sync Pattern：When $2[15: 13]=001$ ，the normal ADC output is replaced by a fixed 11111110000000 word．
6．Toggle：When $2[15: 13]=101$ ，the normal ADC output is alternating between 1 s and 0 s ．The start state of ADC word can be either 1 s or 0 s ．
7．Custom Pattern：It can be enabled when $2[15: 13]=011$ ．Users can write the required VALUE into register bits＜CUSTOM PATTERN＞，which is Register 5［13：0］．Then，the device will output VALUE at its outputs， about 3 to 4 ADC clock cycles after the $24^{\text {th }}$ rising edge of SCLK．So，the time taken to write one value is 24 SCLK clock cycles＋ 4 ADC clock cycles．To change the customer pattern value，users can repeat writing Register $5[13: 0]$ with a new value．Due to the speed limit of SPI，the refresh rate of the custom pattern may not be high．For example， 128 points custom pattern takes approximately $128 \times(24$ SCLK clock cycles +4 ADC clock cycles）．

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## 注

Only one of the above patterns can be active at any given instant．
Digital demodulator should be disabled，i．e．Register 0x16＝1．

## 10．6．1．2．12 SYNC＿PATTERN：Address：10［8］

By enabling this bit，all channels＇test pattern outputs are synchronized．When $10[8]$ is set as 1 ，the ramp patterns of all 8 channels start simultaneously．

## 10．6．1．3 VCA Register Map

| Address （DEC） | Address （HEX） | Default Value | Function | Description |
| :---: | :---: | :---: | :---: | :---: |
| 51［0］ | 0x33［0］ | 0 | RESERVED | Set to 0 |
| 51［3：0］ | 0x33［3：0］ | 0 | LPF＿PROGRAMMABILITY | $\begin{aligned} & \text { 1000: } 10 \mathrm{MHz} \\ & 0000: 15 \mathrm{MHz}, \\ & 0100: 20 \mathrm{MHz} \text {, } \\ & 0110: 30 \mathrm{MHz}, \\ & 0101: 35 \mathrm{MHz} \\ & 0111: 50 \mathrm{MHz} \\ & \text { Note: } 0 \times 3 \mathrm{D}[14] \text {, that is, } 5 \mathrm{MHz} \text { LPF, should be set } \\ & \text { as } 0 \text {. } \end{aligned}$ |
| 51［4］ | 0x33［4］ | 0 | PGA＿INTEGRATOR＿DISABLE （PGA＿HPF＿DISABLE） | 0：Enable <br> 1：Disable offset integrator for PGA．See the explanation for the PGA integrator function in the Application Information section |
| 51［7：5］ | 0x33［7：5］ | 0 | PGA＿CLAMP＿LEVEL | Low－noise mode：53［11：10］＝ 00 <br> 000：－2 dBFS <br> 010： 0 dBFS <br> 1XX：Clamp is disabled <br> Low－power／medium－power mode；53［11：10］＝ 01／10 <br> 100：－2 dBFS <br> 110： 0 dBFS <br> OXX：clamp is disabled <br> Note：The clamp circuit makes sure that PGA output is in linear range．For example，at 000 setting，PGA output HD3 will worsen by 3 dB at －2－dBFS ADC input．In normal operation，clamp function can be set as 000 in the low－noise mode． The maximum PGA output level can exceed 2Vpp with the clamp circuit enabled． <br> Note：In the low－power and medium－power modes， PGA＿CLAMP is disabled for saving power if 51［7］ ＝0．． <br> Note：Register 61［15］should be set as 0； otherwise，PGA＿CLAMP＿LEVEL is affected by Register 61［15］． |
| 51［13］ | 0x33［13］ | 0 | PGA＿GAIN＿CONTROL | $\begin{aligned} & 0: 24 \mathrm{~dB} \\ & 1: 30 \mathrm{~dB} \end{aligned}$ |
| 51［15：14］ | 0x33［15：14］ | 0 | RESERVED | Set to 0 |
| 52［4：0］ | 0x34［4：0］ | 0 | ACTIVE TERMINATION INDIVIDUAL＿RESISTOR＿CNTL | See 表 7．Register 52［5］should be set as 1 to access these bits |
| 52［5］ | 0x34［5］ | 0 | ACTIVE TERMINATION INDIVIDUAL＿RESISTOR＿ENABLE | 0：Disable <br> 1：Enable internal active termination individual resistor control |


| Address <br> (DEC) | Address <br> (HEX) | Default <br> Value | Function | Description |
| :--- | :--- | :--- | :--- | :--- |$|$| D2[7:6] |
| :--- |
| $0 \times 34[7: 6]$ |

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| Address （DEC） | Address （HEX） | Default Value | Function | Description |
| :---: | :---: | :---: | :---: | :---: |
| 54［6］ | 0x36［6］ | 0 | CW＿1X＿CLK＿SEL | 0：Accept CMOS clock <br> 1：Accept differential clock |
| 54［7］ | 0x36［7］ | 0 | RESERVED | Set to 0 |
| 54［8］ | 0x36［8］ | 0 | CW＿TGC＿SEL | 0：TGC mode <br> 1：CW mode <br> Note ：VCAT and PGA are still working in CW mode．They should be powered down separately through 53［12］． |
| 54［9］ | 0x36［9］ | 0 | CW＿SUM＿AMP＿ENABLE | 0 ：Enable CW summing amplifier <br> 1：Disable CW summing amplifier <br> Note：54［9］is only effective in CW mode． |
| 54［11：10］ | 0x36［11：10］ | 0 | CW＿CLK＿MODE＿SEL | 00： $16 \times$ mode <br> 01： $8 \times$ mode <br> 10： $4 \times$ mode <br> 11： $1 \times$ mode |
| 54［15：12］ | 0x36［15：12］ | 0 | RESERVED | Set to 0 |
| 55［3：0］ | 0x37［3：0］ | 0 | CH1＿CW＿MIXER＿PHASE | $0000 \rightarrow 1111$ ， 16 different phase delays，see表 11 |
| 55［7：4］ | 0x37［7：4］ | 0 | CH2＿CW＿MIXER＿PHASE |  |
| 55［11：8］ | 0x37［11：8］ | 0 | CH3＿CW＿MIXER＿PHASE |  |
| 55［15：12］ | 0x37［15：12］ | 0 | CH4＿CW＿MIXER＿PHASE |  |
| 56［3：0］ | 0x38［3：0］ | 0 | CH5＿CW＿MIXER＿PHASE |  |
| 56［7：4］ | 0x38［7：4］ | 0 | CH6＿CW＿MIXER＿PHASE |  |
| 56［11：8］ | 0x38［11：8］ | 0 | CH7＿CW＿MIXER＿PHASE |  |
| 56［15：12］ | 0x38［15：12］ | 0 | CH8＿CW＿MIXER＿PHASE |  |
| 57［1：0］ | 0x39［1：0］ | 0 | CH1＿LNA＿GAIN＿CNTL | $\begin{aligned} & \text { 00: } 18 \mathrm{~dB} \\ & 01: 24 \mathrm{~dB} \\ & \text { 10: } 15 \mathrm{~dB} \\ & \text { 11: Reserved } \\ & \text { REG52[15] should be set as } 1 . \end{aligned}$ |
| 57［3：2］ | 0x39［3：2］ | 0 | CH2＿LNA＿GAIN＿CNTL |  |
| 57［5：4］ | 0x39［5：4］ | 0 | CH3＿LNA＿GAIN＿CNTL | $\begin{aligned} & \text { 00: } 18 \mathrm{~dB} \\ & \text { 01: } 24 \mathrm{~dB} \\ & \text { 10: } 15 \mathrm{~dB} \\ & \text { 11: Reserved } \\ & \text { REG52[15] should be set as } 1 . \end{aligned}$ |
| 57［7：6］ | 0x39［7：6］ | 0 | CH4＿LNA＿GAIN＿CNTL |  |
| 57［9：8］ | 0x39［9：8］ | 0 | CH5＿LNA＿GAIN＿CNTL |  |
| 57［11：10］ | 0x39［11：10］ | 0 | CH6＿LNA＿GAIN＿CNTL |  |
| 57［13：12］ | 0x39［13：12］ | 0 | CH7＿LNA＿GAIN＿CNTL |  |
| 57［15：14］ | 0x39［15：14］ | 0 | CH8＿LNA＿GAIN＿CNTL |  |
| 59［1：0］ | 0x3B［1：0］ | 0 | RESERVED | Set to 0 |
| 59［3：2］ | 0x3B［3：2］ | 0 | HPF＿LNA | $\begin{aligned} & \text { 00: } 100 \mathrm{kHz} \\ & 01: 50 \mathrm{kHz} \\ & \text { 10: } 200 \mathrm{kHz} \\ & \text { 11: } 150 \mathrm{kHz} \text { with } 0.015 \mu \mathrm{~F} \text { on } \mathrm{INMx} \end{aligned}$ |
| 59［6：4］ | 0x3B［6：4］ | 0 | DIG＿TGC＿ATT＿GAIN | 000：0－dB attenuation <br> 001：6－dB attenuation <br> N ：About $\mathrm{N} \times 6 \mathrm{~dB}$ attenuation when $59[7]=1$ |
| 59［7］ | 0x3B［7］ | 0 | DIG＿TGC＿ATT | 0 ：Disable digital TGC attenuator <br> 1：Enable digital TGC attenuator |
| 59［8］ | 0x3B［8］ | 0 | CW＿SUM＿AMP＿PDN | 0：Power down <br> 1：Normal operation <br> Note：59［8］is only effective in TGC test mode． |
| 59［9］ | 0x3B［9］ | 0 | PGA＿TEST＿MODE | 0 ：Normal CW operation <br> 1：PGA outputs appear at CW outputs． |
| 59［15：10］ | 0x3B［15：10］ | 0 | RESERVED | Set to 0 |
| 61［12：0］ | 0x3D［12：0］ | 0 | RESERVED | Set to 0 |


| Address （DEC） | Address （HEX） | Default Value | Function | Description |
| :---: | :---: | :---: | :---: | :---: |
| 61［13］ | 0x3D［13］ | 0 | V2I＿CLAMP | 0 ：Clamp disabled <br> 1：Clamp enabled at the V2l input．An additional voltage clamp at the V2I input．This limits the amount of overload signal the PGA sees． |
| 61［14］ | 0x3D［14］ | 0 | 5 MHz ＿LPF | 0：5－MHz LPF disabled <br> 1： $5-\mathrm{MHz}$ LPF enabled．Suppress signals $>5 \mathrm{MHz}$ or high－order harmonics．The LPF Register 51［3：1］needs to be set as 100，that is， $10 \mathbf{M H z}$ ． |
| 61［15］ | 0x3D［15］ | 0 | PGA＿CLAMP＿－6dBFS | 0：Disable the $-6-\mathrm{dBFS}$ clamp．PGA＿CLAMP is set by Reg51［7：5］． <br> 1：Enable the－6－dBFS clamp．PGA＿CLAMP Reg51［7：5］should be set as 000 in the low－ noise mode or 100 in the low－power／medium－ power mode．In this setting，PGA output HD3 will be worsen by 3 dB at $-6-\mathrm{dBFS}$ ADC input．The actual PGA output is reduced to approximately 1.5 Vpp，about 2.5 dB below the ADC full－scale input 2 Vpp ．As a result，AFE5812＇s LPF is not saturated，and it can suppress harmonic signals better at PGA output．Due to PGA output reduction，the ADC output dynamic range is impacted． <br> Note：This bit is ONLY valid when PGA＝24dB． |

## 10．6．1．4 VCA Register Description

## 10．6．1．4．1 LNA Input Impedances Configuration（Active Termination Programmability）

Different LNA input impedances can be configured through the register $52[4: 0]$ ．By enabling and disabling the feedback resistors between LNA outputs and ACTx pins，LNA input impedance is adjustable accordingly．表 6 describes the relationship between LNA gain and 52［4：0］settings．The input impedance settings are the same for both TGC and CW paths．
The AFE5812 also has four preset active termination impedances as described in 52［7：6］．An internal decoder is used to select appropriate resistors corresponding to different LNA gain．

表 6．Register 52［4：0］Description

| 52［4：0］／0x34［4：0］ | FUNCTION |
| :---: | :--- |
| 00000 | No feedback resistor enabled |
| 00001 | Enables $450-\Omega$ feedback resistor |
| 00010 | Enables $900-\Omega$ feedback resistor |
| 00100 | Enables $1800-\Omega$ feedback resistor |
| 01000 | Enables $3600-\Omega$ feedback resistor |
| 10000 | Enables $4500-\Omega$ feedback resistor |

The input impedance of AFE can be programmed through Register 52［8：0］．Each bit of Register 52［4：0］controls one active termination resistor．The following tables indicate the nominal impedance values when individual active termination resistors are selected．See Active Termination for more details．表 7 shows the corresponding impedances under different Register 52［4：0］values，while 表 8 shows the Register 52［4：0］settings under different impedances．

注
表 7 and 表 8 show nominal input impedance values．Due to silicon process variation，the actual values can vary．

表 7．Register 52［4：0］versus LNA Input Impedances

| 52［4：0］／0x34［4：0］ | $\mathbf{0 0 0 0 0}$ | $\mathbf{0 0 0 0 1}$ | $\mathbf{0 0 0 1 0}$ | $\mathbf{0 0 0 1 1}$ | $\mathbf{0 0 1 0 0}$ | $\mathbf{0 0 1 0 1}$ | $\mathbf{0 0 1 1 0}$ | 00111 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| LNA：15dB | High Z | $118 \Omega$ | $236 \Omega$ | $79 \Omega$ | $472 \Omega$ | $94 \Omega$ | $157 \Omega$ | $67 \Omega$ |

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表 7．Register 52［4：0］versus LNA Input Impedances（接下页）

| 52［4：0］／0x34［4：0］ | $\mathbf{0 0 0 0 0}$ | $\mathbf{0 0 0 0 1}$ | $\mathbf{0 0 0 1 0}$ | $\mathbf{0 0 0 1 1}$ | $\mathbf{0 0 1 0 0}$ | $\mathbf{0 0 1 0 1}$ | $\mathbf{0 0 1 1 0}$ | $\mathbf{0 0 1 1 1}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| LNA：18dB | High Z | $90 \Omega$ | $180 \Omega$ | $60 \Omega$ | $360 \Omega$ | $72 \Omega$ | $120 \Omega$ | $51 \Omega$ |
| LNA：24dB | High Z | $50 \Omega$ | $100 \Omega$ | $33 \Omega$ | $200 \Omega$ | $40 \Omega$ | $66.67 \Omega$ | $29 \Omega$ |
| 52［4：0］／0x34［4：0］ | $\mathbf{0 1 0 0 0}$ | $\mathbf{0 1 0 0 1}$ | $\mathbf{0 1 0 1 0}$ | $\mathbf{0 1 0 1 1}$ | $\mathbf{0 1 1 0 0}$ | $\mathbf{0 1 1 0 1}$ | $\mathbf{0 1 1 1 0}$ | $\mathbf{0 1 1 1 1}$ |
| LNA：15dB | $944 \Omega$ | $105 \Omega$ | $189 \Omega$ | $73 \Omega$ | $315 \Omega$ | $86 \Omega$ | $135 \Omega$ | $63 \Omega$ |
| LNA：18dB | $720 \Omega$ | $80 \Omega$ | $144 \Omega$ | $55 \Omega$ | $240 \Omega$ | $65 \Omega$ | $103 \Omega$ | $48 \Omega$ |
| LNA：24dB | $400 \Omega$ | $44 \Omega$ | $80 \Omega$ | $31 \Omega$ | $133 \Omega$ | $36 \Omega$ | $57 \Omega$ | $27 \Omega$ |
| 52［4：0］／0x34［4：0］ | 10000 | 10001 | 10010 | 10011 | $\mathbf{1 0 1 0 0}$ | $\mathbf{1 0 1 0 1}$ | $\mathbf{1 0 1 1 0}$ | $\mathbf{1 0 1 1 1}$ |
| LNA：15dB | $1181 \Omega$ | $107 \Omega$ | $197 \Omega$ | $74 \Omega$ | $337 \Omega$ | $87 \Omega$ | $139 \Omega$ | $64 \Omega$ |
| LNA：18dB | $900 \Omega$ | $82 \Omega$ | $150 \Omega$ | $56 \Omega$ | $257 \Omega$ | $67 \Omega$ | $106 \Omega$ | $49 \Omega$ |
| LNA：24dB | $500 \Omega$ | $45 \Omega$ | $83 \Omega$ | $31 \Omega$ | $143 \Omega$ | $37 \Omega$ | $59 \Omega$ | $27 \Omega$ |
| 52［4：0］／0x34［4：0］ | 11000 | 11001 | 11010 | $\mathbf{1 1 0 1 1}$ | $\mathbf{1 1 1 0 0}$ | $\mathbf{1 1 1 0 1}$ | $\mathbf{1 1 1 1 0} \Omega$ | $\mathbf{1 1 1 1 1 1}$ |
| LNA：15dB | $525 \Omega$ | $96 \Omega$ | $163 \Omega$ | $68 \Omega$ | $249 \Omega$ | $80 \Omega$ | $121 \Omega$ | $60 \Omega$ |
| LNA：18dB | $400 \Omega$ | $73 \Omega$ | $124 \Omega$ | $52 \Omega$ | $189 \Omega$ | $61 \Omega$ | $92 \Omega$ | $46 \Omega$ |
| LNA：24dB | $222 \Omega$ | $41 \Omega$ | $69 \Omega$ | $29 \Omega$ | $105 \Omega$ | $34 \Omega$ | $51 \Omega$ | $25 \Omega$ |

表 8．LNA Input Impedances versus Register 52［4：0］

| Z（ $\Omega$ ） | LNA：15dB | LNA：18dB | LNA：24dB | Z（ $\Omega$ ） | LNA：15dB | LNA：18dB | LNA：24dB | Z（ $\Omega$ ） | LNA：15dB | LNA：18dB | LNA：24dB |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 |  |  | 11111 | 67 | 00111 | 10101 |  | 139 | 10110 |  |  |
| 27 |  |  | $\begin{array}{\|l\|} \hline 10111 / 011 \\ 11 \end{array}$ | 68 | 11011 |  |  | 143 |  |  | 10100 |
| 29 |  |  | $\begin{aligned} & 00111 / 110 \\ & 11 \end{aligned}$ | 69 |  |  | 11010 | 144 |  | 01010 |  |
| 31 |  |  | $\begin{array}{\|l\|} \hline 01011 / 100 \\ 11 \end{array}$ | 72 |  | 00101 |  | 150 |  | 10010 |  |
| 33 |  |  | 00011 | 73 | 01011 | 11001 |  | 157 | 00110 |  |  |
| 34 |  |  | 11101 | 74 | 10011 |  |  | 163 | 11010 |  |  |
| 36 |  |  | 01101 | 79 | 00011 |  |  | 176 |  |  |  |
| 37 |  |  | 10101 | 80 | 11101 | 01001 | 01010 | 180 |  | 00010 |  |
| 40 |  |  | 00101 | 81 |  |  |  | 189 | 01010 | 11100 |  |
| 41 |  |  | 11001 | 82 |  | 10001 |  | 197 | 10010 |  |  |
| 44 |  |  | 01001 | 83 |  |  | 10010 | 200 |  |  | 00100 |
| 45 |  |  | 10001 | 86 | 01101 |  |  | 222 |  |  | 11000 |
| 46 |  | 11111 |  | 87 | 10101 |  |  | 236 | 00010 |  |  |
| 48 |  | 01111 |  | 90 |  | 00001 |  | 240 |  | 01100 |  |
| 49 |  | 10111 |  | 92 |  | 11110 |  | 249 | 11100 |  |  |
| 50 |  |  | 00001 | 94 | 00101 |  |  | 257 |  | 10100 |  |
| 51 |  |  | $\begin{array}{\|l} \hline 00111 / 111 \\ 10 \end{array}$ | 96 | 11001 |  |  | 315 | 01100 |  |  |
| 52 |  | 11011 |  | 100 |  |  | 00010 | 337 | 10100 |  |  |
| 55 |  | 01011 |  | 103 |  | 01110 |  | 360 |  | 00100 |  |
| 56 |  | 10011 |  | 105 | 01001 |  | 11100 | 400 |  | 11000 | 01000 |
| 57 |  |  | 01110 | 106 |  | 10110 |  | 472 | 00100 |  |  |
| 59 |  |  | 10110 | 107 | 10001 |  |  | 500 |  |  | 10000 |
| 60 | 11111 | 00011 |  | 118 | 00001 |  |  | 525 | 11000 |  |  |
| 61 |  | 11101 |  | 120 |  | 00110 |  | 667 |  |  |  |
| 63 | 01111 |  |  | 121 | 11110 |  |  | 720 |  | 01000 |  |
| 64 | 10111 |  |  | 122 |  |  |  | 900 |  | 10000 |  |

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表 8．LNA Input Impedances versus Register 52［4：0］（接下页）

| $\mathbf{Z}(\boldsymbol{\Omega})$ | LNA：15dB | LNA：18dB | LNA：24dB | $\mathbf{Z}(\boldsymbol{\Omega})$ | LNA：15dB | LNA：18dB | LNA：24dB | $\mathbf{Z}(\boldsymbol{\Omega})$ | LNA：15dB | LNA：18dB | LNA：24dB |
| :---: | :--- | :--- | :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 65 |  | 01101 |  | 124 |  | 11010 |  | 944 | 01000 |  |  |
| 66.7 |  |  | 00110 | 133 |  |  | 01100 | 1181 | 10000 |  |  |
|  |  |  |  | 135 | 01110 |  |  |  |  |  |  |

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## 10．6．1．4．2 Programmable Gain for CW Summing Amplifier

Different gain can be configured for the CW summing amplifier through the register 54［4：0］．By enabling and disabling the feedback resistors between the summing amplifier inputs and outputs，the gain is adjustable accordingly to maximize the dynamic range of CW path．表 9 describes the relationship between the summing amplifier gain and $54[4: 0]$ settings．

表 9．Register 54［4：0］Description

| $\mathbf{5 4 [ 4 : 0 ] / 0 x 3 6 [ 4 : 0 ] ~}$ | FUNCTION |
| :---: | :--- |
| 00000 | No feedback resistor |
| 00001 | Enables $250-\Omega$ feedback resistor |
| 00010 | Enables $250-\Omega$ feedback resistor |
| 00100 | Enables $500-\Omega$ feedback resistor |
| 01000 | Enables $1000-\Omega$ feedback resistor |
| 10000 | Enables $2000-\Omega$ feedback resistor |

表 10．Register 54［4：0］vs Summing Amplifier Gain

| 54［4：0］／0x36［4：0］ | $\mathbf{0 0 0 0 0}$ | $\mathbf{0 0 0 0 1}$ | $\mathbf{0 0 0 1 0}$ | $\mathbf{0 0 0 1 1}$ | $\mathbf{0 0 1 0 0}$ | $\mathbf{0 0 1 0 1}$ | $\mathbf{0 0 1 1 0}$ | $\mathbf{0 0 1 1 1}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CW I／V Gain | N／A | 0.50 | 0.50 | 0.25 | 1.00 | 0.33 | 0.33 | 0.20 |
| $54[4: 0] / 0 \times 36[4: 0]$ | 01000 | 01001 | 01010 | $\mathbf{0 1 0 1 1}$ | $\mathbf{0 1 1 0 0}$ | $\mathbf{0 1 1 0 1}$ | $\mathbf{0 1 1 1 0}$ | $\mathbf{0 1 1 1 1}$ |
| CW I／V Gain | 2.00 | 0.40 | 0.40 | 0.22 | 0.67 | 0.29 | 0.29 | 0.18 |
| $54[4: 0] / 0 \times 36[4: 0]$ | 10000 | $\mathbf{1 0 0 0 1}$ | $\mathbf{1 0 0 1 0}$ | $\mathbf{1 0 0 1 1}$ | $\mathbf{1 0 1 0 0}$ | $\mathbf{1 0 1 0 1}$ | $\mathbf{1 0 1 1 0}$ | $\mathbf{1 0 1 1 1}$ |
| CW I／V Gain | 4.00 | 0.44 | 0.44 | 0.24 | 0.80 | 0.31 | 0.31 | 0.19 |
| $\mathbf{5 4 [ 4 : 0 ] / 0 x 3 6 [ 4 : 0 ] ~}$ | $\mathbf{1 1 0 0 0}$ | $\mathbf{1 1 0 0 1}$ | $\mathbf{1 1 0 1 0}$ | $\mathbf{1 1 0 1 1}$ | $\mathbf{1 1 1 0 0}$ | $\mathbf{1 1 1 0 1}$ | $\mathbf{1 1 1 1 0}$ | $\mathbf{1 1 1 1 1}$ |
| CW I／V Gain | 1.33 | 0.36 | 0.36 | 0.21 | 0.57 | 0.27 | 0.27 | 0.17 |

## 10．6．1．4．3 Programmable Phase Delay for CW Mixer

Accurate CW beamforming is achieved through adjusting the phase delay of each channel．In the AFE5812， 16 different phase delays can be applied to each LNA output．It meets the standard requirement of typical ultrasound beamformer，that is，$\frac{1}{16} \lambda$ beamformer resolution．表 9 describes the relationship between the phase delays and the register 55 and 56 settings．

表 11．CW Mixer Phase Delay vs Register Settings
CH1 to 55［3：0］，CH2 to 55［7：4］，CH3 to 55［11：8］，CH4 to 55［15：12］， CH5 to 56［3：0］，CH6 to 56［7：4］，CH7 to 56［11：8］，CH8 to 56［15：12］

| Phase Delay | Register Settings |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CHX＿CW＿MIXER＿PHASE | 0000 | 0001 | 0010 | 0011 | 0100 | 0101 | 0110 | 0111 |
| PHASE SHIFT | 0 | $22.5^{\circ}$ | $45^{\circ}$ | $67.5^{\circ}$ | $90^{\circ}$ | $112.5^{\circ}$ | $135^{\circ}$ | $157.5^{\circ}$ |
| CHX＿CW＿MIXER＿PHASE | 1000 | 1001 | 1010 | 1011 | 1100 | 1101 | 1110 | 1111 |
| PHASE SHIFT | $180^{\circ}$ | $202.5^{\circ}$ | $225^{\circ}$ | $247.5^{\circ}$ | $270^{\circ}$ | $292.5^{\circ}$ | $315^{\circ}$ | $337.5^{\circ}$ |

## 10．6．2 Digital Demodulator Register Description

表 12．Digital Demodulator Register Map ${ }^{(1)(2)(3)}$

| Register Name | Address <br> （HEX） <br> BIT［5：0］ | Address <br> （DEC） <br> BIT［5：0］ | Default | Description |
| :--- | :--- | :--- | :---: | :--- |

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表 12．Digital Demodulator Register Map ${ }^{(1)(2)(3)}$（接下页）

| Register Name | Address <br> （HEX） <br> BIT［5：0］ | Address （DEC） <br> BIT［5：0］ | Default | Description |
| :---: | :---: | :---: | :---: | :---: |
| DHPF | OA［12］ | 10［12］ | 1 | ```0= Enable first-order digital HPF. -3 dB cut off frequency is at 0.0225 * Fs / 2. Its transfer function equation is h(n)=a/b, where a=[1- 7569 / 2 }\mp@subsup{}{}{13}\mathrm{ ] and b = [1 -1]; 1 = Disable first-order digital HPF.``` |
| OUTPUT＿CHANNEL＿SEL | 0A［11］ | 10［11］ | 0 | Swap channel pairs．It is used in 4 LVDS bypass configuration to select which of the two possible data streams to pass on．See 表 11. |
| SIN＿COS＿RESET＿ON＿TX ＿TRIG | OA［10］ | 10［10］ | 1 | $\begin{aligned} & 0=\text { Continuous phase } \\ & 1=\text { Reset down conversion phase on TX_TRIG } \end{aligned}$ |
| FULL＿LVDS＿MODE | OA［9］ | 10［9］ | 0 | $\begin{aligned} & 0=\text { Use } 4 \text { LVDS lines }(1,3,5,7) \\ & 1=\text { Use } 8 \text { LVDS lines ( } 1 \text { through } 8 \text { ) } \end{aligned}$ <br> Note： 4 LVDS mode valid only for decimation factors $\geq 4$ ．See 表 14. |
| RESERVED | OA［8：5］ | 10［8：5］ | 0 | Must set to 0 |
| RESERVED | OA［4］ | 10［4］ | 0 | Must set to 1 |
| DEC＿BYPASS | OA［3］ | 10［3］ | 0 | $0=$ Enable decimation filter 1 ＝Bypass decimation filter |
| DWN＿CNV＿BYPASS | OA［2］ | 10［2］ | 0 | 0 ＝Enable down conversion block <br> 1 ＝Bypass down conversion block．Note：the decimation filter can still be used when the down conversion block is bypassed． |
| RESERVED | 0A［1］ | 10［1］ | 1 | Must set to 1 |
| DC＿REMOVAL＿BYPASS | OA［0］ | 10［0］ | 0 | $\begin{aligned} & 0=\text { Enable DC removal block } \\ & 1=\text { Bypass DC removal block } \\ & \hline \end{aligned}$ |
| SYNC＿WORD | OB［15：0］ | 11［15：0］ | 0x2772 | LVDS sync word．When MODULATE＿BYPASS $=1$ ，there is no sync word output． |
| PROFILE＿INDX | OE［15：11］ | 14［15：11］ | 0 | Profile word selector． <br> The Profile Index register is a special 5－bit data register．Read value still uses 16－bit convention，which means data will be available on LSB $0 \mathrm{e}[4: 0]$ ） |
| DC＿REMOVAL＿1＿5 | 14［13：0］ | 20［13：0］ | 0 | 54［13：0］$\rightarrow$ DC offset for channel 1，SCID1＿SEL，SCID0＿SEL $=01$ $94[13: 0] \rightarrow$ DC offset for channel 5，SCID1＿SEL，SCIDO＿SEL＝ 10 Note：Considering the CH－to－CH DC offset variation，the offset value must be set individually．Therefore，SCID1＿SEL，SCID0＿SEL should not be set as 11 ． <br> Note：DC＿REMOVAL＿X＿X registers are write－only． |
| DC＿REMOVAL＿2＿6 | 15［13：0］ | 21［13：0］ | 0 | $55[13: 0] \rightarrow$ DC offset for channel 2，SCID1＿SEL，SCID0＿SEL $=01$ $95[13: 0] \rightarrow$ DC offset for channel 6，SCID1＿SEL，SCIDO＿SEL＝ 10 Note：Considering the CH－to－CH DC offset variation，the offset value must be set individually．Therefore，SCID1＿SEL，SCID0＿SEL should not be set as 11 ． <br> Note：DC＿REMOVAL＿X＿X registers are write－only． |
| DC＿REMOVAL＿3＿7 | 16［13：0］ | 22［13：0］ | 0 | 56［13：0］$\rightarrow$ DC offset for channel 3，SCID1＿SEL，SCID0＿SEL＝01 $96[13: 0] \rightarrow$ DC offset for channel 7，SCID1＿SEL，SCIDO＿SEL＝10 Note：Considering the CH－to－CH DC offset variation，the offset value must be set individually．Therefore，SCID1＿SEL，SCIDO＿SEL should not be set as 11 ． <br> Note：DC＿REMOVAL＿X＿X registers are write－only． |
| DC＿REMOVAL＿4＿8 | 17［13：0］ | 23［13：0］ | 0 | 57［13：0］$\rightarrow$ DC offset for channel 4，SCID1＿SEL，SCID0＿SEL $=01$ 97［13：0］$\rightarrow$ DC offset for channel 8，SCID1＿SEL，SCIDO＿SEL＝ 10 <br> Note：Considering the CH－to－CH DC offset variation，the offset value must be set individually．Therefore，SCID1＿SEL，SCIDO＿SEL should not be set as 11 ． <br> Note：DC＿REMOVAL＿X＿X registers are write－only． |
| DEC＿SHIFT＿FORCE＿EN | 1D［7］ | 29［7］ | 0 | $0=$ Profile vector specifies the number of bit to shift for the decimation filter output． <br> 1 ＝Register 1D［6：4］specifies the number of bit to shift for the decimation filter output． |
| DEC＿SHIFT＿FORCE | 1D［6：4］ | 29［6：4］ | 0 | Specify that the decimation filter output is right－shifted by $(20-N)$ bit， $\mathrm{N}=0 \times 1 \mathrm{D}[6: 4] . \mathrm{N}=0$ ，minimal digital gain； $\mathrm{N}=7$ maximal digital gain； additional $12-\mathrm{dB}$ digital gain can be applied by setting DEC＿SHIFT＿SCALE $=1$ ，that is， $0 \times 0 \mathrm{~A}[13]=1$ |

表 12．Digital Demodulator Register Map ${ }^{(1)(2)(3)}$（接下页）

| Register Name | Address （HEX） BIT［5：0］ | Address （DEC） <br> BIT［5：0］ | Default | Description |
| :---: | :---: | :---: | :---: | :---: |
| TM＿COEFF＿EN | 1D［3］ | 29［3］ | 0 | 1 ＝Set coefficient output test mode |
| TM＿SINE＿EN | 1D［2］ | 29［2］ | 0 | 1 ＝Set sine output mode；the sine waveform specifications can be configured through register $0 \times 1 \mathrm{E}$ ． |
| RESERVED | 1D［1］ | 29［1］ | 0 | Must set to 0 |
| RESERVED | 1D［0］ | 29［0］ | 0 | Must set to 0 |
| TM＿SINE＿DC | 1E［15：9］ | 30［15：9］ | 0 | 7－bit signed value for sine wave DC offset control． |
| TM＿SINE＿AMP | 1E［8：5］ | 30［8：5］ | 0 | 4－bit unsigned value，controlling the sine wave amplitude（powers of two），from unity to the full scale of 14 bit，including saturation． $0=$ No sine（only DC） |
| TM＿SINE＿STEP | 1E［4：0］ | 30［4：0］ | 0 | 5 －bit unsigned value，controlling the sine wave frequency with resolution of $\mathrm{Fs} / 2^{6}$ ，which is 0.625 MHz for $40-\mathrm{MHz}$ ADC clock． |
| MANUAL＿COEFF＿START＿ EN | 1F［15］ | 31［15］ | 0 | $0=$ The starting address of the coefficient RAM is set by the profile vector，that is，the starting address is set manually． <br> $1=$ The starting address of the coefficient RAM is set by the register $0 \times 1 F[14: 7]$ ． |
| MANUAL＿COEFF＿START ADDR | 1F［14：7］ | 31［14：7］ | 0 | When $0 \times 1 \mathrm{~F}[15]$ is set，the starting address of coefficient RAM is set by these 8 bits． |
| MANUAL＿DEC＿FACTOR＿ EN | 1F［6］ | 31［6］ | 0 | $0=$ The decimation factor is set by profile vector． <br> $1=$ The decimation factor is set by the register $0 \times 1 \mathrm{~F}[5: 0]$ ． |
| MANUAL＿DEC＿FACTOR | 1F［5：0］ | 31［5：0］ | 0 | When $0 \times 1 \mathrm{~F}[6]$ is set，the decimation factor is set by these 6 bits． Note：It is from 1 to 32 ． |
| MANUAL＿FREQ＿EN | 20［0］ | 32［0］ | 0 | $0=$ The down convert frequency is set by profile vector． <br> $1=$ The down convert frequency is set by the register $0 \times 21[15: 0]$ ． |
| MANUAL＿FREQ | 21［15：0］ | 33［15：0］ | 0 | When $0 \times 20[0]$ is set，the value of manual down convert frequency is calculated as $\mathrm{N} \times \mathrm{Fs} / 2^{16}$ |

表 13．Configuring Data Output：

| Register Name | SPI Address |
| :--- | :--- |
| SERZ＿FACTOR | $0 \times 03[14: 13]$ |
| OUTPUT＿RESOLUTION | $0 \times 03[11: 9]$ |
| MSB＿FIRST | $0 \times 04[4]$ |
| OUT＿MODE | $0 \times 02[15: 13]$ |
| CUSTOM＿PATTERN | $0 \times 05[15: 0]$ |
| OUTPUT＿CHANNEL＿SEL | $0 \times 0 \mathrm{~A}[11]$ |
| MODULATE＿BYPASS | $0 \times 0 \mathrm{~A}[14]$ |
| FULL＿LVDS＿MODE | $0 \times 0 \mathrm{~A}[9]$ |

1．Serializer configuration：
－Serialization Factor 0x03［14：13］：It can be set using demodulator register SERZ＿FACTOR．Default serialization factor for the demodulator is $16 \times$ ．However，the actual LVDS clock speed can be set by the serialization factor in the ADC SPI interface as well；the ADC serialization factor is adjusted to $14 \times$ by default．Therefore，it is necessary to sync these two settings when the demodulator is enabled，that is，set the ADC register $0 \times 03[14: 13]=01$ ．
－Output Resolution $0 \times 03[11: 9]$ ：In the default setting，it is 14 bits．The demodulator output resolution depends on the decimation factor．16－bit resolution can be used when higher decimation factor is selected．
－For RF mode（passing 14 bits only），demodulator serialization factor can be changed to $14 \times$ by setting demodulator register 0xC3［14：13］to 10.
2．Channel selection：
－Using register MODULATE＿BYPASS $0 \times 0 \mathrm{~A}[14]$ ，channel output mode can be selected as IQ modulated or single－channel I or Q output．
－Channel output is also selected using registers OUTPUT＿CHANNEL＿SEL 0x0A［11］and FULL＿LVDS＿MODE 0x0A［9］and decimation factor．
－Each of the two demodulator subchips in a device has four channels named A，B，C，and D．

## 注

After decimation，the LVDS FCLK rate keeps the same as the ADC sampling rate． Considering the reduced data amount，zeros are appended after I and Q data and ensure the LVDS data rate matches the LVDS clock rate．For detailed information about channel multiplexing，see 表14．In the table，A．I refers to CHA in－phase output，and A．Q refers to CHA quadrature output．For example，$M=3$ ，the valid data output rate is Fs／ 3 for both I and Q channels，that is $2 \times \mathrm{Fs} / 3$ bandwidth is occupied．The left Fs／ 3 bandwidth is then filled by M－2 zeros．As a result，the demod LVDS output data are A．I，A．Q，0，A．I A．Q 0 after SYNC＿WORD，FCLK $=$ Fs and DCLK $=$ Fs $\times 8$ ．When two ADC CHs＇data are transferred by one LVDS lane，M－4 zeros are filled after A．I，A．Q，B．I，and B．Q．See more details in 表 14 and 图 89.

表14．Channel Selection ${ }^{(1)}$

| Decimation Factor（M） | Modulate Bypass | Output Channel Select | Full LVDS Mode | Decimation Factor M | LVDS Output Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $M \geq 2$ | 0 | 0 | 0 | $\mathrm{M}<4$ | LVDS1：A．I，A．Q，（zeros） |
|  |  |  |  |  | LVDS2：B．I，B．Q，（zeros） |
|  |  |  |  |  | LVDS3：C．I，C．Q，（zeros） |
|  |  |  |  |  | LVDS4：D．I，D．Q，（zeros） |
|  |  |  |  | $M \geq 4$ | LVDS1：A．I，A．Q，B．I，B．Q，（zeros）LVDS2：idle |
|  |  |  |  |  | LVDS3：C．I，C．Q，D．I，D．Q，（zeros）LVDS4：idle |
|  |  |  | 1 | X | LVDS1：A．I，A．Q，（zeros） |
|  |  |  |  |  | LVDS2：B．I，B．Q，（zeros） |
|  |  |  |  |  | LVDS3：C．I，C．Q，（zeros） |
|  |  |  |  |  | LVDS4：D．I，D．Q，（zeros） |
|  |  | 1 | 0 | $\mathrm{M}<4$ | LVDS1：B．I，B．Q，（zeros） |
|  |  |  |  |  | LVDS2：A．I，A．Q，（zeros） |
|  |  |  |  |  | LVDS3：D．I，D．Q，（zeros） |
|  |  |  |  |  | LVDS4：C．l，C．Q，（zeros） |
|  |  |  |  | $\mathrm{M} \geq 4$ | LVDS1：B．I，B．Q，A．I，A．Q，（zeros） |
|  |  |  |  |  | LVDS2：idle |
|  |  |  |  |  | LVDS3：D．I，D．Q，C．I，C．Q，（zeros） |
|  |  |  |  |  | LVDS4：idle |
|  |  |  | 1 | X | LVDS1：B．I，B．Q，（zeros） |
|  |  |  |  |  | LVDS2：A．I，A．Q，（zeros） |
|  |  |  |  |  | LVDS3：D．I，D．Q，（zeros） |
|  |  |  |  |  | LVDS4：C．I，C．Q，（zeros） |
| $M \geq 2$ | 1 | 0 | X | X | LVDS1：A．I；Note：the same A．I is repeated by M times． |
|  |  |  |  |  | LVDS2：A．Q；Note：the same A．Q is repeated by $M$ times． |
|  |  |  |  |  | LVDS3：C．I；Note：the same C．I is repeated by M times． |
|  |  |  |  |  | LVDS4：C．Q；Note：the same C．Q is repeated by M times． |
|  |  | 1 | X | $X$ | LVDS1：B．I；Note：the same B．I is repeated by M times． |
|  |  |  |  |  | LVDS2：B．Q；Note：the same B．Q is repeated by M times． |
|  |  |  |  |  | LVDS3：D．I；Note：the same D．I is repeated by M times． |
|  |  |  |  |  | LVDS4：D．Q；Note：the same D．Q is repeated by M times． |
| $\mathrm{M}=1$ | 0 | 0 | X | 1 | LVDS1：A．I；LVDS2：B．I；LVDS3：C．I；LVDS4：D．I |
| $\mathrm{M}=1$ | 0 | 1 | X | 1 | LVDS1：B．I；LVDS2：A．I；LVDS3：D．I；LVDS4：C．I |
| $\mathrm{M}=1$ | 1 | 0 | X | 1 | LVDS1：A．I；LVDS2：A．Q；LVDS3：C．I；LVDS4：C．Q |
| $\mathrm{M}=1$ | 1 | 1 | X | 1 | LVDS1：B．I；LVDS2：B．Q；LVDS3：D．I；LVDS4：D．Q |

（1）This table refers to individual demodulator subchip，which has four LVDS outputs，that is LVDS1 through LVDS4；and four input CHs， that is CH．A to CH．D．See 图 86.


图 89．Output Data Format at $M=3 \sim 5$
3．Output mode：
－Using register OUT＿MODE，ramp pattern and custom pattern can be enabled．
－Custom pattern：In the case of a custom pattern，custom pattern value can be set using register CUSTOM＿PATTERN．Note：LSB always comes out first regardless of whether $0 \times 04[4]=0$ or 1 ，that is， MSB＿FIRSTT $=0$ or 1 ．
－Ramp pattern：Demodulator generated ramp pattern includes information of chip＿id as well． 8 MSB（that is，Data［15．．8］）bits are ramp pattern．Next 5 bits（that is，Data［3．．7］）gives value of chip ID．Data［2］ corresponds to subchip ID， 0 or 1；Data［1：0］are filled with zeros．

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## 10．6．2．1 Common Demod Registers

表 15．DC Removal Block

| Register Name | SPI Address |
| :--- | :--- |
| DC＿REMOVAL＿BYPASS | $0 \times 0$ A［0］ |
| DC＿REMOVAL＿1＿5 | $0 \times 14[13: 0]$ |
| DC＿REMOVAL＿2＿6 | $0 \times 15[13: 0]$ |
| DC＿REMOVAL＿3＿7 | $0 \times 16[13: 0]$ |
| DC＿REMOVAL＿4＿8 | $0 \times 17[13: 0]$ |

－DC removal block can be bypassed using the register bit DC＿REMOVAL＿BYPASS．
－DC removal is designed to be done manually．
－Manual DC offset removal：Registers DC＿REMOVAL＿1＿5，DC＿REMOVAL＿2＿6，DC＿REMOVAL＿3＿7，and DC＿REMOVAL＿4＿8 can be used to give manual offset．Value should be given in 2＇s complement format．In the case of these registers，SCID values should be given accordingly（see SPI for Demodulator for more information）．Example：For DC offset of channel 5，the address of the register would be 0x91（in hex）．Here SCID0 is 0 and SCID1 is 1 ．

表 16．Down Conversion Block

| Register Name | SPI Address |
| :--- | :--- |
| DWN＿CNV＿BYPASS | $0 \times 0 \mathrm{~A}[2]$ |
| SIN＿COS＿RESET＿ON＿TX＿TRIG | $0 \times 0 \mathrm{~A}[10]$ |
| MANUAL＿FREQ＿EN | $0 \times 20[0]$ |
| MANUAL＿FREQ | $0 \times 21[15: 0]$ |

－Down conversion block can be bypassed using register DWN＿CNV＿BYPASS．
－Down conversion frequency can be given using the down conversion frequency（ $f$ ）parameter of the profile vector．Alternatively，manual registers MANUAL＿FREQ＿EN and MANUAL＿FREQ can be used to provide down conversion frequency．
－Down conversion frequency $(f)$ ：＇$f$＇can be set with resolution Fs／ $2^{16}$（where Fs is the sampling frequency）． An integer value of＇ $2^{16} f$／$F s^{\prime}$＇is given to the profile vector or respective register．
－Down conversion signal can be configured to be reset at each TX＿TRIG pulse．This facility can be enabled using SIN＿COS＿RESET＿ON＿TX＿TRIG．

表 17．Decimation Block

| Register Name | SPI Address |
| :--- | :--- |
| DEC＿BYPASS | $0 \times 0 \mathrm{~A}[3]$ |
| MANUAL＿DEC＿FACTOR＿EN | $0 \times 1 \mathrm{~F}[6]$ |
| MANUAL＿DEC＿FACTOR | $0 \times 1 \mathrm{~F}[5: 0]$ |
| MANUAL＿COEFF＿START＿EN | $0 \times 1 \mathrm{~F}[15]$ |
| MANUAL＿COEFF＿START＿ADDR | $0 \times 1 \mathrm{~F}[14: 7]$ |
| DEC＿SHIFT＿FORCE＿EN | $0 \times 1 \mathrm{D}[7]$ |
| DEC＿SHIFT＿FORCE | $0 \times 1 \mathrm{D}[6: 4]$ |
| DEC＿SHIFT＿SCALE | $0 \times 0 \mathrm{~A}[13]$ |

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－Decimation block can be bypassed using register DEC＿BYPASS．
－Decimation factor：This can be set using the decimation factor（M）parameter of the profile vector． Alternatively，it can be set using registers MANUAL＿DEC＿FACTOR＿EN and MANUAL＿DEC＿FACTOR．
－Filter coefficients：Filter coefficients should be written to coefficient RAM（see Profile RAM and Coefficient RAM）．The format of the filter coefficient is 2＇s complement．Its address pointer should be given in profile vector，or alternatively，registers MANUAL＿COEFF＿START＿EN and MANUAL＿COEFF＿START＿ADDR can be used．
－Filter digital gain：Decimation block takes 14 －bit input data and 14－bit input coefficients and gives 36 －bit output internally．While implementing this FIR filter，after multiplication and addition，the 36 －bit internal filter output should be scaled approximately to make the final demod output as 16 bit，that is，applying digital gain or attenuation．Filter gain or attenuation depends on two parameters：decimation shift scale and gain compensation factor．
－Decimation shift scale can be chosen using register DEC＿SHIFT＿SCALE．The gain compensation factor can be given to the gain compensation factor（G）parameter of the profile vector，or can be given using registers DEC＿SHIFT＿FORCE＿EN and DEC＿SHIFT＿FORCE．
－The internal 36 －bit filter output is right－shifted by N bits，where N equals：
－20－G when Dec＿Shift＿Scale $=0$
－20－G－2 when Dec＿Shift＿Scale $=1$
The minimal gain occurs when $G=0$ and DEC＿SHIFT＿SCALE $=0$ ．The total scaling range can be a factor of $2^{9}$ ，that is，approximately 54 dB ．

## 表 18．Test Modes

| Register Name | SPI Address |
| :--- | :--- |
| TM＿SINE＿DC | $0 \times 1 \mathrm{E}[15: 9]$ |
| TM＿SINE＿AMP | $0 \times 1 \mathrm{E}[8: 5]$ |
| TM＿SINE＿STEP | $0 \times 1 \mathrm{E}[4: 0]$ |
| TM＿SINE＿EN | $0 \times 1 \mathrm{D}[2]$ |
| TM＿COEFF＿EN | $0 \times 1 \mathrm{D}[3]$ |

1．Sine test mode：
The normal ADC output can be replaced by：

$$
\begin{equation*}
x_{n}=C+2^{k} \sin \left(\frac{\pi N n}{2^{5}}\right) \tag{5}
\end{equation*}
$$

－$N$ is a 5 －bit unsigned value，controlling the sine wave frequency with resolution of $F_{S} / 2^{6}$ ，which is 0.625 MHz for $40-\mathrm{MHz}$ ADC clock．
－$k$ is 4 －bit unsigned value，controlling the wave amplitude，from unity to the full scale of 14 bits，including saturation．
－C is 7－bit signed value for DC offset control．
The controlling values fit into one 16－bit register．This test pattern shall allow testing of demodulation， decimation filter，DC removal，gain control，and so on．
2．Coefficient output test mode：
－The input to the decimating filter can be replaced with a sequence of one impulse and zero samples， where one impulse（ $0 \times 4000$ ）is followed by $(16 \times \mathrm{M})$ zeros（that is， $0 \times 0000$ ）．
－This mode is useful to check decimation filter coefficients．
－This mode can be enabled using register TM＿COEFF＿EN．
3．RF mode：
RF mode allows for the streaming of ADC data through the demodulator to the LVDS．Note：Test pattern from the ADC output stage cannot be sent to the demodulator（it can only be sent to the LVDS when the demodulator is off）．RF mode without sync word can be set by the following：
（a）Configure the ADC Serialization rate as 16bit，by setting ADC register 03［14：13］＝01B．
（b）Write $0 \times 0041$ to demod register $0 \times D F$ ；that is MANUAL＿DEC＿FACTOR＿EN $=1$ and MANUAL＿DEC＿FACTOR $=1$ ．
（c）Write 0x121F to demod register 0xCA，that is，MODULATE＿BYPASS $=0$ ，FULL＿LVDS＿MODE $=1$ ， DC＿REMOVAL＿BYPASS $=1$ ，DWN＿CNV＿BYPASS $=1$ DEC＿BYPASS $=1$ ， SYN＿COS＿RESET＿ON＿TX＿TRIG $=0$ ．
（d）Write $0 \times 6800$ to demod register $0 \times C 3$ ，that is，SERZ＿FACTOR $=16 \times$ ，OUTPUT＿RESOLUTION $=16 \times$ ，
（e）Write $0 \times 0010$ to demod register $0 \times C 4$ ，that is，MSB＿FIRST $=1$
（f）Provide TX＿TRIG pulse or set demod register 0xC0［2］MANUAL＿TX＿TRIG
（g）Note：For $\bar{R}$ F mode（passing 14 bits only），demodulator serialization factor can be changed to $14 \times$ by setting demodulator register $0 \times \mathrm{C} 3[14: 13]$ to 10 B and ADC register 03［14：13］＝0．

## 10．6．2．2 Profile RAM and Coefficient RAM

Writing data to profile RAM and coefficient RAM is similar to registers．Both RAMs do not get reset after resetting the device．RAM does not have default values，so it is necessary to write required values to RAM．RAM address values need to be given to the pointer register that points to the location wherever data needs to be written． Because both RAMs are part of the demodulator，SPI＿DIG＿EN should be low while writing．

## 注

TI recommends to program the RAMs before configuring other registers．
PROFILE＿INDX Reg． $0 \times 0$ E［15：11］must be reprogrammed in order to make profile and filter RAM correctly loaded．
A trigger is required to make new settings effective，such as profile RAM，coefficient RAM， and PROFILE＿INDX Reg．0x0E［15：11］－either an external trigger event through the TX＿SYNC＿IN pin or a manual trigger event through Register 0［2］．
ADC CLK is required during demod register，profile and coefficent RAM programming．

表 19．Profile Related Registers

| Register Name | SPI Address |
| :--- | :--- |
| PROFILE＿MEM＿ADDR＿WR | $0 \times 08[4: 0]$ |
| PROFILE＿BANK | $0 \times 09[63: 0]$ |
| PROFILE＿INDEX | $0 \times 0 E[15: 11]$ |

－Profile RAM can store up to 32 vectors／profiles．Each vector／profile has 64 bits．
－Pointer value should be given to the register PROFILE＿MEM＿ADDR＿WR before writing to RAM．
－The 64 bits of each vector／profile are arranged as follows：
表20．Profile RAM ${ }^{(1)(2)}$

| Name of Parameter | Address | Description |
| :--- | :--- | :--- |
| Reserved | RAM［63：50］ | Set as 0 |
| Reserved | RAM［49：36］ | Set as 0 |
| Pointer to coeff memory $(P)^{(3)}$ | RAM［35：28］ | A pointer to filter coefficient memory（8 bits），pointing to 8 coefficient <br> blocks．The relevant coefficients start from address $\mathrm{P} \times 8$ in the <br> coefficients memory and will continue for M blocks． |
| Decimation Factor $(\mathrm{M})^{(3)}$ | Recimation factor for decimation block |  |
| Down conversion frequency $(f)^{(3)}$ | RAM［21：6］ | Down conversion frequency for down conversion block |
| Reserved | RAM［5］ | Set as 0 |
| Gain compensation factor $(G)^{(3)}$ | RAM［4：2］ | Gain compensation factor parameter for decimation block |
| 2 LSBs | RAM［1：0］ | Set as 0 |

（1） 2 LSB＇s（that is，RAM［1：0］）are ignored and can be set as zeros．
（2）A particular profile vector can be activated using register PROFILE＿INDEX．Address pointing to the location of particular vector is to be given in PROFILE＿INDEX．
（3）Alternative manual register is available

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## 10．6．2．2．1 Programming the Profile RAM

1．Set SEN and SPI＿DIG＿EN as 0 ．
2．Set SPI address $0 x \mathrm{C} 8[4: 0]$ with the base address，for example $0 \times 0000$ ． $0 \times \mathrm{C} 8$ means both demodulator subchips are enabled．
3．The 64 profile vector bits are arranged as following：
－RAM［63：50］$=0$（reserved）
－RAM［49：36］＝ 0 （reserved）
－RAM［35：28］＝Pointer to coeff memory（8 bit）
－RAM［27：22］＝Decimation factor（6 bit）
－RAM［21：6］＝Demodulation frequency（16 bit）
－RAM［5］＝ 0
－RAM［4：2］＝Gain compensation factor（3 bit）
－RAM［1：0］＝ 2 LSBs are ignored，can be set as zeros．
4．Write the above 64 bits to SPI address 0xC9（MSB first）．
5．Repeat steps 3 and 4 for the following profile entries（the address in register $0 x C 8$ auto increments）．
6．Set SEN and SPI＿DIG＿EN as 1 ．

## 10．6．2．2．2 Procedure for Configuring Next Vector

1．Write profile index（5 bits）to SPI address $0 x C E[15: 11]$ ．OxCE means both demodulator subchips are enabled．

表 21．Filter Coefficient RAM

| Register Name | SPI Address |
| :--- | :--- |
| COEFF＿MEM＿ADDR＿WR | $0 \times 06[7: 0]$ |
| COEFF＿BANK | $0 \times 07[111: 0]$ |
| MANUAL＿COEFF＿START＿ADDR | $0 \times 1 \mathrm{~F}[14: 7]$ |
| MANUAL＿COEFF＿START＿EN | $0 \times 1 \mathrm{~F}[15]$ |

－Coefficient RAM can store up to 256 coefficient memory blocks．The size of each block is 112 bits．
－Pointer value should be given to the register COEFF＿MEM＿ADDR＿WR before writing to RAM．
－Write 112 bits to SPI address $0 \times C 7$（MSB first）．Each coefficient memory block consists of eight 14－bit coefficients which are aligned in the following manner：coefficient order from right to left and bit order from right to left）．
－Note：The coefficients are in 2＇s complement format．
表 22．Coefficient RAM Mapping ${ }^{(1)}$

| Coeff 7［13：0］ | Coeff 6［13：0］ | Coeff 5［13：0］ | Coeff 4［13：0］ | Coeff 3［13：0］ | Coeff 2［13：0］ | Coeff 1［13：0］ | Coeff 0［13：0］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $111: 98$ | $97: 84$ | $83: 70$ | $69: 56$ | $55: 42$ | $41: 28$ | $27: 14$ | $13: 0$ |

（1）Note that SPI serialization is done from left to right（ $0 x$ Coeff $7[13]$ first and $0 x$ Coeff $0[0]$ last）．
－Because the decimation block uses $16 \times \mathrm{M}$ tap FIR filter and filter coefficients are symmetric，only half（that is $8 \times \mathrm{M}$ ）filter coefficients are necessary to be stored（ M is the decimation factor）．Each 8 coefficient block that is written to the memory represents a single phase of a polyphase filter．Therefore，the relation between the filter coefficients Cn and their index（ $\mathrm{i}, \mathrm{j}$ ）in the coefficients memory is given by：
$\mathrm{n}=\mathrm{M} \times(1+\mathrm{I})-(1+\mathrm{j})$
where
－I is the index in the coefficients block，from 0 to 7.
－$j$ is the block index，from 0 to（ $M-1$ ）．

Example for $\mathrm{M}=4$
表 23．Coefficient RAM Mapping

| $\mathbf{j l I}$ | $\mathbf{7}$ | $\mathbf{6}$ | $\mathbf{5}$ | $\mathbf{4}$ | $\mathbf{3}$ | $\mathbf{2}$ | $\mathbf{1}$ | $\mathbf{0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | Coeff 31 | Coeff 27 | Coeff 23 | Coeff 19 | Coeff 15 | Coeff 11 | Coeff 7 | Coeff 3 |
| 1 | Coeff 30 | Coeff 26 | Coeff 22 | Coeff 18 | Coeff 14 | Coeff 10 | Coeff 6 | Coeff 2 |
| 2 | Coeff 29 | Coeff 25 | Coeff 21 | Coeff 17 | Coeff 13 | Coeff 9 | Coeff 5 | Coeff 1 |
| 3 | Coeff 28 | Coeff 24 | Coeff 20 | Coeff 16 | Coeff 12 | Coeff 8 | Coeff 4 | Coeff 0 |

－Coefficient start address can be given using the Pointer to Coeff Memory（ P ）parameter of profile RAM． Alternatively，the start address can be given using register MANUAL＿COEFF＿START＿ADDR．（While using this register，register enable bit MANUAL＿COEFF＿START＿EN should be set to 1．）

## 10．6．2．2．3 Programming the Coefficient RAM

1．Set SPI address $0 x C 6[7: 0]$ with the base address，for example $0 \times 0000$ ． $0 x \mathrm{C} 6$ means both demodulator subchips are enabled．
2．Write 112 bits to SPI address 0xC7（MSB first）．Each coefficient memory word consists of eight 14－bit coefficients，which are aligned in the following manner：coefficient order from right to left and bit order from right to left．Note：The coefficients are in 2＇s complement format．

图 90.

| Coeff 7［13：0］ | Coeff 6［13：0］ | Coeff 5［13：0］ | Coeff 4［13：0］ | Coeff 3［13：0］ | Coeff 2［13：0］ | Coeff 1［13：0］ | Coeff 0［13：0］ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $111: 98$ | $97: 84$ | $83: 70$ | $69: 56$ | $55: 42$ | $41: 28$ | $27: 14$ | $13: 0$ |

注
Note that SPI serialization is done from left to right（Coeff $7[13]$ first and Coeff $0[0]$ last）．
3．Repeat the previous step for the following coefficient bulk entries（the address in register 0xC6 auto increments）．

## 10．6．2．2．4 Filter Coefficent Test Mode

Coefficient test mode allows for the streaming of coefficients through the demodulator to the LVDS．Filter coefficient test mode can be set by the following：
1．Enable TM＿COEFF＿EN．
2．Write OUTPUT＿RESOLUTION $(0 x 03[11: 9])=0 b 100$ ，that is， 16 －bit output．（Note that output bit resolution of 14 bits will not give proper result．）
3．Write DC＿REMOVAL＿BYPASS $(0 \times 0 A[0])=1, D W N \_C N V \_B Y P A S S ~(0 \times 0 A[2])=1$ ．
4．Write DC＿DEC＿SHIFT＿FORCE＿EN $(0 x 1 D[7])=1$ ，DEC＿SHIFT＿FORCE（0x1D［6：4］＝0b110，and DEC＿SHIFT＿SCALE（0x0a［13］）＝ 1 ．
5．Write MODULATE＿BYPASS $(0 \times 0 A[14])=1$ ．After writing all of the above settings，coefficients come at the output in the sequence as follow．
6．$M=2$
－Address 0：C15 C13 C11 C09 C07 C05 C03 C01；Address 1：C14 C12 C10 C08 C06 C04 C02 C00
－The order in which coefficients come at the output will be： 0 C01 C03 C05 C07 C09 C11 C13 C15 C14 C12 C10 C08 C06 C04 C02 C00 C00 C02 C04 C06 C08 C10 C12 C14 C15 C13 C11 C09 C07 C05 C03 C01 0
7．$M=8$
－The coefficients come to the output as shown in 图 91.

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NOTE：When it reaches the last sample，it starts giving coefficients in the reverse direction until it reaches the point it started．
图 91．Coefficient Readout Sequence

## 10．6．2．2．5 TX＿SYNC and SYNC＿WORD Timing

As shown in 图 92，hardware TX＿SYNC is latched at the next negative edge of the ADC Clock after 0 to 1 transition of TX＿SYNC．The time gap between latched edge and the start of the LVDS SYNC＿WORD is kT ns where T is the time period of ADC clock and $\mathrm{k}=16+$ decFactor $+1 . \mathrm{t}_{\text {SETUP }}$ and $\mathrm{t}_{\text {HOLD }}$ can be considered as 1.5 ns in the normal condition．Both are at the negative edge of the ADC clock．


图 92．Sync Word Generation With Respect to TX＿TRIG when DC＿REMOVAL＿BYPASS 10［0］＝ 0

## 10．6．2．2．6 FIR Filter Delay versus TX＿TRIG Timing

AFE5812＇s decimation filter is a symmetric $M \times 16$－order FIR filter，where $M$ is the decimation factor from 1 to 32 ． Half of the $M \times 16$ coefficients are stored in the filter coefficient memory．
For a discrete－time FIR filter，its output is a weighted sum of the current and a finite number of previous values of the input as 公式 7 shows．

$$
Y[n]=\mathrm{C} 0 \times \mathrm{X}[\mathrm{n}]+\mathrm{C} 1 \times \mathrm{X}[\mathrm{n}-1] \ldots+\mathrm{C}_{\mathrm{N}} \times \mathrm{X}[\mathrm{n}-\mathrm{N}]
$$

where
－$X[n]$ is the input signal．
－ $\mathrm{Y}[\mathrm{n}]$ is the output signal．
－ CN is the filter coefficients．
－ N is the filter order．
Therefore，the delay of AFE5812 output is related to decimation factor，M．The TX＿TRIG timing also plays a role in this．In the following description，$M=1$ and $M=2$ are used as examples to derive a generic timing relationship among TX＿TRIG，AFE input，and AFE output．
The following register settings were used when the delay relationship was measured：
表 24．Settings for evaluating FIR Filter Delay versus TX＿TRIG Timing

| Register Setting | Register Setting <br> （HEX） | Description |
| :---: | :---: | :---: |
| $22[0]=0$ | $0 \times 16[0]=0$ | Enable demodulator． $0 \times 16$ belongs to ADC register |
| Profile RAM | Profile RAM | Set different decimation factor and other settings in profile RAM． |
| Coeff RAM | Coeff RAM | Write filter coefficients in coefficient memory． |
| 29［7］＝ 1 | $0 \times 1 \mathrm{D}[7]=1$ | Set DEC＿SHIFT＿FORCE＿EN |
| 10［13］＝ 1 | $0 \times A[13]=1$ | Set DEC＿SHIFT＿SCALE |
| 29［6：4］$=6$ | $0 \times 1 \mathrm{D}[6: 4]=6$ | Set DEC＿SHIFT＿FORCE |
| $\begin{aligned} 10[15] & =0,10[12]=1 \\ 10[4] & =1,10[1]=1 \end{aligned}$ | $\begin{gathered} 0 \times A[15]=0,0 \times A[12] \\ =1,0 \times A[4]=1 \\ 0 \times A[1]=1 \end{gathered}$ | RESERVED bits |
| $10[0]=1$ | $0 \times 0 \mathrm{~A}[0]=1$ | Set DC＿REMOVAL＿BYPASS |
| 10［10］＝ 1 | $0 \times 0 \mathrm{~A}[10]=1$ | Reset down conversion phase on TX＿TRIG |
| 03［14：13］＝ 11 | 03［14：13］＝ 11 | SERZ＿FACTOR 16X |
| 03［11：9］＝ 100 | 03［11：9］＝ 100 | OUTPUT＿RESOLUTION 16X |
| 04［4］＝ 1 | 04［4］＝ 1 | MSB＿FIRST |
| 11［15：0］ | 0xB［15：0］ | Set custom SYNC＿WORD value if needed |
| 10［2］＝0 | $0 \times 0 \mathrm{~A}[2]=0$ | Down conversion is enabled． |
| Profile RAM［21：6］＝0 | Profile RAM［21：6］＝0 | Down convert frequency set to 0 ，that is，multiply input signal with DC． |
| Note：Even if this frequency is set to a non－zero value，it will not change the demod latency．For experiment ease，mixing with DC is performed．ADC sampling frequency and VCA LPF settings were kept such that the AFE5812＇s demod sees a single pulse． |  |  |

When $\mathrm{M}=1$ ， 8 filter coefficients written in the memory are C0，C1 to C7．An impulse signal is applied at both VCA input and TX TRIG．Due to the impulse input，coefficients start coming at the output according to timing diagram shown in 图 93，where 20－cycle delay is observed．


图 93．Expected Latency Timing When $\mathbf{M}=1$
By adjusting the timing between AFE input and TX＿TRIG，the user can obtain a timing diagram similar to 图 93.


图 94．Measured Latency Timing When $M=1$
By adjusting the timing between AFE input and TX＿TRIG，the user can obtain a timing diagram similar to 图 94.
When $M=2$ ，if the impulse is given one clock before TX＿TRIG signal，then the sample followed after the sync word gives impulse response of the filter as shown in 图 95.


图 95．Measured Latency Timing When $M=2$

图 96 shows a generic timing diagram．The number of zeros comes before the sync word is equal to $Z$ ．The sync word comes after $S$ number of cycles，impulse response starts coming after $L$ number of cycles，and input impulse is given after IP cycles with respect to TX＿TRIG signal．Therefore，for different decimation factor（M）， values of these numbers are listed in 表 25 and 图 96.

表 25．Generic Latency versus Decimation Factor $\mathbf{M}^{(1)(2)}$

| $\mathbf{M}$ | Number of Zeros（ZNo） | Sync Word Latency（S） | Data Latency（L） | Input Impulse（IP）${ }^{(3)}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 2 | 17 | 18 | -2 |
| 2 | 3 | 18 | 19 | -1 |
| 3 | 4 | 19 | 20 | 0 |
| 4 | 5 | 20 | 21 | 1 |
| 5 | 6 | 21 | 22 | 2 |
| 6 | 7 | 22 | 23 | 3 |
| 7 | 8 | 23 | 24 | 4 |
| 8 | 9 | 24 | 25 | 5 |
| M | $16+M$ | $17+M$ | $M-3$ |  |

（1）When DC＿REMOVAL＿BYPASS $10[0]=0$ or $0 \times A[0]=0$ ，the sync word latency and data latency becomes $17+M$ and $18+M$
（2）ADC＇s low latency mode enabled by register $0 \times 2[12$ ］does not impact $S$ and $L$ ．
（3）Negative number represents input is given in advance with respect to TX＿TRIG signal．


图 96．Measured Latency Timing at Any M

## 10．6．2．2．6．0．1 Expression of Decimation Filter Response

Based on 表 25，the decimation filter＇s response is formulated．图 97 indicates that the Tx＿Trig sample is considered as the reference for time scale．So，the input to the device at Tx＿Trig clock will be expressed as X［0］， the next sample input as X［1］，and so on．Similarly，the output of the device followed by the AFE5812＇s demodulator will be expressed as $\mathrm{Y}[0]$ at the instant of Tx＿Trig， $\mathrm{Y}[1]$ at the next clock，and so on； Cn or $\mathrm{C}(\mathrm{n})$ indicates the coefficient of $\mathrm{n}^{\text {th }}$ index．

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## 图 97．Typical Timing Expression Among ADC CLK，Input，TX＿TRIG，and Output

For $\mathbf{M}=\mathbf{1}$ ，the number of zeros，$Z N o=2$ ；Sync word latency $S=17$ ．So，the output values from sample 18 are relevant and the first few samples are：
－ $\mathrm{Y}[18]=\mathrm{C} 0 \times \mathrm{X}[-2]+\mathrm{C} 1 \times \mathrm{X}[-3]+\mathrm{C} 2 \times \mathrm{X}[-4]+\ldots+\mathrm{C} 7 \times \mathrm{X}[-9]+\mathrm{C} 7 \times \mathrm{X}[-10]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-17]$
－ $\mathrm{Y}[19]=\mathrm{C} 0 \times \mathrm{X}[-1]+\mathrm{C} 1 \times \mathrm{X}[-2]+\mathrm{C} 2 \times \mathrm{X}[-3]+\ldots+\mathrm{C} 7 \times \mathrm{X}[-8]+\mathrm{C} 7 \times \mathrm{X}[-9]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-16]$
－ $\mathrm{Y}[20]=\mathrm{C} 0 \times \mathrm{X}[0]+\mathrm{C} 1 \times \mathrm{X}[-1]+\mathrm{C} 2 \times \mathrm{X}[-2]+\ldots+\mathrm{C} 7 \times \mathrm{X}[-7]+\mathrm{C} 7 \times \mathrm{X}[-8]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-15]$
All these samples appear at the output because no samples are dropped for decimation factor $=1$ ．
For $\mathbf{M}=\mathbf{2}$ ，the number of zeros，$Z N o=3$ ；Sync word latency $S=18$ ．So，the output values from sample 19 are relevant and the first few samples are described as：
－ $\mathrm{Y}[19]=\mathrm{C} 0 \times \mathrm{X}[-1]+\mathrm{C} 1 \times \mathrm{X}[-2]+\mathrm{C} 2 \times \mathrm{X}[-3]+\ldots+\mathrm{C} 15 \times \mathrm{X}[-16]+\mathrm{C} 15 \times \mathrm{X}[-17]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-32]$
－ $\mathrm{Y}[20]=\mathrm{C} 0 \times \mathrm{X}[0]+\mathrm{C} 1 \times \mathrm{X}[-1]+\mathrm{C} 2 \times \mathrm{X}[-2]+\ldots+\mathrm{C} 15 \times \mathrm{X}[-15]+\mathrm{C} 15 \times \mathrm{X}[-16]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-31]$
－ $\mathrm{Y}[21]=\mathrm{C} 0 \times \mathrm{X}[1]+\mathrm{C} 1 \times \mathrm{X}[0]+\mathrm{C} 2 \times \mathrm{X}[-1]+\ldots+\mathrm{C} 15 \times \mathrm{X}[-14]+\mathrm{C} 15 \times \mathrm{X}[-15]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-30]$
But for $M=2$ ，every alternate sample must be dropped．The decimation is adjusted in such a way that the first sample after sync is retained．Hence in this case， $\mathrm{Y}[19], \mathrm{Y}[21], \mathrm{Y}[23]$ ，and so forth are retained and $\mathrm{Y}[20], \mathrm{Y}[22]$ ， Y［24］，and so forth are dropped．

For $\mathbf{M}=3$ ，the number of zeros，$Z N o=4$ ；Sync word latency $S=19$ ．So，the output values from sample 20 are relevant and the first few samples are described as：
－ $\mathrm{Y}[20]=\mathrm{C} 0 \times \mathrm{X}[0]+\mathrm{C} 1 \times \mathrm{X}[-1]+\mathrm{C} 2 \times \mathrm{X}[-2]+\ldots+\mathrm{C} 23 \times \mathrm{X}[-23]+\mathrm{C} 23 \times \mathrm{X}[-24]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-47]$
－ $\mathrm{Y}[21]=\mathrm{C} 0 \times \mathrm{X}[1]+\mathrm{C} 1 \times \mathrm{X}[0]+\mathrm{C} 2 \times \mathrm{X}[-1]+\ldots+\mathrm{C} 23 \times \mathrm{X}[-22]+\mathrm{C} 23 \times \mathrm{X}[-23]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-46]$
－ $\mathrm{Y}[22]=\mathrm{C} 0 \times \mathrm{X}[2]+\mathrm{C} 1 \times \mathrm{X}[1]+\mathrm{C} 2 \times \mathrm{X}[0]+\ldots+\mathrm{C} 23 \times \mathrm{X}[-21]+\mathrm{C} 23 \times \mathrm{X}[-22]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-45]$
－ $\mathrm{Y}[23]=\mathrm{C} 0 \times \mathrm{X}[3]+\mathrm{C} 1 \times \mathrm{X}[2]+\mathrm{C} 2 \times \mathrm{X}[1]+\ldots+\mathrm{C} 23 \times \mathrm{X}[-20]+\mathrm{C} 23 \times \mathrm{X}[-21]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-44]$
But for $\mathrm{M}=3$ ，the last two of every three samples must be dropped．The decimation is adjusted in such a way that the first sample after sync is retained．Hence in this case， $\mathrm{Y}[20], \mathrm{Y}[23], \mathrm{Y}[26]$ ，and so forth are retained and Y［21］，Y［22］，Y［24］，Y［25］，and so forth are dropped．
For any M，this pattern can be generalized for a decimation factor of $M$ ．The number of $Z N o=M+1$ ，Sync word latency $S=16+M$ ．So，the output values from sample $(17+M)$ are relevant and the first few samples are described as：
－ $\mathrm{Y}[17+\mathrm{M}]=\mathrm{C} 0 \times \mathrm{X}[\mathrm{M}-3]+\mathrm{C} 1 \times \mathrm{X}[\mathrm{M}-4]+\mathrm{C} 2 \times \mathrm{X}[\mathrm{M}-5]+\ldots+\mathrm{C}(8 \mathrm{M}-1) \times \mathrm{X}[-7 \mathrm{M}-2]+\mathrm{C}(8 \mathrm{M}-1) \times \mathrm{X}[-7 \mathrm{M}-3]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-15 \mathrm{M}-$ 2］
－ $\mathrm{Y}[18+\mathrm{M}]=\mathrm{C} 0 \times \mathrm{X}[\mathrm{M}-2]+\mathrm{C} 1 \times \mathrm{X}[\mathrm{M}-3]+\mathrm{C} 2 \times \mathrm{X}[\mathrm{M}-4]+\ldots+\mathrm{C}(8 \mathrm{M}-1) \times \mathrm{X}[-7 \mathrm{M}-1]+\mathrm{C}(8 \mathrm{M}-1) \times \mathrm{X}[-7 \mathrm{M}-2]+\ldots+\mathrm{C}[0] \times \mathrm{X}[-15 \mathrm{M}-$ 1］
For a decimation factor of $M$ which is not 1 ，the decimation is adjusted in such a way that the first sample after sync is retained．Hence in this case， $\mathrm{Y}[17+\mathrm{M}], \mathrm{Y}[17+2 \mathrm{M}], \mathrm{Y}[17+3 \mathrm{M}]$ ，and so forth are retained and the rest of samples between these，that is， $\mathrm{Y}[18+\mathrm{M}], \mathrm{Y}[19+2 \mathrm{M}], \ldots, \mathrm{Y}[16+2 \mathrm{M}]$ are dropped．

## 11 Application and Implementation

## 注

Information in the following applications sections is not part of the Tl component specification，and TI does not warrant its accuracy or completeness．Tl＇s customers are responsible for determining suitability of components for their purposes．Customers should validate and test their design implementation to confirm system functionality．

## 11．1 Application Information

图 98 lists a typical application circuit diagram．The configuration for each block is discussed in the following sections．表 26 lists companion TI devices that are used to complete the analog signal chain in a system．

## 表 26．Application Companion Devices

| Part Number | Part Description | Functions |
| :---: | :---: | :---: |
| THS4130，SLOS318 | Fully Differential Input／Output Low Noise Amplifier With Shutdown | TGC Vcntl Opamp，CW summing amplifier and active filter |
| OPA1632，SBOS286 | Fully Differential I／O Audio Amplifier | TGC Vcntl amplifier，CW summing amplifier and active filter |
| OPA2211A，SBOS377 | $1.1 \mathrm{nV} / \mathrm{rtHz}$ Noise，Low Power，Precision Operational Amplifier | CW summing amplifier and active filter |
| LME49990，SNOSB16 | Ultra－low Distortion，Ultra－low Noise Operational Amplifier | CW summing amplifier and active filter |
| LMH6629，SNOSB18 | Ultra－Low Noise，High－Speed Operational Amplifier with Shutdown | CW summing amplifier and active filter |
| ADS8413，SLAS490 | 16－bit，Unipolar Diff Input，2MSPS Sampling rate， 4.75 V to 5.25 V ADC with LVDS Serial Interface | CW Audio ADC |
| ADS8881，SBAS547 | 18－Bit，1－MSPS，Serial Interface，microPower，Truly－Differential Input， SAR ADC | CW Audio ADC |
| DAC7811，SBAS337 | 12－Bit，Serial Input，Multiplying Digital to Analog Converter | TGC Ventl Digital to Analog Converter |
| LMK04803，SNAS489 | Low Noise Clock Jitter Cleaner With Dual Cascaded PLLs and Integrated 1.9 GHz VCO | Jitter cleaner and clock synthesizer |
| CDCM7005，SCAS793 | High Performance，Low Phase Noise，Low Skew Clock Synchronizer | Jitter cleaner and clock synthesizer |
| CDCE72010，SLAS490 | 10 Outputs Low Jitter Clock Synchronizer and Jitter Cleaner | Jitter cleaner and clock synthesizer |
| CDCLVP1208，SCAS890 | Low Jitter，2－Input Selectable 1：8 Universal－to－LVPECL Buffer | Clock buffer |
| LMK00308，SNAS576 | 3．1－GHz Differential Clock Buffer／Level Translator | Clock buffer |
| LMK01000，SNAS437 | 1．6 GHz High Performance Clock Buffer，Divider，and Distributor | Clock buffer |
| SN74AUP1T04，SCES800 | Low Power，1．8／2．5／3．3－V Input，3．3－V CMOS Output，Single Inverter Gate | 1．8V／2．5V／3．3V Level shifter for SPI |
| UCC28250 SLUSA29 | Advanced PWM Controller with Pre－Bias Operation | Synchronized DC－DC power supply controller |

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## 11．2 Typical Application



图 98．Application Circuit with Internally Generated 1．4V Demod Supply

## Typical Application（接下页）

## 11．2．1 Design Requirement

The AFE5812 is a highly integrated analog front－end solution．In order to maximize its performance，users must carefully optimize its surrounding circuits，such as T／R switch，Vcntl circuits，audio ADCs for CW path，clock distribution network，synchronized power supplies and digital processors．Some common practices are described below．
Typical requirements for a traditional medical ultrasound imaging system are shown in 表 27.

## 表 27．Design Parameters

| PARAMETER | EXAMPLE VALUES |
| :---: | :---: |
| Signal center frequency $\left(\mathrm{f}_{0}\right)$ | $1 \sim 20 \mathrm{MHz}$ |
| Signal Bandwidth（BW） | $10 \sim 100 \%$ of $\mathrm{f}_{0}$ |
| Overloaded signals due to $\mathrm{T} / \mathrm{R}$ <br> switch leakage | $\sim 2 \mathrm{Vpp}$ |
| Maximum input signal amplitude | 100 mVpp to 1 Vpp |
| Transducer noise level | $1 \mathrm{nV} / \mathrm{rtHz}$ |
| Dynamic range | $151 \mathrm{dBc} / \mathrm{Hz}$ |
| Time gain compensation range | 40 dB |
| Total harmonic distortion | $40 \mathrm{dBc} @ 5 \mathrm{MHz}$ |

## 11．2．2 Detailed Design Procedure

Medical ultrasound imaging is a widely－used diagnostic technique that enables visualization of internal organs， their size，structure，and blood flow estimation．An ultrasound system uses a focal imaging technique that involves time shifting，scaling，and intelligently summing the echo energy using an array of transducers to achieve high imaging performance．The concept of focal imaging provides the ability to focus on a single point in the scan region．By subsequently focusing at different points，an image is assembled．
When initiating an imaging，a pulse is generated and transmitted from each of the 64 transducer elements．The pulse，now in the form of mechanical energy，propagates through the body as sound waves，typically in the frequency range of 1 MHz to 15 MHz ．The sound waves are attenuated as they travel through the objects being imaged，and the attenuation coefficients a are about $0.54 \mathrm{~dB} /(\mathrm{MHz} \times \mathrm{cm})$ in soft tissue and $6 \sim 10 \mathrm{~dB} /(\mathrm{MHz} \times \mathrm{cm})$ in bone（ source：http：／／en．wikipedia．org／wiki／Attenuation）．Most medical ultrasound systems use the reflection imaging mode and the total signal attenuation is calculated by $2 \times$ depth $\times a \times \mathrm{f}_{0}$ ．As the signal travels，portions of the wave front energy are reflected．Signals that are reflected immediately after transmission are very strong because they are from reflections close to the surface；reflections that occur long after the transmit pulse are very weak because they are reflecting from deep in the body．As a result of the limitations on the amount of energy that can be put into the imaging object，the industry developed extremely sensitive receive electronics with wide dynamic range．
Receive echoes from focal points close to the surface require little，if any，amplification．This region is referred to as the near field．However，receive echoes from focal points deep in the body are extremely weak and must be amplified by a factor of 100 or more．This region is referred to as the far field．In the high－gain（far field）mode， the limit of performance is the sum of all noise sources in the receive chain．In high－gain（far field）mode，system performance is defined by its overall noise level，which is limited by the noise level of the transducer assembly and the receive low－noise amplifier（LNA）．However in the low－gain（near field）mode，system performance is defined by the maximum amplitude of the input signal that the system can handle．The ratio between noise levels in high－gain mode and the signal amplitude level in low－gain mode is defined as the dynamic range of the system．The high integration and high dynamic range of the device make it ideally suited for ultrasound imaging applications．
The device includes an integrated LNA and VCAT（which use the gain that can be changed with enough time to handle both near－and far－field systems），a low－pass antialiasing filter to limit the noise bandwidth，an ADC with high SNR performance，and a CW mixer．图 98 illustrates an application circuit of the device．
Use the following steps to design medical ultrasound imaging systems：
1．Use the signal center frequency and signal bandwidth to select an appropriate ADC sampling frequency．

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2．Use the time gain compensation range to select the range of the VCNTL signal．
3．Use the transducer noise level and maximum input signal amplitude to select the appropriate LNA gain．The device input－referred noise level reduces with higher LNA gain．However，higher LNA gain leads to lower input signal swing support．
4．Select different passive components for different device pins as shown in 图 98.
5．Select the appropriate input termination configuration as discussed in Active Termination．
6．Select the clock configuration for the ADC and CW clocks as discussed in CW Clock Selection and ADC Clock Configurations．

## 11．2．2．1 LNA Configuration

## 11．2．2．1．1 LNA Input Coupling and Decoupling

The LNA closed－loop architecture is internally compensated for maximum stability without the need of external compensation components．The LNA inputs are biased at 2.2 V and AC coupling is required．图 99 shows a typical input configuration． $\mathrm{C}_{\mathbb{I}}$ is the input $A C$ coupling capacitor． $\mathrm{C}_{\mathrm{ACT}}$ is a part of the active termination feedback path．Even if the active termination is not used，the $\mathrm{C}_{\mathrm{ACT}}$ is required for the clamp functionality．The recommended values for $\mathrm{C}_{\mathrm{ACT}}$ is $\geq 1 \mu \mathrm{~F}$ and $\mathrm{C}_{\mathrm{IN}}$ is $\geq 0.1 \mu \mathrm{~F}$ ．A pair of clamping diodes is commonly placed between the T／R switch and the LNA input．Schottky diodes with suitable forward drop voltage（for example：the BAT754／54 series，the BAS40 series，the MMBD7000 series，or similar）can be considered depending on the transducer echo amplitude．


图 99．LNA Input Configurations
This architecture minimizes any loading of the signal source that may lead to a frequency－dependent voltage divider．The closed－loop design yields low offsets and offset drift． $\mathrm{C}_{\text {BYPASS }}(\geq 0.015 \mu \mathrm{~F})$ is used to set the HPF cut－ off frequency and decouple the complementary input．Its cut－off frequency is inversely proportional to the $\mathrm{C}_{\text {BYPASS }}$ value．The HPF cut－off frequency can be adjusted through the register 59［3：2］表 28 lists．Low－frequency signals at T／R switch output，such as signals with slow ringing，can be filtered out．In addition，the HPF can minimize system noise from DC－DC converters，pulse repetition frequency（PRF）trigger，and frame clock．Most ultrasound systems＇signal－processing unit includes digital HPFs or band－pass filters（BPFs）in FPGAs or ASICs．Further noise suppression can be achieved in these blocks．In addition，a digital HPF is also available in the AFE5812 ADC or digital demodulator．If low－frequency signal detection is desired in some applications，the LNA HPF can be disabled．

表 28．LNA HPF Settings（ $\mathrm{C}_{\text {BYPASS }}=15 \mathrm{nF}$ ）

| Reg59［3：2］（0x3B［3：2］） | Frequency（kHz） |
| :---: | :---: |
| 00 | 100 |
| 01 | 50 |
| 10 | 200 |
| 11 | 150 |

CM＿BYP and VHIGH pins，which generate internal reference voltages，need to be decoupled with $\geq 1-\mu \mathrm{F}$ capacitors．Bigger bypassing capacitors（ $>2.2 \mu \mathrm{~F}$ ）may be beneficial if low－frequency noise exists in the system．

## 11．2．2．1．2 LNA Noise Contribution

The noise specification is critical for LNA and it determines the dynamic range of the entire system．The LNA of the AFE5812 achieves low power and an exceptionally low－noise voltage of $0.63 \sim 0.9 \mathrm{nV} / \sqrt{ } \mathrm{Hz}$ ，and a low current noise of $2 \sim 2.7 \mathrm{pA} / \sqrt{ } \mathrm{Hz}$ ．

Typical ultrasonic transducer＇s impedance， $\mathrm{R}_{\mathrm{S}}$ ，varies from tens of ohms to several hundreds of ohms．Voltage noise is the dominant noise in most cases；however，the LNA current noise flowing through the source impedance $\left(R_{S}\right)$ generates additional voltage noise．
LNA＿Noise total $=\sqrt{\mathrm{V}_{\text {LNAnoise }}^{2}+\mathrm{R}_{\mathrm{s}}^{2} \times \mathrm{L}_{\text {LNAnoise }}^{2}}$
The AFE5812 achieves low－noise figure（NF）over a wide range of source resistances as shown in 图32，图33， and 图 34.

## 11．2．2．1．3 Active Termination

In ultrasound applications，signal reflection exists due to long cables between the transducer and system．The reflection results in extra ringing added to echo signals in PW mode．Because the axial resolution depends on echo signal length，such ringing effect can degrade the axial resolution．Therefore，either passive termination or active termination is preferred if good axial resolution is desired．图 100 shows three termination configurations．


S0499－01
图 100．Termination Configurations
Under the no termination configuration，the input impedance of the AFE5812 is about $6 \mathrm{k} \Omega(8 \mathrm{~K} / 20 \mathrm{pF})$ at 1 MHz ．Passive termination requires external termination resistor $\mathrm{R}_{\mathrm{t}}$ ，which contributes to additional thermal noise． The LNA supports active termination with programmable values，as shown in 图 101.


图 101．Active Termination Implementation
The AFE5812 has four pre－settings $50,100,200$ ，and $400 \Omega$ ，which are configurable through the registers．Other termination values can be realized by setting the termination switches shown in 图101．Register［52］is used to enable these switches．The input impedance of the LNA under the active termination configuration approximately follows：
$Z_{\text {IN }}=\frac{R_{f}}{1+\frac{A v_{\mathrm{LNA}}}{2}}$
表 6 lists the LNA $R_{\mathbb{N}} S$ under different LNA gains．System designers can achieve fine tuning for different probes．
The equivalent input impedance is given by 公式 10 where $R_{I N}(8 \mathrm{k} \Omega)$ and $\mathrm{C}_{\mathrm{IN}}(20 \mathrm{pF})$ are the input resistance and capacitance of the LNA．

$$
\begin{equation*}
\mathrm{Z}_{\mathrm{IN}}=\frac{\mathrm{R}_{f}}{1+\frac{\mathrm{A} v_{\mathrm{LNA}}}{2}} / / \mathrm{C}_{\mathrm{IN}} / / \mathrm{R}_{\mathrm{IN}} \tag{10}
\end{equation*}
$$

Therefore，the $Z_{\mathbb{I N}}$ is frequency dependent，and it decreases as frequency increases as shown in 图 10．Because 2 to 10 MHz is the most commonly used frequency range in medical ultrasound，this rolling－off effect does not impact system performance greatly．Active termination can be applied to both CW and TGC modes．Because each ultrasound system includes multiple transducers with different impedances，the flexibility of impedance configuration is a great plus．
图 32，图 33，and 图 34 show the NF under different termination configurations．It indicates that no termination achieves the best noise figure；active termination adds less noise than passive termination．Thus，termination topology should be carefully selected based on each use scenario in ultrasound．

## 11．2．2．1．4 LNA Gain Switch Response

The LNA gain is programmable through SPI．The gain switching time depends on the SPI speed as well as the LNA gain response time．During the switching，glitches might occur and they can appear as artifacts in images． In addition，the signal chain needs about $14 \mu \mathrm{~s}$ to settle after the LNA gain change．Thus，LNA gain switching may not be preferred when switching time or settling time for the signal chain is limited．

## 11．2．2．2 Voltage－Controlled Attenuator

The attenuator in the AFE5812 is controlled by a pair of differential control inputs，the $\mathrm{V}_{\mathrm{CNTLM}, \mathrm{P}}$ pins．The differential control voltage spans from 0 to 1.5 V ．This control voltage varies the attenuation of the attenuator based on its linear－in－dB characteristic．Its maximum attenuation（minimum channel gain）appears at $\mathrm{V}_{\text {CNTLP }}-$ $\mathrm{V}_{\text {CNTLM }}=1.5 \mathrm{~V}$ and minimum attenuation（maximum channel gain）occurs at $\mathrm{V}_{\text {CNTLP }}-\mathrm{V}_{\text {CNTLM }}=0$ ．The typical gain range is 40 dB and remains constant，independent of the PGA setting．
When only single－ended $\mathrm{V}_{\mathrm{CNTL}}$ signal is available，this $1.5-\mathrm{Vpp}$ signal can be applied on the $\mathrm{V}_{\text {CNTLP }}$ pin with the $V_{\text {CNTLM }}$ pin connected to ground；As 图 102 show，the TGC gain curve is inversely proportional to the $\mathrm{V}_{\text {CNTLP }}$－ $V_{\text {CNTLM }}$ ．


图 102． $\mathrm{V}_{\text {CNTLP }}$ and $\mathrm{V}_{\text {CNTLM }}$ Configurations
As discussed in the theory of operation，the attenuator architecture uses seven attenuator segments that are equally spaced in order to approximate the linear－in－dB gain－control slope．This approximation results in a monotonic slope；the gain ripple is typically less than $\pm 0.5 \mathrm{~dB}$ ．

The control voltage input（ $\mathrm{V}_{\text {CNTLM，P }}$ pins）represents a high－impedance input．The $\mathrm{V}_{\text {CNTLM，}}$ pins of multiple AFE5812 devices can be connected in parallel with no significant loading effects．When the voltage level （ $\mathrm{V}_{\text {CNTLP }}-\mathrm{V}_{\text {CNTLM }}$ ）is above 1.5 V or below 0 V ，the attenuator continues to operate at its maximum attenuation level or minimum attenuation level，respectively．TI recommends to limit the voltage from -0.3 to 2 V ．

When the AFE5812 operates in CW mode，the attenuator stage remains connected to the LNA outputs． Therefore，TI recommends to power down the VCA using the PDN＿VCA register bit．In this case， $\mathrm{V}_{\text {CNTLP }}$－ $\mathrm{V}_{\text {CNTLM }}$ voltage does not matter．
The AFE5812 gain－control input has a $-3-\mathrm{dB}$ bandwidth of approximately 800 kHz ．This wide bandwidth， although useful in many applications（for example，fast $\mathrm{V}_{\text {CNTL }}$ response），can also allow high－frequency noise to modulate the gain control input and finally affect the Doppler performance．In practice，this modulation can be avoided by additional external filtering（ $\mathrm{RV}_{\mathrm{CNTL}}$ and $\mathrm{CV}_{\mathrm{CNTL}}$ ）at $\mathrm{V}_{\mathrm{CNTLM,P}}$ pins as 图 81 shows．However，the external filter＇s cutoff frequency cannot be kept too low as this results in low gain response time．Without external filtering，the gain control response time is typically less than $1 \mu \mathrm{~s}$ to settle within $10 \%$ of the final signal level of 1 VPP（ -6 －dBFS）output as indicated in 图 51 and 图 52.
Typical $\mathrm{V}_{\text {CNTLM，P }}$ signals are generated by an 8－to 12－bit 10－MSPS digital－to－analog converter（DAC）and a differential operation amplifier．Tl＇s DACs，such as TLV5626 and DAC7821／11（10 MSPS／12 bit），could be used to generate TGC control waveforms．Differential amplifiers with output common mode voltage control（that is， THS4130 and OPA1632）can connect the DAC to the $\mathrm{V}_{\text {CNTLMP }}$ pins．The buffer amplifier can also be configured as an active filter to suppress low－frequency noise．The $\mathrm{V}_{\text {CNTLM／P }}$ circuit achieves low noise to prevent the $\mathrm{V}_{\text {CNTLMP }}$ noise being modulated to RF signals．TI recommends that $\mathrm{V}_{\text {CNTLM／P }}$ noise for one AFE is below 25 $\mathrm{nV} / \mathrm{rtHz}$ at 1 kHz and $5 \mathrm{nV} / \mathrm{rtHz}$ at 50 kHz ．In high－channel count premium systems，the $\mathrm{V}_{\text {CNTLM／P }}$ noise requirement is higher as shown below．


图 103．Allowed Noise on the VCNTL Signal Across Frequency and Different Channels
More information can be found in the literatures SLOS318 and SBAA150．See 图 2 for the $\mathrm{V}_{\text {CNTL }}$ vs Gain curves．表 29 also shows the absolute gain vs $\mathrm{V}_{\text {CNTL }}$ ，which may help program DAC correspondingly．
In PW Doppler and color Doppler modes， $\mathrm{V}_{\text {CNTL }}$ noise should be minimized to achieve the best close－in phase noise and SNR．DTGC feature is implemented to address this need in the AFE5812．In the DTGC mode，no external $\mathrm{V}_{\text {CNTL }}$ is needed．Refer to 图 64.

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表 29． $\mathrm{V}_{\text {CNTLP }}-\mathrm{V}_{\text {CNTLM }}$ vs Gain Under Different LNA and PGA Gain Settings（Low－Noise Mode）

| $\mathrm{V}_{\text {CNTLP }}-\mathrm{V}_{\mathrm{CNTLM}}$ <br> （V） | $\begin{gathered} \text { Gain (dB) } \\ \text { LNA }=15 \mathrm{~dB} \\ \text { PGA }=24 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} \text { Gain (dB) } \\ \text { LNA }=18 \mathrm{~dB} \\ \text { PGA }=24 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} \text { Gain (dB) } \\ \text { LNA }=24 \mathrm{~dB} \\ \text { PGA }=24 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} \text { Gain (dB) } \\ \text { LNA }=15 \mathrm{~dB} \\ \text { PGA }=30 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} \text { Gain (dB) } \\ \text { LNA }=18 \mathrm{~dB} \\ \text { PGA }=30 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} \text { Gain (dB) } \\ \text { LNA }=24 \mathrm{~dB} \\ \text { PGA }=30 \mathrm{~dB} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 39.45 | 42.45 | 48.45 | 45.25 | 48.25 | 54.25 |
| 0.1 | 36.91 | 39.91 | 45.91 | 42.71 | 45.71 | 51.71 |
| 0.2 | 33.78 | 36.78 | 42.78 | 39.58 | 42.58 | 48.58 |
| 0.3 | 30.39 | 33.39 | 39.39 | 36.19 | 39.19 | 45.19 |
| 0.4 | 26.74 | 29.74 | 35.74 | 32.54 | 35.54 | 41.54 |
| 0.5 | 23.69 | 26.69 | 32.69 | 29.49 | 32.49 | 38.49 |
| 0.6 | 20.11 | 23.11 | 29.11 | 25.91 | 28.91 | 34.91 |
| 0.7 | 16.54 | 19.54 | 25.54 | 22.34 | 25.34 | 31.34 |
| 0.8 | 13.27 | 16.27 | 22.27 | 19.07 | 22.07 | 28.07 |
| 0.9 | 9.48 | 12.48 | 18.48 | 15.28 | 18.28 | 24.28 |
| 1.0 | 6.16 | 9.16 | 15.16 | 11.96 | 14.96 | 20.96 |
| 1.1 | 2.65 | 5.65 | 11.65 | 8.45 | 11.45 | 17.45 |
| 1.2 | 0.52 | 3.52 | 9.52 | 6.32 | 9.32 | 15.32 |
| 1.3 | －0．58 | 2.42 | 8.42 | 5.22 | 8.22 | 14.22 |
| 1.4 | －1．01 | 1.99 | 7.99 | 4.79 | 7.79 | 13.79 |
| 1.5 | －1 | 2 | 8 | 4.8 | 7.8 | 13.8 |

## 11．2．2．3 CW Operation

## 11．2．2．3．1 CW Summing Amplifier

To simplify CW system design，a summing amplifier is implemented in the AFE5812 to sum and convert 8－ channel mixer current outputs to a differential voltage output．Low noise and low power are achieved in the summing amplifier while maintaining the full dynamic range required in CW operation．
This summing amplifier has five internal gain adjustment resistors which can provide 32 different gain settings （register 54［4：0］，图 101 and 表 9）．System designers can easily adjust the CW path gain depending on signal strength and transducer sensitivity．For any other gain values，an external resistor option is supported．The gain of the summation amplifier is determined by the ratio between the $500-\Omega$ resistors after LNA and the internal or external resistor network $\mathrm{R}_{\mathrm{EXT} / \mathrm{NT} \text { ．Thus，the matching between these resistors plays a more important role than }}$ absolute resistor values．Better than $1 \%$ matching is achieved on chip．Due to process variation，the absolute resistor tolerance could be higher．If external resistors are used，the gain error between I／Q channels or among multiple AFEs may increase．TI recommends to use internal resistors and low tolerance capacitor $\mathrm{C}_{\text {ExT }}$ to set the gain in order to achieve better gain matching（across channels and multiple AFEs）．This summing amplifier has first－order LPF response to remove high－frequency components from the mixers，such as $2 \mathrm{f} 0 \pm \mathrm{fd}$ ．Its cut－off frequency is determined by：

$$
\begin{equation*}
f_{\mathrm{HP}}=\frac{1}{2 \pi \mathrm{R}_{\mathrm{INT} / \mathrm{EXT}} \mathrm{C}_{\mathrm{EXT}}} \tag{11}
\end{equation*}
$$

Note that when different gain is configured through Register 54［4：0］，the LPF response varies as well．


S0501－01
图 104．CW Summing Amplifier Block Diagram
Multiple AFE5812s are usually used in parallel to expand CW beamformer channel count．The AFE5812 CW＇s voltage outputs can be summed and filtered externally further to achieve desired gain and filter response．AC－ coupling capacitors $\mathrm{C}_{\mathrm{AC}}$ are required to block the DC component of the CW carrier signal． $\mathrm{C}_{A C}$ can vary from 1 to $10 \mu \mathrm{~F}$ depending on the desired low－frequency Doppler signal from slow blood flow．Multiple AFE5812s＇I／Q outputs can be summed together with a low－noisel differential amplifiers before 16， 18 －bit differential audio ADCs． The TI ultra－low noise differential precision amplifier OPA1632 and THS4130 are suitable devices．

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图 106 shows an alternative current summing circuit．However，this circuit only achieves good performance when a lower－noise operational amplifier is available compared to the AFE5812＇s internal summing differential amplifier．


图 105．CW Circuit With Multiple AFE5812s（Voltage Output Mode）


图 106．CW Circuit With Multiple AFE5812s（Current Output Mode，CM＿BYP＝1．5V）
The CW I／Q channels are well matched internally to suppress image frequency components in the Doppler spectrum．Low－tolerance components（ R and C ）and precise operational amplifiers should be used for achieving good matching in the external circuits as well．

## 注

The local oscillator inputs of the passive mixer are $\cos (\omega t)$ for I－CH and $\sin (\omega t)$ for Q－CH， respectively．Depending on the users＇CW Doppler complex FFT processing，swapping I／Q channels in FPGA or DSP may be needed to get correct blood flow directions．

## 11．2．2．3．2 CW Clock Selection

The AFE5812 can accept differential LVDS，LVPECL，and other differential clock inputs as well as single－ended CMOS clock．An internally generated VCM of 2.5 V is applied to CW clock inputs，that is，CLKP＿16X／ CLKM＿16X and CLKP＿1X／CLKM＿1X．Because this $2.5-$ V VCM is different from the one used in standard LVDS or LVPECL clocks，AC coupling is required between clock drivers and the AFE5812 CW clock inputs．When the CMOS clock is used，CLKM＿1X and CLKM＿16X should be tied to ground．图 107 shows common clock configurations．TI recommends appropriate termination to achieve good signal integrity．

（a）LVPECL Configuration

（b）LVDS Configuration

（c）Transformer Based Configuration

（d）CMOS Configuration
图 107．Clock Configurations

The combination of the clock noise and the CW path noise can degrade the CW performance．The internal clocking circuit is designed for achieving excellent phase noise required by CW operation．The phase noise of the AFE5812 CW path is better than $155 \mathrm{dBc} / \mathrm{Hz}$ at $1-\mathrm{kHz}$ offset．Consequently，the phase noise of the mixer clock inputs needs to be much better than $155 \mathrm{dBc} / \mathrm{Hz}$ ．

In the $16 / 8 / 4 \times f_{\mathrm{cw}}$ operations modes，low phase noise clock is required for $16,8,4 \times f_{\mathrm{cw}}$ clocks（that is， CLKP＿16X／CLKM＿16X pins）to maintain good CW phase noise performance．The $1 \times f_{\mathrm{cw}}$ clock（that is， CLKP＿1X／CLKM＿1 X pins）is only used to synchronize the multiple AFE5812 chips and is not used for demodulation．Thus， $1 \times f_{\mathrm{cw}}$ clock＇s phase noise is not a concern．However，in the $1 \times f_{\mathrm{cw}}$ operation mode，low－ phase noise clocks are required for both CLKP＿16X／CLKM＿16X and CLKP＿1X／CLKM＿1X pins because both of them are used for mixer demodulation．In general，a higher slew rate clock has lower phase noise；thus，clocks with high amplitude and fast slew rate are preferred in CW operation．In the CMOS clock mode，a 5－V CMOS clock can achieve the highest slew rate．

Clock phase noise can be improved by a divider as long as the divider＇s phase noise is lower than the target phase noise．The phase noise of a divided clock can be improved approximately by a factor of $20 \log \mathrm{NdB}$ where $N$ is the dividing factor of 16,8 ，or 4 ．If the target phase noise of mixer LO clock $1 \times f_{\mathrm{cw}}$ is $160 \mathrm{dBc} / \mathrm{Hz}$ at 1 kHz off carrier，the $16 \times f_{\mathrm{cw}}$ clock phase noise should be better than $160-20 \log 16=136 \mathrm{dBc} / \mathrm{Hz}$ ．Tl＇s jitter cleaners LMK048X／CDCM7005／CDCE72010 exceed this requirement and can be selected for the AFE5812．In the $4 \times / 1 \times$ modes，higher－quality input clocks are expected to achieve the same performance because N is smaller．Thus， the $16 \times$ mode is a preferred mode because it reduces the phase noise requirement for system clock design．In addition，the phase delay accuracy is specified by the internal clock divider and distribution circuit．Note in the $16 \times$ operation mode，the CW operation range is limited to 8 MHz due to the $16 \times$ CLK．The maximum clock frequency for the $16 \times$ CLK is 128 MHz ．In the $8 \times, 4 \times$ ，and $1 \times$ modes，higher CW signal frequencies up to 15 MHz can be supported with small degradation in performance，for example，the phase noise is degraded by 9 dB at 15 MHz ，compared to 2 MHz ．

As the channel number in a system increases，clock distribution becomes more complex．It is not preferred to use one clock driver output to drive multiple AFEs because the clock buffer＇s load capacitance increases by a factor of N ．As a result，the falling and rising time of a clock signal is degraded．A typical clock arrangement for multiple AFE5812s is shown in 图 108．Each clock buffer output drives one AFE5812 in order to achieve the best signal integrity and fastest slew rate，that is，better phase noise performance．When clock phase noise is not a concern，for example，the $1 \times f_{\mathrm{cw}}$ clock in the $16,8,4 \times f_{\mathrm{cw}}$ operation modes，one clock driver output may excite more than one AFE5812．Nevertheless，special considerations should be applied in such a clock distribution network design．In typical ultrasound systems，it is required that all clocks are generated from a same clock source，such as $16 \times f_{\mathrm{cw}}, 1 \times f_{\mathrm{cw}}$ clocks，audio ADC clocks，RF ADC clock，pulse repetition frequency signal， frame clock，and so on．By doing this，interference due to clock asynchronization can be minimized．


图 108．CW Clock Distribution

## 11．2．2．3．3 CW Supporting Circuits

As a general practice in CW circuit design，in－phase and quadrature channels should be strictly symmetrical by using well－matched layout and high－accuracy components．
In systems，additional high－pass wall filters（ 20 to 500 Hz ）and low－pass audio filters（ 10 to 100 kHz ）with multiple poles are usually needed．Because the CW Doppler signal ranges from 20 Hz to 20 kHz ，noise under this range is critical．Consequently，low－noise audio operational amplifiers are suitable to build these active filters for CW post－processing，that is，OPA1632 or OPA2211．To find more filter design techniques，see www．ti．com．For the TI active filter design tool，see http：／／focus．ti．com／docs／toolsw／folders／print／filter－designer．html．
The filtered audio CW I／Q signals are sampled by audio ADCs and processed by DSP or PC．Although CW signal frequency is from 20 Hz to 20 kHz ，higher sampling rate ADCs are still preferred for further decimation and SNR enhancement．Due to the large dynamic range of CW signals，high resolution ADCs（ $\geq 16$ bit）are required， such as ADS8881（ 18bit，1MSPS），ADS8413（2 MSPS，16－bit，92－dBFS SNR）and ADS8472（1 MSPS，16－bit， $95-\mathrm{dBFS}$ SNR）．ADCs for in－phase and quadrature－phase channels must be strictly matched，not only amplitude matching but also phase matching，in order to achieve the best I／Q matching．In addition，the in－phase and quadrature ADC channels must be sampled simultaneously．

## 11．2．2．4 Low Frequency Support

In addition，the signal chain of the AFE5812 can handle signal frequency lower than 100 kHz ，which enables the AFE5812 to be used in both sonar and medical applications．The PGA integrator has to be turned off in order to enable the low frequency support．Meanwhile，a large capacitor like $1 \mu \mathrm{~F}$ can be used for setting low corner frequency of the LNA DC offset correction circuit as shown in 图62．See 图 59 to find AFE5812＇s low frequency response．

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## 11．2．2．5 ADC Operation

## 11．2．2．5．1 ADC Clock Configurations

To ensure that the aperture delay and jitter are the same for all channels，the AFE5812 uses a clock tree network to generate individual sampling clocks for each channel．The clock，for all the channels，are matched from the source point to the sampling circuit of each of the eight internal ADCs．The variation on this delay is described in the aperture delay parameter of the output interface timing．Its variation is given by the aperture jitter number of the same table．


图 109．ADC Clock Distribution Network
The AFE5812 ADC clock input can be driven by differential clocks（sine wave，LVPECL，or LVDS）or singled clocks（LVCMOS）similar to CW clocks as shown in 图 107．In the single－end case，TI recommends that the use of low jitter square signals（LVCMOS levels，1．8－V amplitude）．See TI document SLYT075 for further details on the theory．
The jitter cleaner LMK048x，CDCM7005 or CDCE72010 is suitable to generate the AFE5812＇s ADC clock and ensure the performance for the14－bit ADC with 77－dBFS SNR．图 109 shows a clock distribution network．

## 11．2．2．5．2 ADC Reference Circuit

The ADC＇s voltage reference can be generated internally or provided externally．When the internal reference mode is selected，the REFP／M become output pins and should be floated．When $3[15]=1$ and $1[13]=1$ ，the device is configured to operate in the external reference mode in which the VREF＿IN pin should be driven with a $1.4-\mathrm{V}$ reference voltage and REFP／M must be left open．Because the input impedance of the VREF＿IN is high， no special drive capability is required for the $1.4-\mathrm{V}$ voltage reference

The digital beam－forming algorithm in an ultrasound system relies on gain matching across all receiver channels． A typical system would have about 12 octal AFEs on the board．In such a case，it is critical to ensure that the gain is matched，essentially requiring the reference voltages seen by all the AFEs to be the same．Matching references within the eight channels of a chip is done by using a single internal reference voltage buffer． Trimming the reference voltages on each chip during production ensures that the reference voltages are well－ matched across different chips．When the external reference mode is used，a solid reference plane on a PCB can ensure minimal voltage variation across devices．More information on voltage reference design can be found in the document SLYT339．

The dominant gain variation in the AFE5812 comes from the VCA gain variation．The gain variation contributed by the ADC reference circuit is much smaller than the VCA gain variation．Hence，in most systems，using the ADC internal reference mode is sufficient to maintain good gain matching among multiple AFE5812s．In addition， the internal reference circuit without any external components achieves satisfactory thermal noise and phase noise performance．

## 11．2．3 Application Curves

图 110 show the output SNR of one AFE channel from VCNTL $=0 \mathrm{~V}$ and VCNTL $=1.2 \mathrm{~V}$ ，respectively，with an input signal at 5 MHz captured at a sample rate of 50 MHz ．VCNTL $=0 \mathrm{~V}$ represents far field while VCNTL $=1.2$ V represents near field．图 111 shows the CW phase noise or dyanmic range of a singe AFE channel．


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### 11.3 Do's and Don'ts

### 11.3.1 Driving the inputs (analog or digital) beyond the power-supply rails

For device reliability, an input must not go more than 300 mV below the ground pins or 300 mV above the supply pins as suggested in the Absolute Maximum Ratings table. Exceeding these limits, even on a transient basis, can cause faulty or erratic operation and can impair device reliability.

### 11.3.2 Driving the device signal input with an excessively high level signal

The device offers consistent and fast overload recovery with a $6-\mathrm{dB}$ overloaded signal. For very large overload signals ( $>6 \mathrm{~dB}$ of the linear input signal range), TI recommends back-to-back Schottky clamping diodes at the input to limit the amplitude of the input signal. Refer to the LNA Input Coupling and Decoupling section for more details.

### 11.3.3 Driving the VCNTL signal with an excessive noise source

Noise on the VCNTL signal gets directly modulated with the input signal and causes higher output noise and reduction in SNR performance. Maintain a noise level for the VCNTL signal as discussed in the VoltageControlled Attenuator section.

### 11.3.4 Using a clock source with excessive jitter, an excessively long input clock signal trace, or having other signals coupled to the ADC or CW clock signal trace

These situations cause the sampling interval to vary, causing an excessive output noise and a reduction in SNR performance. For a system with multiple devices, the clock tree scheme must be used to apply an ADC or CW clock. Refer to the ADC Clock Configurations section for clock mismatch between devices, which can lead to latency mismatch and reduction in SNR performance. Clocks generated by FPGA may include excessive jitter and must be evaluated carefully before driving ADC or CW circuits.

### 11.3.5 LVDS routing length mismatch

The routing length of all LVDS lines routing to the FPGA must be matched to avoid any timing related issue. For systems with multiple devices, the LVDS serialized data clock (DCLKP, DCLKM) and the frame clock (FCLKP, FCLKM) of each individual device must be used to deserialize the corresponding LVDS serialized data (DnP, DnM).

### 11.3.6 Failure to provide adequate heat removal

Use the appropriate thermal parameter listed in the Thermal Information table and an ambient, board, or case temperature in order to calculate device junction temperature. A suitable heat removal technique must be used to keep the device junction temperature below the maximum limit of $105^{\circ} \mathrm{C}$.

## 12 Power Supply Recommendations

## 12．1 Power／Performance Optimization

The AFE5812 has options to adjust power consumption and meet different noise performances．This feature would be useful for portable systems operated by batteries when low power is more desired．Refer to characteristics information listed in the Electrical Characteristics as well as the Typical Characteristics．

## 12．2 Power Management Priority

Power management plays a critical role to extend battery life and ensure long operation time．The AFE5812 has fast and flexible power－down and power－up control which can maximize battery life．The AFE5812 can be powered down or up through external pins or internal registers．表 30 indicates the affected circuit blocks and priorities when the power management is invoked．The higher priority controls can overwrite the lower priority controls．
In the device，all the power－down controls are logically ORed to generate final power down for different blocks． The higher priority controls can cover the lower priority controls．

表 30．Power Management Priority

|  | Name | Blocks | Priority |
| :---: | :---: | :---: | :---: |
| Pin | PDN＿GLOBAL | All | High |
| Pin | PDN＿VCA | LNA＋VCAT＋PGA | Medium |
| Register | VCA＿PARTIAL＿PDN | LNA＋VCAT＋PGA | Low |
| Register | VCA＿COMPLETE＿PDN | LNA＋VCAT＋PGA | Medium |
| Pin | PDN＿ADC | ADC | Medium |
| Register | ADC＿PARTIAL＿PDN | ADC | Low |
| Register | ADC＿COMPLETE＿PDN | ADC | Medium |
| Register | PDN＿VCAT＿PGA | VCAT＋PGA | Lowest |
| Register | PDN＿LNA | LNA | Lowest |

## 12．3 Partial Power－Up and Power－Down Mode

The partial power－up and power－down mode is also called fast power－up and power－down mode．In this mode， most amplifiers in the signal path are powered down，while the internal reference circuits remain active as well as the LVDS clock circuit，that is，the LVDS circuit still generates its frame and bit clocks．
The partial power－down function allows the AFE5812 to wake up from a low－power state quickly．This configuration ensures that the external capacitors are discharged slowly；thus，a minimum wake－up time is needed as long as the charges on those capacitors are restored．The VCA wake－up response is typically about 2 $\mu \mathrm{s}$ or $1 \%$ of the power－down duration，whichever is larger．The longest wake－up time depends on the capacitors connected at INP and INM，because the wake－up time is the time required to recharge the capacitors to the desired operating voltages． $0.1 \mu \mathrm{~F}$ at INP and 15 nF at INM can give a wake－up time of 2.5 ms ．For larger capacitors，this time will be longer．The ADC wake－up time is about $1 \mu \mathrm{~s}$ ．Thus，the AFE5812 wake－up time is more dependent on the VCA wake－up time．This also assumes that the ADC clock has been running for at least $50 \mu \mathrm{~s}$ before normal operating mode resumes．The power－down time is instantaneous，less than $1 \mu \mathrm{~s}$ ．
This fast wake－up response is desired for portable ultrasound applications in which the power saving is critical． The pulse repetition frequency of an ultrasound system could vary from 50 kHz to 500 Hz ，while the imaging depth（that is，the active period for a receive path）varies from $10 \mu \mathrm{~s}$ to hundreds of $\mu \mathrm{s}$ ．The power saving can be significant when a system＇s PRF is low．In some cases，only the VCA would be powered down while the ADC keeps running normally to ensure minimal impact to FPGAs．
In the partial power－down mode，the AFE5812 typically dissipates only $26 \mathrm{~mW} / \mathrm{ch}$ ，representing an $80 \%$ power reduction compared to the normal operating mode．This mode can be set using either pins（PDN＿VCA and PDN＿ADC）or register bits（VCA＿PARTIAL＿PDN and ADC＿PARTIAL＿PDN）．

## 12．4 Complete Power－Down Mode

To achieve the lowest power dissipation of $0.7 \mathrm{~mW} / \mathrm{CH}$ ，the AFE5812 can be placed into a complete power－down mode．This mode is controlled through the registers ADC＿COMPLETE＿PDN，VCA＿COMPLETE＿PDN，or PDN＿GLOBAL pin．In the complete power－down mode，all circuits including reference circuits within the AFE5812 are powered down，and the capacitors connected to the AFE5812 are discharged．The wake－up time depends on the time needed to recharge these capacitors．The wake－up time depends on the time that the AFE5812 spends in shutdown mode． $0.1 \mu \mathrm{~F}$ at INP and 15 nF at INM can give a wake－up time close to 2.5 ms ．

## 注

When the complete power－down mode is enabled，the digital demodulator may lose register settings．Therefore，it is required to reconfigure the demodulator registers，filter coefficient memory，and profile memory after exiting the complete power－down mode．

## 12．5 Power Saving in CW Mode

Usually，only half the number of channels in a system are active in the CW mode．Thus，the individual channel control through ADC＿PDN＿CH＜7：0＞and VCA＇s PDN＿CH＜7：0＞can power down unused channels and save power consumption greatly．Under the default register setting in CW mode，the voltage controlled attenuator， PGA，and ADC are still active．During the debug phase，both the PW and CW paths can run simultaneously．In real operation，these blocks need to be powered down manually．

## 13 Layout

### 13.1 Layout Guidelines

Proper grounding and bypassing, short lead length, and the use of ground and power-supply planes are particularly important for high-frequency designs. Achieving optimum performance with a high-performance device such as the AFE5812 requires careful attention to the PCB layout to minimize the effects of board parasitics and optimize component placement. A multilayer PCB usually ensures best results and allows convenient component placement. To maintain proper LVDS timing, all LVDS traces should follow a controlled impedance design. In addition, all LVDS trace lengths should be equal and symmetrical; TI recommends to keep trace length variations less than 150 mil ( 0.150 inch or 3.81 mm ).
To avoid noise coupling through supply pins, it is recommended to keep sensitive input net classes, such as INM, INP, ACT pins, away from AVDD 3.3 V, AVDD_5V, DVDD, AVDD_ADC, DVDD_LDO1/2 nets or planes. For example, vias connected to these pins should NOT be routed across any supply plane. That is to avoid power planes under INM, INP, and ACT pins.
In addition, appropriate delay matching should be considered for the CW clock path, especially in systems with high channel count. For example, if clock delay is half of the $16 \times$ clock period, a phase error of $22.5^{\circ}$ could exist. Thus, the timing delay difference among channels contributes to the beamformer accuracy.
Additional details on BGA PCB layout techniques can be found in the TI application report MicroStar BGA Packaging Reference Guide (SSYZ015), which can be downloaded from www.ti.com.

## 13．2 Layout Example



图 112．Layout Example

## Layout Example（接下页）



图 113．Layout Example

Layout Example（接下页）


图 114．Layout Example

## Layout Example（接下页）



图 115．Layout Example

## 14 器件和文档支持

## 14.1 文档支持

14．1．1 相关文档
《MicroStar BGA 封装参考指南》，SSYZ015
《高速时钟数据转换器》，SLYT075
《宽带差分互阻抗 DAC 输出设计》，SBAA150
TI 有源滤波器设计工具，WEBENCH® Filter Designer
《AFE5818 数据表》，SBAS624
《AFE5816 数据表》，SBAS688
《CDCM7005 数据表》，SCAS793
《CDCE72010 数据表》，SCAS858
《TLV5626 数据表》，SLAS236
《DAC7821 数据表》，SBAS365
《THS413x 数据表》，SLOS318
《OPA1632 数据表》，SBOS286
《LMK048x 数据表》，SNAS489
《OPA2211 数据表》，SBOS377
《ADS8413 数据表》，SLAS490
《ADS8472 数据表》，SLAS514
《SN74AUP1T04 数据表》，SCES800
《ISO7240 数据表》，SLLS868

## 14.2 商标

All trademarks are the property of their respective owners．
14.3 静电放电警告

这些装置包含有限的内置 ESD 保护。存储或装卸时，应将导线一起截短或将装置放置于导电泡棉中，以防止 MOS 门极遭受静电损伤。

## 14.4 术语表

SLYZ022－TI 术语表。
这份术语表列出并解释术语，首字母缩略词和定义。

## 15 机械封装和可订购信息

以下页中包括机械封装和可订购信息。 这些信息是针对指定器件可提供的最新数据。这些数据会在无通知且不对本文档进行修订的情况下发生改变。欲获得该数据表的浏览器版本，请查阅左侧的导航栏。

## PACKAGING INFORMATION

| Orderable Device | Status <br> (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan <br> (2) | Lead finish/ Ball material <br> (6) | MSL Peak Temp <br> (3) | Op Temp ( ${ }^{\circ} \mathrm{C}$ ) | Device Marking <br> (4/5) | Samples |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AFE5812ZCF | ACTIVE | NFBGA | ZCF | 135 | 160 | RoHS \& Green | SNAGCU | Level-3-260C-168 HR | -40 to 85 | AFE5812 | Samples |

${ }^{(1)}$ The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.
${ }^{(2)}$ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed $0.1 \%$ by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
Green: Tl defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement
${ }^{(3)}$ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
${ }^{(4)}$ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device
${ }^{(5)}$ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
${ }^{(6)}$ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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## TRAY



Chamfer on Tray corner indicates Pin 1 orientation of packed units.
*All dimensions are nominal

| Device | Package Name | Package Type | Pins | SPQ | Unit array matrix | Max temperature ( $\left.{ }^{\circ} \mathrm{C}\right)$ | L (mm) | $\begin{gathered} \mathrm{W} \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \mathrm{KO} \\ (\mu \mathrm{~m}) \end{gathered}$ | $\begin{gathered} \mathrm{P} 1 \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \mathrm{CL} \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \text { CW } \\ (\mathrm{mm}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AFE5812ZCF | ZCF | NFBGA | 135 | 160 | $10 \times 16$ | 150 | 315 | 135.9 | 7620 | 19.2 | 13.5 | 10.35 |



NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
B. This drawing is subject to change without notice.
C. This is a lead-free solder ball design.

## 重要声明和免责声明

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[^0]:    （1）When programming the SPI，8－bit address is required．This table and the following sections only list the Add＿Bit5 to Add＿Bit0．The Add＿Bit7＝SCID1＿SEL and Add＿Bit6＝SCID0＿SEL need to be appended as 11，10，or 01，which determines if SubChip1 or SubChip0 is being programmed．If SCID1＿SEL，SCID0＿SEL＝11，then both subchips get written with the same register value．See 表 3 ．
    （2）Reserved register bits must be programmed based on their descriptions．Unlisted register bits must be programmed as zeros．
    （3）ADC CLK is required to access the demodulation registers．

