

TLV522 双路毫微功耗、500nA、RRIO CMOS 运算放大器

1 特性

- 无与伦比的性价比
- 宽电源电压范围：1.7V 至 5.5V
- 低电源电流：500nA
- 良好偏移电压：4mV（最大值）
- 良好 $TcVos$ ：1.5 μ V/ $^{\circ}$ C
- 增益带宽：8MHz
- 轨到轨输入和输出 (RRIO)
- 单位增益稳定
- 低输入偏置电流：1pA
- 强化的电磁干扰 (EMI) 保护
- 温度范围：-40 $^{\circ}$ C 至 125 $^{\circ}$ C
- 8 引脚超薄小外形尺寸 (VSSOP) 封装

2 应用

- 个人健康监视器
- 电池组
- 太阳能或能量采集系统
- PIR、烟雾、燃气和火灾检测系统
- 电池供电物联网 (IoT) 设备
- 远程传感器/无线传感节点
- 可穿戴设备
- 血糖监测

3 说明

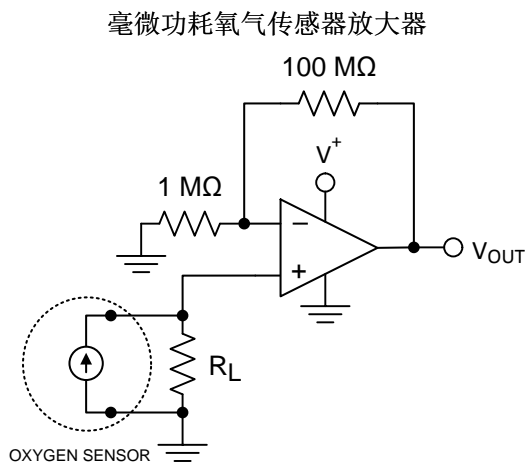
TLV522 是一款 500nA 双路毫微功耗运算放大器，属于 TI 的超值性能毫微功耗运算放大器系列。TLV522 具有 8kHz 增益带宽和 500nA 静态电流，是楼宇自动化和遥感节点中的常见电池供电类应用的理想选择。该器件的互补金属氧化物半导体 (CMOS) 输入级可实现超低 I_{BIAS} ，从而降低兆欧级反馈电阻拓扑（例如高阻抗光电二极管和充电检测应用）中经常引入的误差。此外，内置的电磁干扰 (EMI) 保护可降低器件对手机、WiFi、无线电发射器、RFID 阅读器所发出意外射频 (RF) 信号的敏感度。

TLV522 采用 8 引脚 VSSOP (MSOP) 封装，运行温度范围为 -40 $^{\circ}$ C 至 125 $^{\circ}$ C。

器件信息⁽¹⁾

器件型号	封装	封装尺寸 (标称值)
TLV522	VSSOP (8)	3.00mm x 3.00mm

(1) 要了解所有可用封装，请见数据表末尾的可订购产品附录。



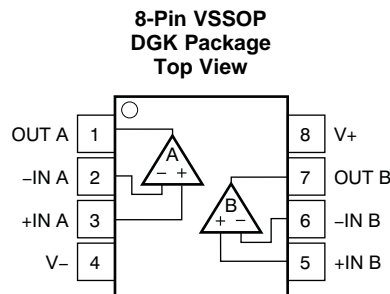
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4 修订历史记录

日期	修订版本	注释
2016 年 5 月	*	首次发布。

5 Pin Configuration and Functions



Pin Functions

PIN		I/O	DESCRIPTION
PIN	NAME		
1	OUT A	O	Channel A Output
2	-IN A	I	Channel A Inverting Input
3	+IN A	I	Channel A Non-Inverting Input
4	V-	P	Negative (lowest) power supply
5	+IN B	I	Channel B Non-Inverting Input
6	-IN B	I	Channel B Inverting Input
7	OUT B	O	Channel B Output
8	V+	P	Positive (highest) power supply

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾⁽²⁾⁽³⁾

		MIN	MAX	UNIT
Supply voltage, V+ to V–		-0.3	6	V
Signal input pins	Voltage ⁽²⁾	V– – 0.3	V+ + 0.3	V
	Current ⁽²⁾	-10	10	mA
Output short current		Continuous ⁽⁴⁾		
Junction temperature		-40	150	°C
Storage temperature, T _{stg}		-65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) Input pins are diode-clamped to the power-supply rails. Input signals that can swing more than 0.3 V beyond the supply rails should be current-limited to 10 mA or less.
- (3) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/Distributors for availability and specifications.
- (4) Short-circuit to V–.

6.2 ESD Ratings

		VALUE	UNIT
V _(ESD)	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins ⁽¹⁾	±2000
		Charged device model (CDM), per JEDEC specification JESD22-C101, all pins ⁽²⁾	±250

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Ratings

over operating free-air temperature range (unless otherwise noted)

	MIN	NOM	MAX	UNIT
Supply Voltage (V+ – V–)	1.7		5.5	V
Specified Temperature	-40		125	°C

6.4 Thermal Information

THERMAL METRIC ⁽¹⁾		TLV522 DGK (VSSOP) 8 PINS	UNIT
R _{θJA}	Junction-to-ambient thermal resistance	182.5	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	73.6	
R _{θJB}	Junction-to-board thermal resistance	104.1	
Ψ _{JT}	Junction-to-top characterization parameter	13.7	
Ψ _{JB}	Junction-to-board characterization parameter	102.5	
R _{θJC(bot)}	Junction-to-case (bottom) thermal resistance	N/A	

- (1) For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, [SPRA953](#).

6.5 Electrical Characteristics

$T_A = 25^\circ\text{C}$, $V^+ = 3.3\text{ V}$, $V^- = 0\text{ V}$, $V_{CM} = V_O = V^+/2$, and $R_L > 1\text{ M}\Omega$, unless otherwise noted.

PARAMETER	TEST CONDITIONS	MIN	TYP ⁽¹⁾	MAX	UNIT
OFFSET VOLTAGE					
Input offset voltage (V_{OS})	$V_{CM} = 0.3\text{ V}$	-4	± 1	4	mV
	$V_{CM} = 3\text{ V}$	-4	± 1	4	
Drift (dV_{OS}/dT)			1.5		$\mu\text{V}/^\circ\text{C}$
Power-Supply Rejection Ratio (PSRR)	$V^+ = 1.8\text{ V to } 3.3\text{ V}$, $V_{CM} = 0.3\text{ V}$	80	109		dB
INPUT VOLTAGE RANGE					
Common-Mode voltage range (V_{CM})	CMRR $\geq 62\text{ dB}$	0		3.3	V
Common-Mode Rejection Ratio (CMRR)	$0\text{ V} < V_{CM} < 3.3\text{ V}$	62	90		dB
	$0\text{ V} < V_{CM} < 2.2\text{ V}$		90		
INPUT BIAS CURRENT					
Input bias current (I_{BIAS})			± 1		pA
Input offset current (I_{OS})			± 0.1		
INPUT IMPEDANCE					
Differential			$10^{13} \parallel 2.5$		$\Omega \parallel \text{pF}$
Common mode			$10^{13} \parallel 2.5$		
NOISE					
Input voltage noise density, $f = 1\text{ kHz}$ (e_n)			300		$\text{nV}/\sqrt{\text{Hz}}$
Current noise density, $f = 1\text{ kHz}$ (i_n)			65		$\text{fA}/\sqrt{\text{Hz}}$
OPEN-LOOP GAIN					
Open-loop voltage gain (A_{OL})	$V^+ = 5\text{ V}$ $R_L = 100\text{ k}\Omega$ to $V^+/2$, $0.5\text{ V} < V_O < 4.5\text{ V}$	91	101		dB
OUTPUT					
Voltage output swing from positive rail	$V^+ = 1.8\text{ V}$, $R_L = 100\text{ k}\Omega$ to $V^+/2$		3	20	mV
Voltage output swing from negative rail	$V^+ = 1.8\text{ V}$, $R_L = 100\text{ k}\Omega$ to $V^+/2$		2	20	
Output current sourcing	Sourcing, $V^+ = 1.8\text{ V}$ V_O to V^- , $V_{IN}(\text{diff}) = 100\text{ mV}$	1	3		mA
Output current sinking	Sinking, $V^+ = 1.8\text{ V}$ V_O to V^+ , $V_{IN}(\text{diff}) = -100\text{ mV}$	1	5		
FREQUENCY RESPONSE					
Gain-bandwidth product (GBWP)	$C_L = 20\text{ pF}$		8		kHz
Slew rate (SR)	$G = +1$, Rising edge, $1V_{p-p}$, $C_L = 20\text{ pF}$		3.6		V/ms
	$G = +1$, Falling edge, $1V_{p-p}$, $C_L = 20\text{ pF}$		3.7		
POWER SUPPLY					
Quiescent current per channel (I_Q)	$V_{CM} = 0.3\text{ V}$, $I_O = 0$		500	800	nA

(1) Refer to [Typical Characteristics](#).

6.6 Typical Characteristics

$T_A = 25\text{ }^\circ\text{C}$, $V_{OUT} = V_{CM} = V_S/2$, $R_{LOAD} = 1\text{ M}\Omega$ connected to $V_S/2$, and $C_L = 20\text{ pF}$, unless otherwise noted.

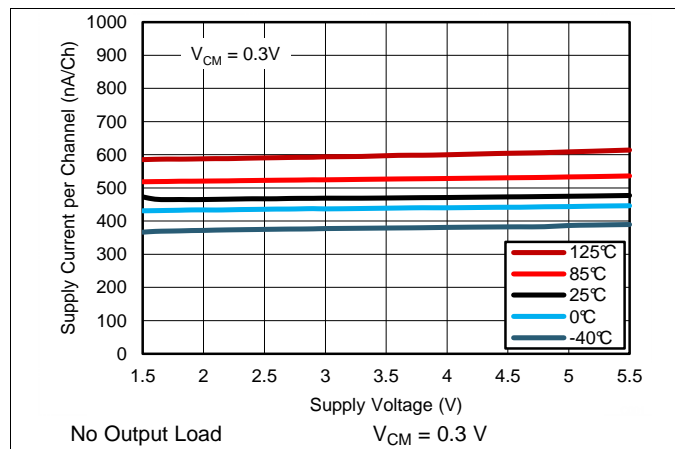


Figure 1. Supply Voltage vs Supply Current per Channel, Low Vcm

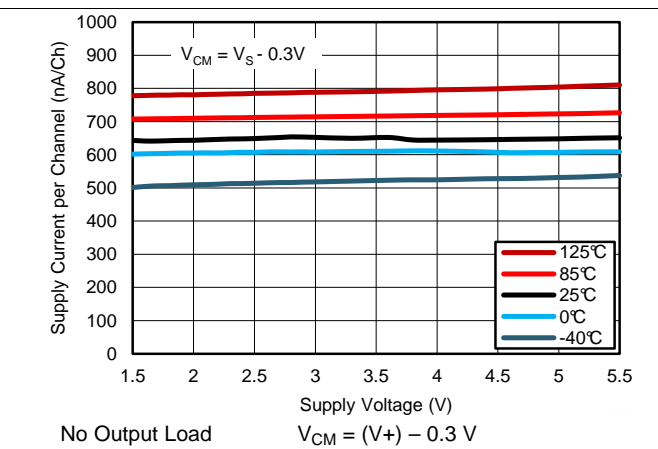


Figure 2. Supply Voltage vs Supply Current per Channel, High Vcm

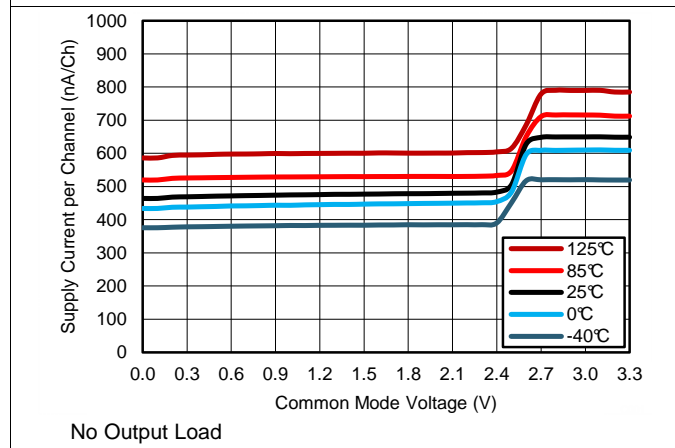


Figure 3. Supply Current vs Common Mode at 3.3 V

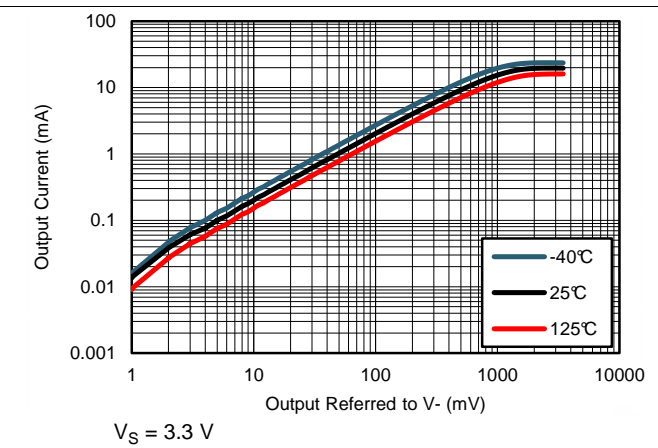


Figure 4. Output Sinking Current vs Output Swing at 3.3 V

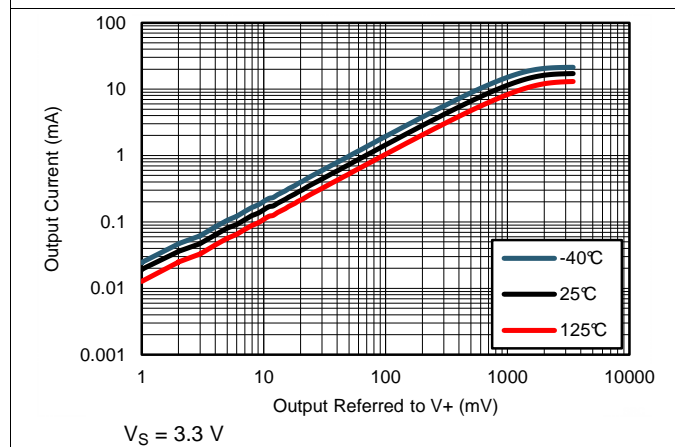


Figure 5. Output Sourcing Current vs Output Swing at 3.3 V

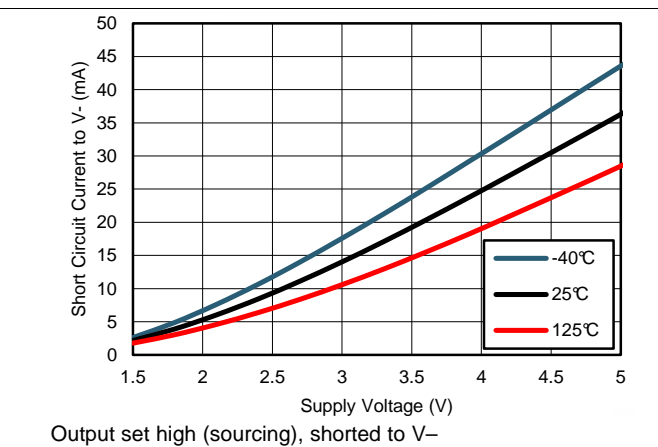


Figure 6. Output Short Circuit Current to V- vs Supply Voltage

Typical Characteristics (continued)

$T_A = 25\text{ }^\circ\text{C}$, $V_{OUT} = V_{CM} = V_S/2$, $R_{LOAD} = 1\text{ M}\Omega$ connected to $V_S/2$, and $C_L = 20\text{ pF}$, unless otherwise noted.

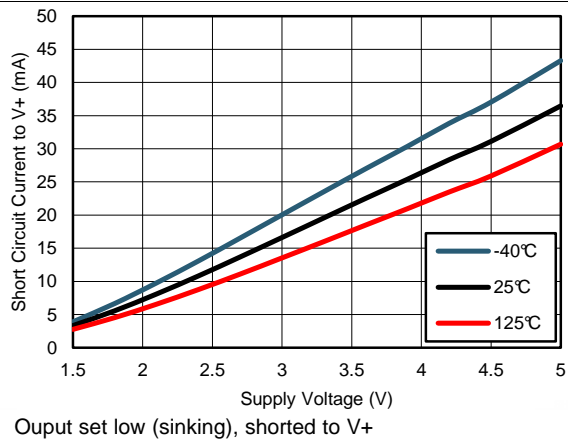


Figure 7. Output Short Circuit Current to V+ vs Supply Voltage
Output set low (sinking), shorted to V+

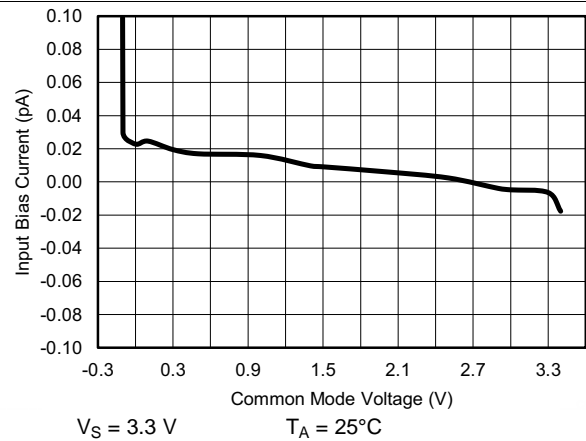


Figure 8. Input Bias Current vs Common Mode Voltage at 3.3 V

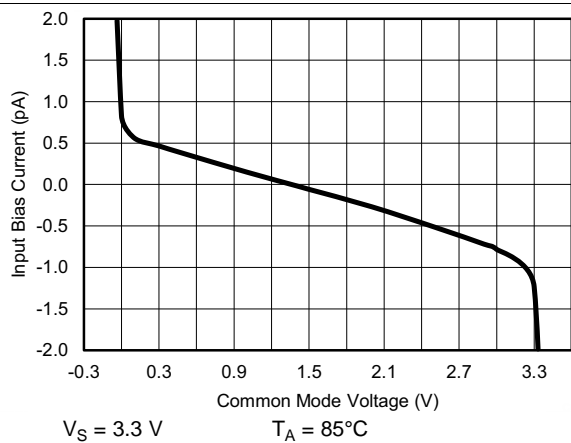


Figure 9. Input Bias Current vs Common Mode Voltage at 3.3 V

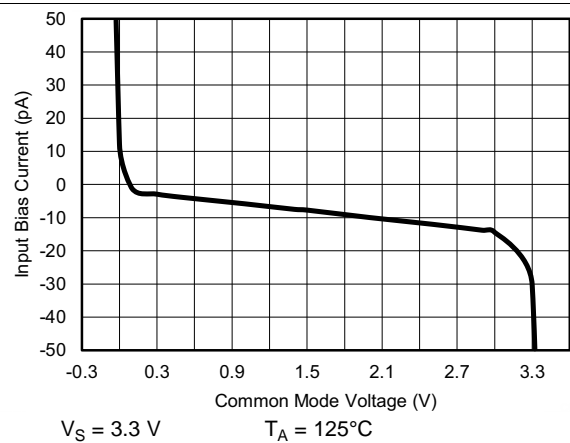


Figure 10. Input Bias Current vs Common Mode Voltage at 3.3 V

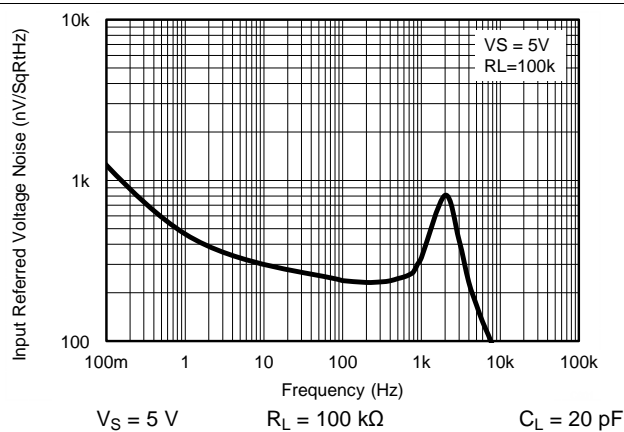


Figure 11. Input Referred Voltage Noise

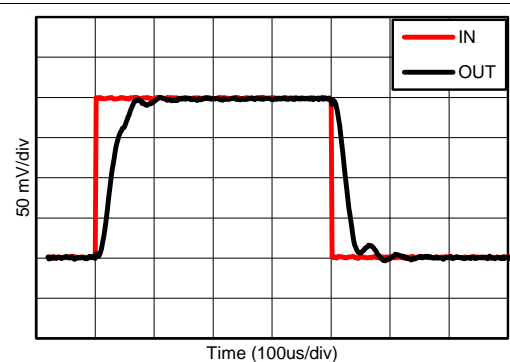
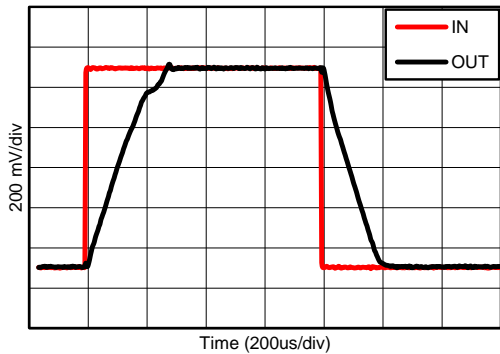


Figure 12. Pulse Response, 200mVpp at 1.8 V

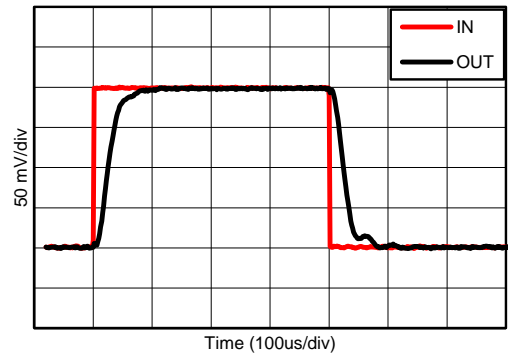
Typical Characteristics (continued)

$T_A = 25\text{ }^\circ\text{C}$, $V_{OUT} = V_{CM} = V_S/2$, $R_{LOAD} = 1\text{ M}\Omega$ connected to $V_S/2$, and $C_L = 20\text{ pF}$, unless otherwise noted.



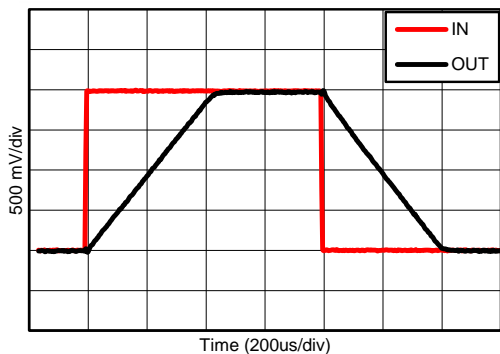
$V_S = \pm 0.9\text{ V}$ $R_L = 10\text{ M}\Omega$ $C_L = 20\text{ pF}$
 $G = +1$ $V_{IN} = \pm 500\text{ mV}$

Figure 13. Pulse Response, 1Vpp at 1.8V



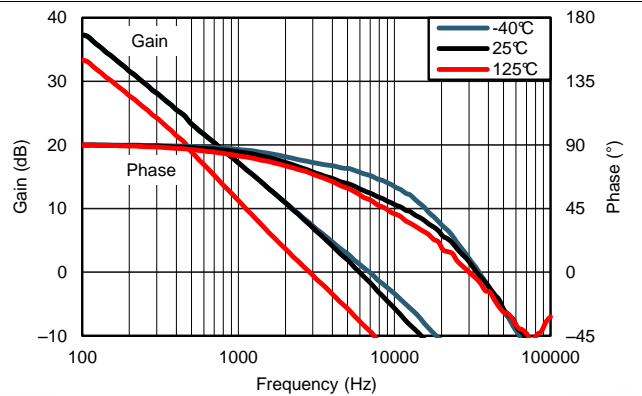
$V_S = \pm 2.5\text{ V}$ $R_L = 10\text{ M}\Omega$ $C_L = 20\text{ pF}$
 $G = +1$ $V_{IN} = \pm 100\text{ mV}$

Figure 14. Pulse Response, 200mVpp at 5V



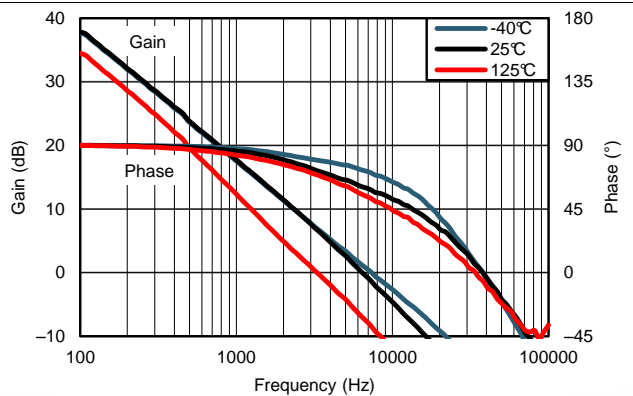
$V_S = \pm 2.5\text{ V}$ $R_L = 10\text{ M}\Omega$ $C_L = 20\text{ pF}$
 $G = +1$ $V_{IN} = \pm 1\text{ V}$

Figure 15. Pulse Response, 2Vpp at 5V



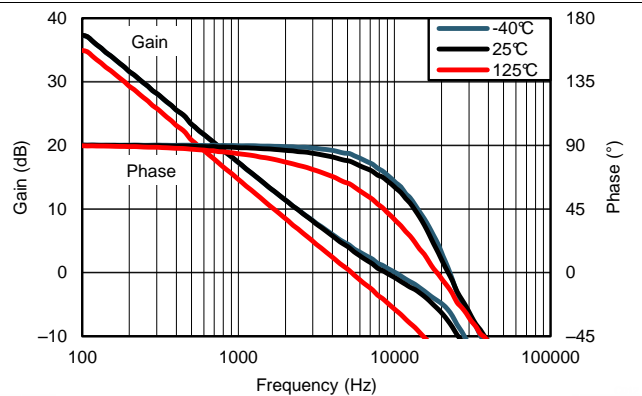
$V_S = 1.8\text{ V}$ $R_L = 100\text{ k}\Omega$ $C_L = 20\text{ pF}$

Figure 16. Gain and Phase vs Temperature at 1.8 V



$V_S = 5\text{ V}$ $R_L = 100\text{ k}\Omega$ $C_L = 20\text{ pF}$

Figure 17. Gain and Phase vs Temperature at 5 V



$V_S = 1.8\text{ V}$ $R_L = 1\text{ M}\Omega$ $C_L = 20\text{ pF}$

Figure 18. Gain and Phase vs Temperature at 1.8 V

Typical Characteristics (continued)

$T_A = 25\text{ }^\circ\text{C}$, $V_{OUT} = V_{CM} = V_S/2$, $R_{LOAD} = 1\text{ M}\Omega$ connected to $V_S/2$, and $C_L = 20\text{ pF}$, unless otherwise noted.

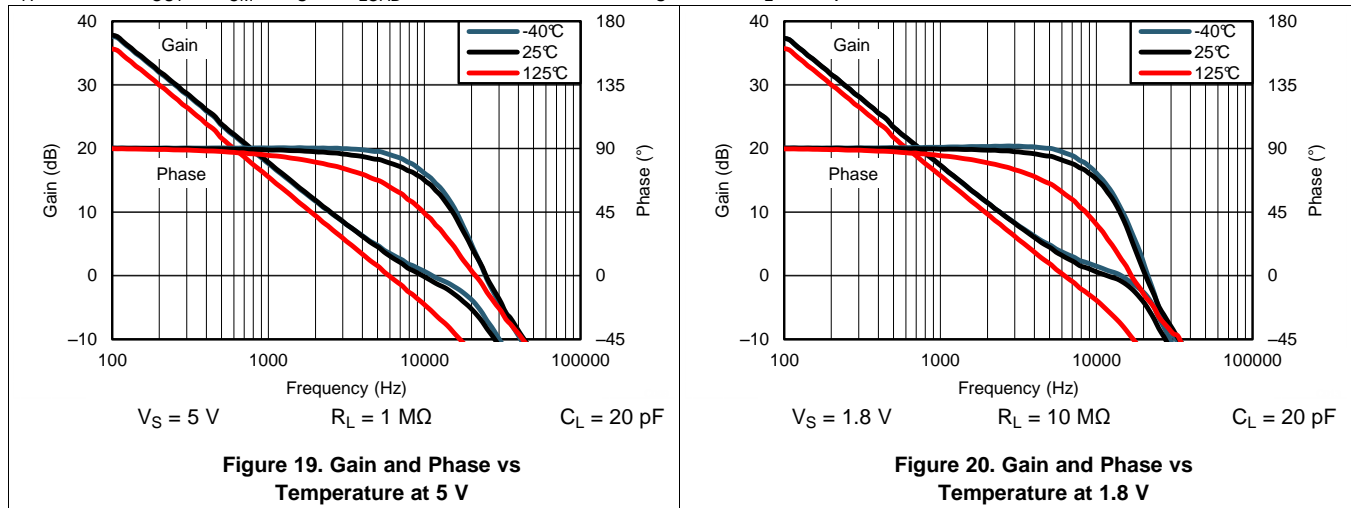


Figure 19. Gain and Phase vs Temperature at 5 V

Figure 20. Gain and Phase vs Temperature at 1.8 V

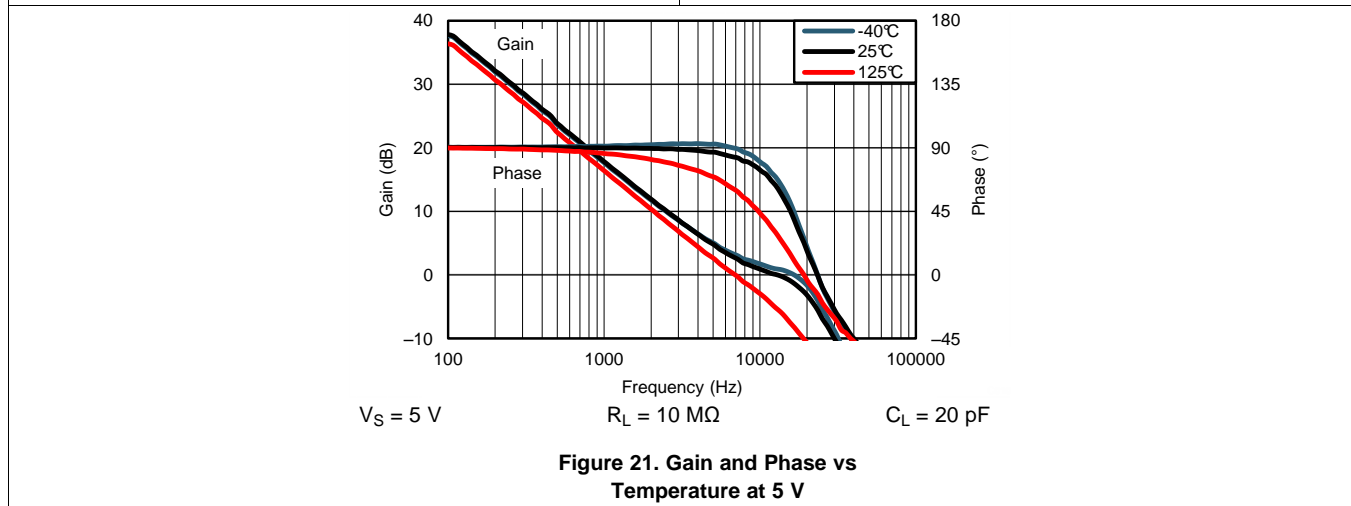


Figure 21. Gain and Phase vs Temperature at 5 V

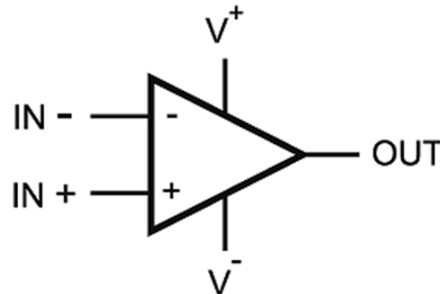
7 Detailed Description

7.1 Overview

The TLV522 dual op amplifier is unity-gain stable and can operate on a single supply, making it highly versatile and easy to use.

The TLV522 is fully specified and tested from 1.7 V to 5.5 V. Parameters that vary significantly with operating voltages or temperature are shown in the *Typical Characteristics* curves.

7.2 Functional Block Diagram



7.3 Feature Description

The amplifier's differential inputs consist of a non-inverting input (IN+) and an inverting input (IN-). The device amplifies only the difference in voltage between the two inputs, which is called the differential input voltage. The output voltage of the op-amp V_{OUT} is given by [Equation 1](#):

$$V_{OUT} = A_{OL} (IN^+ - IN^-) \quad (1)$$

where A_{OL} is the open-loop gain of the amplifier, typically around 100 dB.

7.4 Device Functional Modes

7.4.1 Rail-To-Rail Input

The input common-mode voltage range of the TLV522 extends to the supply rails. This is achieved with a complementary input stage — an N-channel input differential pair in parallel with a P-channel differential pair. The N-channel pair is active for input voltages close to the positive rail, typically $(V^+) - 800 \text{ mV}$ to 200 mV above the positive supply, while the P-channel pair is on for inputs from 300 mV below the negative supply to approximately $(V^+) - 800 \text{ mV}$. There is a small transition region, typically $(V^+) - 1.2 \text{ V}$ to $(V^+) - 0.8 \text{ V}$, in which both pairs are on. This 400 mV transition region can vary 200 mV with process variation. Within the 400 mV transition region PSRR, CMRR, offset voltage, offset drift, and THD may be degraded compared to operation outside this region.

7.4.2 Supply Current Changes Over Common Mode

Because of the ultra-low supply current, changes in common mode voltages will cause a noticeable change in the supply current as the input stages transition through the transition region, as shown in [Figure 22](#) below.

Device Functional Modes (continued)

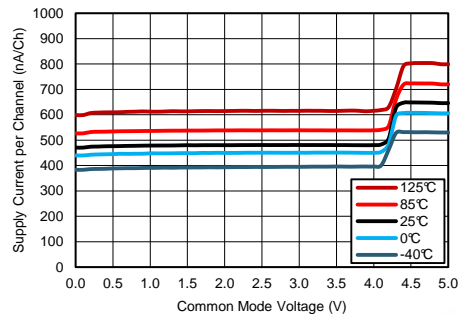


Figure 22. Supply Current Change Over Common Mode at 5 V

For the lowest supply current operation, keep the input common mode range between V^- and 1 V below V^+ .

7.4.3 Design Optimization With Rail-To-Rail Input

In most applications, operation is within the range of only one differential pair. However, some applications can subject the amplifier to a common-mode signal in the transition region. Under this condition, the inherent mismatch between the two differential pairs may lead to degradation of the CMRR and THD. The unity-gain buffer configuration is the most problematic as it will traverse through the transition region if a sufficiently wide input swing is required.

7.4.4 Design Optimization for Nanopower Operation

When designing for ultra-low power, choose system components carefully. To minimize current consumption, select large-value resistors. Any resistors will react with stray capacitance in the circuit and the input capacitance of the operational amplifier. These parasitic RC combinations can affect the stability of the overall system. A feedback capacitor may be required to assure stability and limit overshoot or gain peaking.

When possible, use AC coupling and AC feedback to reduce static current draw through the feedback elements. Use film or ceramic capacitors since large electrolytics may have static leakage currents in the tens to hundreds of nanoamps.

7.4.5 Common-Mode Rejection

The CMRR for the TLV522 is specified in two ways so the best match for a given application may be used. First, the CMRR of the device in the common-mode range below the transition region ($V_{CM} < (V^+) - 1.1$ V) is given. This specification is the best indicator of the capability of the device when the application requires use of one of the differential input pairs. Second, the CMRR at $V_S = 3.3$ V over the entire common-mode range is specified.

7.4.6 Output Stage

The TLV522 output voltage swings 3 mV from rails at 3.3 V supply, which provides the maximum possible dynamic range at the output. This is particularly important when operating on low supply voltages.

The TLV522 Maximum Output Voltage Swing defines the maximum swing possible under a particular output load.

7.4.7 Driving Capacitive Load

The TLV522 is internally compensated for stable unity gain operation, with a 8 kHz typical gain bandwidth. However, the unity gain follower is the most sensitive configuration to capacitive load. The combination of a capacitive load placed directly on the output of an amplifier along with the amplifier's output impedance creates a phase lag, which reduces the phase margin of the amplifier. If the phase margin is significantly reduced, the response will be under damped which causes peaking in the transfer and, when there is too much peaking, the op amp might start oscillating.

Device Functional Modes (continued)

In order to drive heavy (>50pF) capacitive loads, an isolation resistor, R_{ISO} , should be used, as shown in Figure 23. By using this isolation resistor, the capacitive load is isolated from the amplifier's output. The larger the value of R_{ISO} , the more stable the amplifier will be. If the value of R_{ISO} is sufficiently large, the feedback loop will be stable, independent of the value of C_L . However, larger values of R_{ISO} result in reduced output swing and reduced output current drive.

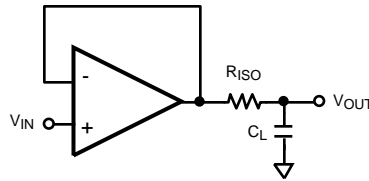


Figure 23. Resistive Isolation of Capacitive Load

8 Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

The TLV522 is a ultra-low power operational amplifier that provides 8 kHz bandwidth with only 490 nA quiescent current, and near precision offset and drift specifications at a low cost. These rail-to-rail input and output amplifiers are specifically designed for battery-powered applications. The input common-mode voltage range extends to the power-supply rails and the output swings to within millivolts of the rails, maintaining a wide dynamic range.

8.2 Typical Application: 60 Hz Twin "T" Notch Filter

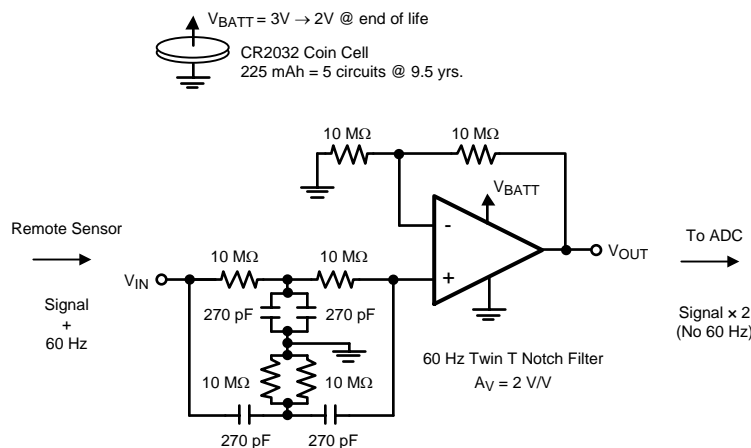


Figure 24. 60 Hz Notch Filter

8.2.1 Design Requirements

Small signals from transducers in remote and distributed sensing applications commonly suffer strong 60 Hz interference from AC power lines. The circuit of Figure 24 notches out the 60 Hz and provides a gain $A_V = 2$ for the sensor signal represented by a 1 kHz sine wave. Similar stages may be cascaded to remove 2nd and 3rd harmonics of 60 Hz. Thanks to the nA power consumption of the TLV522, even 5 such circuits can run for 9.5 years from a small CR2032 lithium cell. These batteries have a nominal voltage of 3 V and an end of life voltage of 2 V. With an operating voltage from 1.7 V to 5.5 V the TLV522 can function over this voltage range.

8.2.2 Detailed Design Procedure

The notch frequency is set by:

$$F_0 = 1 / 2\pi RC. \tag{2}$$

To achieve a 60 Hz notch use $R = 10 \text{ M}\Omega$ and $C = 270 \text{ pF}$. If eliminating 50 Hz noise, which is common in European systems, use $R = 11.8 \text{ M}\Omega$ and $C = 270 \text{ pF}$.

The Twin T Notch Filter works by having two separate paths from V_{IN} to the amplifier's input. A low frequency path through the series input resistors and another separate high frequency path through the series input capacitors. However, at frequencies around the notch frequency, the two paths have opposing phase angles and the two signals will tend to cancel at the amplifier's input.

Typical Application: 60 Hz Twin "T" Notch Filter (continued)

To ensure that the target center frequency is achieved and to maximize the notch depth (Q factor) the filter needs to be as balanced as possible. To obtain circuit balance, while overcoming limitations of available standard resistor and capacitor values, use passives in parallel to achieve the 2C and R/2 circuit requirements for the filter components that connect to ground.

To make sure passive component values stay as expected clean board with alcohol, rinse with deionized water, and air dry. Make sure board remains in a relatively low humidity environment to minimize moisture which may increase the conductivity of board components. Also large resistors come with considerable parasitic stray capacitance which effects can be reduced by cutting out the ground plane below components of concern.

Large resistors are used in the feedback network to minimize battery drain. When designing with large resistors, resistor thermal noise, op amp current noise, as well as op amp voltage noise, must be considered in the noise analysis of the circuit. The noise analysis for the circuit in [Figure 24](#) can be done over a bandwidth of 2 kHz, which takes the conservative approach of overestimating the bandwidth (TLV522 typical GBW/A_V is lower). The total noise at the output is approximately 800 μVpp, which is excellent considering the total consumption of the circuit is only 900 nA. The dominant noise terms are op amp voltage noise, current noise through the feedback network (430 μVpp), and current noise through the notch filter network (280 μVpp). Thus the total circuit's noise is below 1/2 LSB of a 10-bit system with a 2 V reference, which is 1 mV.

8.2.3 Application Curve

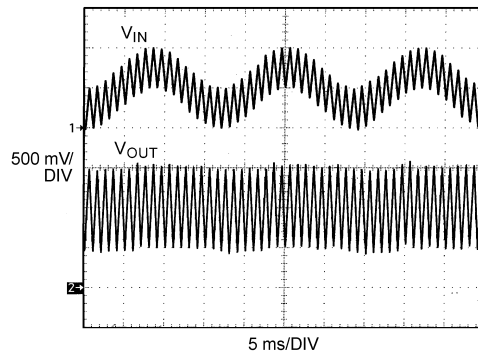


Figure 25. 60 Hz Notch Filter Waveform

8.3 Do's and Don'ts

Do properly bypass the power supplies.

Do add series resistance to the output when driving capacitive loads, particularly cables, MUX and ADC inputs.

Do add series current limiting resistors and external schottky clamp diodes if input voltage is expected to exceed the supplies. Limit the current to 1 mA or less (1 KΩ per volt).

9 Power Supply Recommendations

The TLV522 is specified for operation from 1.7 V to 5.5 V (± 0.85 V to ± 2.75 V) over a -40°C to 125°C temperature range. Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in the [Typical Characteristics](#).

CAUTION

Supply voltages larger than 6 V can permanently damage the device.

For proper operation, the power supplies must be properly decoupled. For decoupling the supply lines it is suggested that 10 nF capacitors be placed as close as possible to the operational amplifier power supply pins. For single supply, place a capacitor between V^+ and V^- supply leads. For dual supplies, place one capacitor between V^+ and ground, and one capacitor between V^- and ground.

If your application expects signals above (> 1 kHz) we recommend you use extra supply filtering.

Extra filtering on the power supply input is recommended when presence of signals with frequency above one kHz (> 1 kHz) on the line is expected. Example of such signal sources are high-frequency switching supplies.

10 Layout

10.1 Layout Guidelines

The V^+ pin should be bypassed to ground with a low ESR capacitor.

The optimum placement is closest to the V^+ and ground pins.

Care should be taken to minimize the loop area formed by the bypass capacitor connection between V^+ and ground.

The ground pin should be connected to the PCB ground plane at the pin of the device.

The feedback components should be placed as close to the device as possible to minimize strays.

There is an internal electrical connection between the exposed Die Attach Pad (DAP) and the V^- pin. For best performance the DAP should be connected to the exact same potential as the V^- pin. Do not use the DAP as the primary V^- supply. Floating the DAP pad is not recommended. The DAP and V^- pin should be joined directly as shown in the [Layout Example](#).

10.2 Layout Example

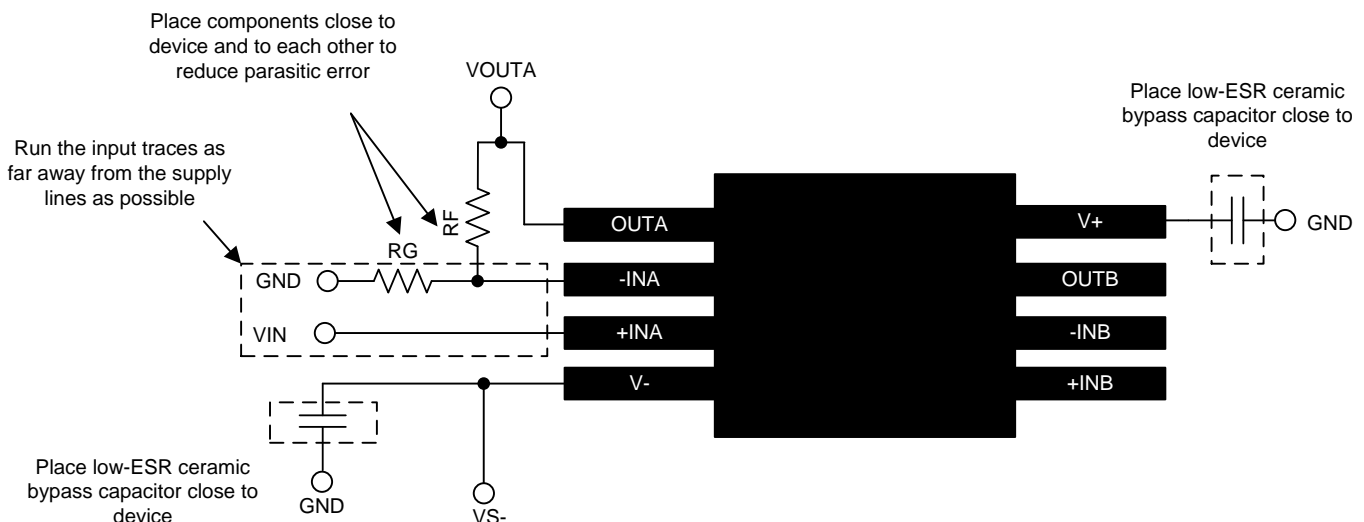


Figure 26. Layout Example (Top View)

11 器件和文档支持

11.1 器件支持

11.1.1 开发支持

TINA-TI 基于 SPICE 的模拟仿真程序, <http://www.ti.com.cn/tool/cn/tina-ti>

DIP 适配器评估模块, <http://www.ti.com.cn/tool/cn/dip-adapter-evm>

TI 通用运行放大器评估模块, <http://www.ti.com.cn/tool/cn/opampevm>

TI FilterPro 滤波器设计软件, <http://www.ti.com.cn/tool/cn/filterpro>

11.2 文档支持

11.2.1 相关文档

相关文档如下:

- AN-1798 《设计电化学传感器》, [SNOA514](#)
- AN-1803 《互阻抗放大器设计注意事项》, [SNOA515](#)
- AN-1852 《设计 pH 电极》, [SNOA529](#)
- 《直观补偿互阻抗放大器》, [SBOA055](#)
- 《高速运算放大器互阻抗注意事项》, [SBOA112](#)
- 《FET 互阻抗放大器噪声分析》, [SBOA060](#)
- 《电路板布局布线技巧》, [SLOA089](#)
- 《运算放大器应用 手册》, [SBOA092](#)

11.3 社区资源

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11.5 静电放电警告



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11.6 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

12 机械、封装和可订购信息

以下页中包括机械封装和可订购信息。这些信息是针对指定器件可提供的最新数据。这些数据会在无通知且不对本档进行修订的情况下发生改变。欲获得该数据表的浏览器版本, 请查阅左侧的导航栏。

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Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TLV522DGKR	ACTIVE	VSSOP	DGK	8	2500	RoHS & Green	NIPDAUAG	Level-1-260C-UNLIM	-40 to 125	SL V522	
TLV522DGKT	ACTIVE	VSSOP	DGK	8	250	RoHS & Green	NIPDAUAG	Level-1-260C-UNLIM	-40 to 125	SL V522	

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(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

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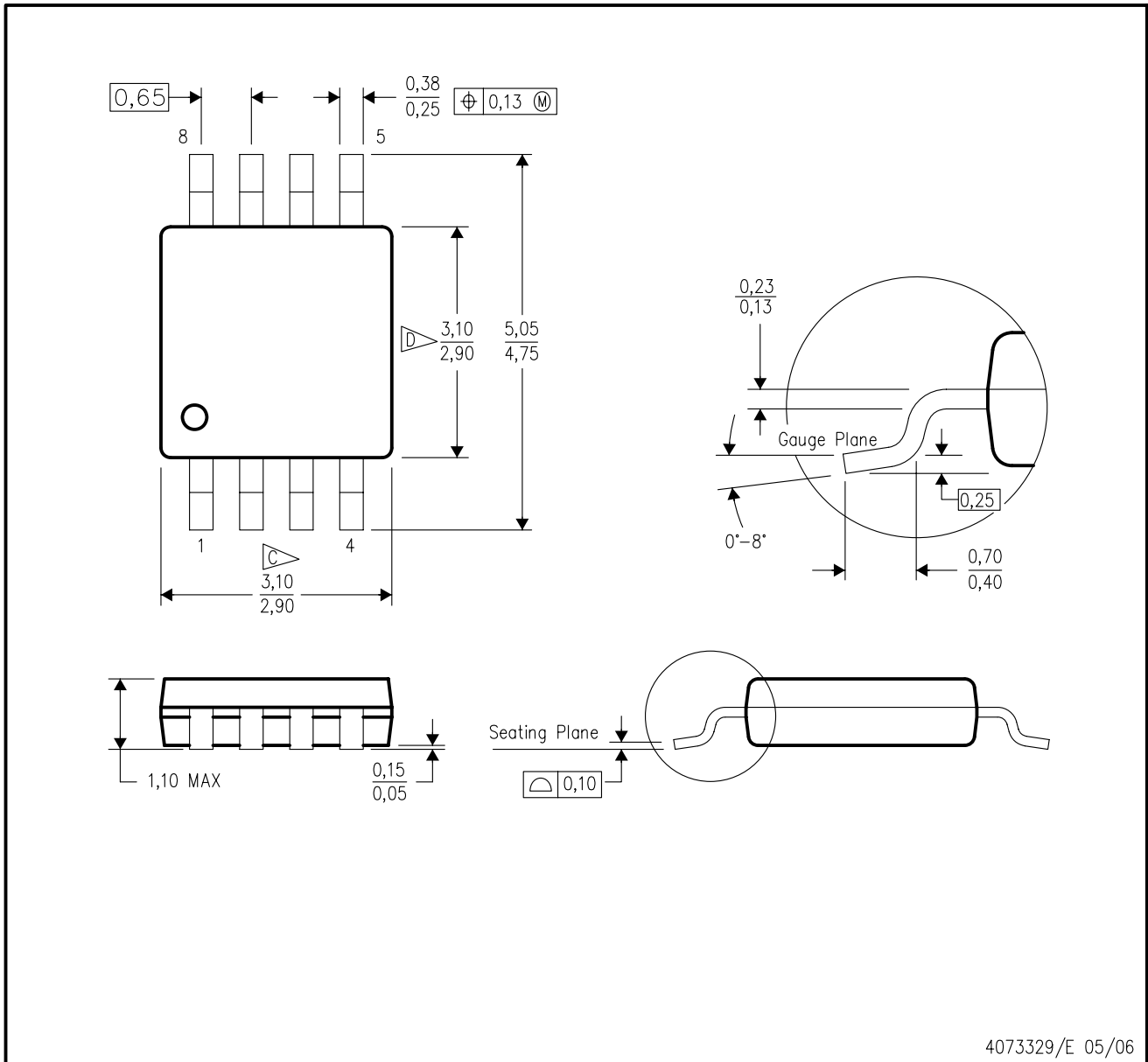
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4073329/E 05/06

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 - B. This drawing is subject to change without notice.
 - C** Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per end.
 - D** Body width does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
 - E. Falls within JEDEC MO-187 variation AA, except interlead flash.



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