UC2875-EP

- Low Startup Current -150 uA
- Outputs Active Low During UVLO
- Soft-Start Control
- Latched Over-Current Comparator With Full Cycle Restart
- Trimmed Reference


NC = No Connect

## description/ordering information

The UC2875 integrated circuit implements control of a bridge power stage by phase-shifting the switching of one half-bridge with respect to the other, allowing constant frequency pulse-width modulation in combination with resonant, zero-voltage switching for high efficiency performance at high frequencies. This circuit may be configured to provide control in either voltage or current mode operation, with a separate over-current shutdown for fast fault protection.

A programmable time delay is provided to insert a dead-time at the turn-on of each output stage. This delay, providing time to allow the resonant switching action, is independently controllable for each output pair (A-B, C-D).

ORDERING INFORMATION

| $T_{A}$ | PACKAGE $\ddagger$ |  | ORDERABLE <br> PART NUMBER | TOP-SIDE <br> MARKING |
| :---: | :--- | :--- | :---: | :---: |
| $-25^{\circ} \mathrm{C}$ to $110^{\circ} \mathrm{C}$ | SOP - DW | Tape and reel | UC2875SDWREP | UC2875SEP |

$\ddagger$ Package drawings, standard packing quantities, thermal data, symbolization, and PCB design guidelines are available at www.ti.com/sc/package.

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

## description/ordering information

With the oscillator capable of operation at frequencies in excess of 2 MHz , overall switching frequencies to 1 MHz are practical. In addition to the standard free running mode, with the CLOCKSYNC pin, the user may configure these devices to accept an external clock synchronization signal, or may lock together up to 5 units with the operational frequency determined by the fastest device.
Protective features include an undervoltage lockout which maintains all outputs in an active-low state until the supply reaches a 10.75 V threshold. 1.5 V hysteresis is built in for reliable, boot-strapped chip supply. Over-current protection is provided, and will latch the outputs in the OFF state within 70 ns of a fault. The current-fault circuitry implements full-cycle restart operation.
Additional features include an error amplifier with band-width in excess of 7 MHz , a 5 V reference, provisions for soft-starting, and flexible ramp generation and slope compensation circuitry.
This device is available in 28 -pin "bat-wing" SOIC plastic package for operation over $-25^{\circ} \mathrm{C}$ to $+110^{\circ} \mathrm{C}$ operation.

## block diagram



Ordering Information


ENHANCED PLASTIC INDICATOR
TAPE and REEL INDICATOR

PACKAGE
DW = Plastic SOIC
TEMPERATURE INDICATOR
$\mathrm{S}=-25^{\circ} \mathrm{C}$ to $110^{\circ} \mathrm{C}$

PRODUCT OPTION

## UC2875-EP

## PHASE SHIFT RESONANT CONTROLLER

SGLS233A - FEBRUARY 2004 - REVISED DECEMBER 2008absolute maximum ratings over operating free-air temperature range (unless otherwise noted) $\dagger \ddagger$
Supply voltage (VC, VIN) ..... 20 V
Output current (sink or source), IO, DC ..... 0.50 A
Pulse ( $0.5 \mu \mathrm{~s}$ ) ..... 3 A
Analog I/O voltage ..... -0.3 V to 5.3 V
Operating jucntion temperature range, $\mathrm{T}_{\mathrm{J}}$ ..... $-55^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Storage temperature range, $T_{\text {stg }}$ ..... $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$
Lead temperature soldering $1,6 \mathrm{~mm}$ ( $1 / 16 \mathrm{inch}$ ) from case for 10 seconds ..... $300^{\circ} \mathrm{C}$
$\dagger$ Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
$\ddagger$ Unless otherwise indicated, voltages are reference to ground and currents are positive into and negative out of the specified terminals.
electrical characteristics, $\mathrm{T}_{\mathrm{A}}=-25^{\circ} \mathrm{C}$ to $110^{\circ} \mathrm{C}, \mathrm{VC}=\mathrm{VIN}=12 \mathrm{~V}$, R $_{\text {FREQSET }}=12 \mathrm{k} \Omega, \mathrm{C}_{\text {FREQSET }}=330 \mathrm{pF}$, $R_{\text {SLOPE }}=12 \mathrm{k} \Omega, \mathrm{C}_{\text {RAMP }}=200 \mathrm{pF}, \mathrm{C}_{\text {DELAYSET }} \mathrm{A}-\mathrm{B}=$ C $_{\text {DELAYSET }}$ C-D $=0.01 \mu \mathrm{~F}$, $I_{\text {DELAYSET A-B }}=I_{\text {DELAYSET C }}$ D $=-500 \mu \mathrm{~A}$, and $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\mathrm{J}}$ (unless otherwise stated)

| PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Undervoltage Lockout |  |  |  |  |  |
| Start threshold |  |  | 10.75 | 11.75 | V |
| UVLO hysteresis |  | 0.5 | 1.25 | 2 | V |
| Supply Current |  |  |  |  |  |
| Supply current, IIN startup | $\mathrm{VIN}=8 \mathrm{~V}, \mathrm{VC}=20 \mathrm{~V}, \mathrm{R}$ SLOPE open, IDELAY $=0$ |  | 150 | 600 | $\mu \mathrm{A}$ |
| Supply current, IC startup | $\mathrm{VIN}=8 \mathrm{~V}, \mathrm{VC}=20 \mathrm{~V}, \mathrm{R}$ SLOPE open, IDELAY $=0$ |  | 10 | 100 | $\mu \mathrm{A}$ |
| Supply current, IIN |  |  | 30 | 44 | mA |
| Supply current, IC |  |  | 15 | 30 | mA |
| Voltage Reference |  |  |  |  |  |
| Output voltage | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ | 4.92 | 5 | 5.08 | V |
| Line regulation voltage | $\mathrm{VIN}=11 \mathrm{~V}$ to 20 V |  | 1 | 10 | mV |
| Load regulation voltage | lVREF $=-10 \mathrm{~mA}$ |  | 5 | 20 | mV |
| Total variation | Line, Load, Temperature | 4.9 |  | 5.1 | V |
| Noise voltage | 10 Hz to 10 kHz |  | 50 |  | $\mu \mathrm{Vrms}$ |
| Long term stability | 1000 hours, $\quad T_{J}=125^{\circ} \mathrm{C}$ |  | 2.5 |  | mV |
| Short circuit current | $\mathrm{VREF}=0 \mathrm{~V}, \quad \mathrm{~T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  | 60 |  | mA |
| Error Amplifier |  |  |  |  |  |
| Offset voltage |  |  | 5 | 15 | mV |
| Input bias current |  |  | 0.6 | 3 | $\mu \mathrm{A}$ |
| Open loop voltage gain (AVOL) | $\mathrm{V}_{\mathrm{E} / \mathrm{AOUT}}=1 \mathrm{~V}$ to 4 V | 60 | 90 |  | dB |
| Common mode rejection ratio (CMRR) | $\mathrm{V}_{\mathrm{CM}}=1.5 \mathrm{~V}$ to 5.5 V | 75 | 95 |  | dB |
| PSRR | $\mathrm{VIN}=11 \mathrm{~V}$ to 20 V | 85 | 100 |  | dB |
| Output sink current | $\mathrm{V}_{\mathrm{E} / \mathrm{AOUT}}=1 \mathrm{~V}$ | 1 | 2.5 |  | mA |
| Output source current | $\mathrm{V}_{\mathrm{E} / \mathrm{AOUT}}=4 \mathrm{~V}$ |  | -1.3 | -0.5 | mA |
| High-level output voltage ( $\mathrm{V}_{\mathrm{OH}}$ ) | $\mathrm{I}_{\mathrm{E} / \text { AOUT }}=-0.5 \mathrm{~mA}$ | 4 | 4.7 | 5 | V |
| Low-level output voltage ( $\mathrm{V}_{\mathrm{OL}}$ ) | $\mathrm{I}_{\mathrm{E} / \text { AOUT }}=1 \mathrm{~mA}$ | 0 | 0.5 | 1 | V |
| Unity gain bandwidth |  | 7 | 11 |  | MHz |
| Slew rate |  | 6 | 11 |  | V/ $/$ sec |

electrical characteristics, $\mathrm{T}_{\mathrm{A}}=-25^{\circ} \mathrm{C}$ to $110^{\circ} \mathrm{C}, \mathrm{VC}=\mathrm{VIN}=12 \mathrm{~V}$, R $_{\text {FREQSET }}=12 \mathrm{k} \Omega, \mathrm{C}_{\text {FREQSET }}=330 \mathrm{pF}$, $R_{\text {SLOPE }}=12 \mathrm{k} \Omega, \mathrm{C}_{\text {RAMP }}=200 \mathrm{pF}, \mathrm{C}_{\text {DELAYSET }} \mathrm{A}-\mathrm{B}=$ C DELAYSET C-D $=0.01 \mu \mathrm{~F}$, $I_{\text {DELAYSET A-B }}=I_{\text {DELAYSET }} C-D=-500 \mu \mathrm{~A}$, and $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\mathrm{J}}$ (unless otherwise stated)

| PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PWM Comparator |  |  |  |  |  |
| Ramp offset voltage | $\mathrm{T}_{J}=25^{\circ} \mathrm{C}, \quad$ See Note 3 |  | 1.3 |  | V |
| Zero phase shift voltage | See Note 4 | 0.55 | 0.9 |  | V |
| PWM phase shift (See Note 1) | $\mathrm{V}_{\text {E/AOUT }}>$ (Ramp Peak + Ramp Offset) | 98 | 99.5 | 102 | \% |
|  | $\mathrm{V}_{\text {E/AOUT }}$ < Zero Phase Shift Voltage | 0 | 0.5 | 2 |  |
| Output Skew (See Note 1) | $\mathrm{V}_{\text {E/AOUT }}<1 \mathrm{~V}$ |  | 5 | $\pm 20$ | ns |
| Ramp to output delay | See Note 6 |  | 65 | 125 | ns |
| Oscillator |  |  |  |  |  |
| Initial accuracy | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ | 0.85 | 1 | 1.15 | MHz |
| Voltage stability | $\mathrm{VIN}=11 \mathrm{~V}$ to 20 V |  | 0.2 | 2 | \% |
| Total variation | Line, Temperature | 0.80 |  | 1.20 | MHz |
| Sync pin threshold | T J $=25^{\circ} \mathrm{C}$ |  | 3.8 |  | V |
| Clock out peak | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  | 4.3 |  | V |
| Clock out low | T J $=25^{\circ} \mathrm{C}$ |  | 3.3 |  | V |
| Clock out pulse width | RCLOCKSYNC $=3.9 \mathrm{k} \Omega$ |  | 30 | 100 | ns |
| Maximum frequency | RFREQSET $=5 \mathrm{k} \Omega$ | 2 |  |  | MHz |
| Ramp Generator/Slope Compensation |  |  |  |  |  |
| Minimum ramp current | ISLOPE $=10 \mu \mathrm{~A}, \quad \mathrm{~V}_{\text {FREQSET }}=$ VREF |  | -11 | -14 | $\mu \mathrm{A}$ |
| Maximum ramp current | ISLOPE $=1 \mathrm{~mA}, \quad \mathrm{~V}_{\text {FREQSET }}=\mathrm{VREF}$ | -0.8 | -0.95 |  | mA |
| Ramp valley |  |  | 0 |  | V |
| Ramp peak - clamping level | RFREQSET $=100 \mathrm{k} \Omega$ |  | 3.8 | 4.1 | V |
| Current Limit |  |  |  |  |  |
| Input bias current | $\mathrm{V}_{\text {CS }}+=3 \mathrm{~V}$ |  | 2 | 5 | $\mu \mathrm{A}$ |
| Threshold voltage |  | 2.4 | 2.5 | 2.6 | V |
| Delay to output |  |  | 85 | 150 | ns |
| Soft-Start/Reset Delay |  |  |  |  |  |
| Charge current | $\mathrm{V}_{\text {SOFTSTART }}=0.5 \mathrm{~V}$ | -20 | -9 | -3 | $\mu \mathrm{A}$ |
| Discharge current | $\mathrm{V}_{\text {SOFTSTART }}=1 \mathrm{~V}$ | 120 | 230 |  | $\mu \mathrm{A}$ |
| Restart threshold |  | 4.3 | 4.7 |  | V |
| Discharge level |  |  | 300 |  | mV |

electrical characteristics, $\mathrm{T}_{\mathrm{A}}=-25^{\circ} \mathrm{C}$ to $110^{\circ} \mathrm{C}, \mathrm{VC}=\mathrm{VIN}=12 \mathrm{~V}$, R $_{\text {FREQSET }}=12 \mathrm{k} \Omega, \mathrm{C}_{\text {FREQSET }}=330 \mathrm{pF}$, $R_{\text {SLOPE }}=12 \mathrm{k} \Omega, \mathrm{C}_{\text {RAMP }}=200 \mathrm{pF}, \mathrm{C}_{\text {DELAYSET }} \mathrm{A}-\mathrm{B}=$ C $_{\text {DELAYSET }} \mathrm{C}-\mathrm{D}=0.01 \mu \mathrm{~F}$,
$I_{\text {DELAYSET A-B }}=I_{\text {DELAYSET C-D }}=-500 \mu \mathrm{~A}$, and $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\mathrm{J}}$ (unless otherwise stated)

| PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Output Drivers |  |  |  |  |  |
| Output low level | IOUT $=50 \mathrm{~mA}$ |  | 0.2 | 0.4 | V |
|  | IOUT $=500 \mathrm{~mA}$ |  | 1.2 | 2.6 |  |
| Output high level | IOUT $=-50 \mathrm{~mA}$ |  | 1.5 | 2.5 | V |
|  | IOUT $=-500 \mathrm{~mA}$ |  | 1.7 | 2.6 |  |
| Delay Set |  |  |  |  |  |
| Delay set voltage | IDELAY $=-500 \mu \mathrm{~A}$ | 2.3 | 2.4 | 2.6 | V |
| Delay time | ${ }^{\text {I DELAY }}=-250 \mu$ A, See Notes 2 and 5 | 150 | 250 | 600 | ns |

NOTES: 1. Phase shift percentage $\left(0 \%=0^{\circ}, 100 \%=180^{\circ}\right)$ is defined as $\theta=200 / T \Phi \%$, where $\theta$ is the phase shift, and $\Phi$ and $T$ are defined in Figure 1. At $0 \%$ phase shift, $\Phi$ is the output skew.
2. Delay time is defined as delay $=T$ ( $1 / 2$-(duty cycle)), where $T$ is defined in Figure 1.
3. Ramp offset voltage has a temperature coefficient of about $4.0 \mathrm{mV} /{ }^{\circ} \mathrm{C}$.
4. Zero phase shift voltage has a temperature coefficient of about $2.0 \mathrm{mV} /{ }^{\circ} \mathrm{C}$.
5. Delay time can be programmed via resistors from the delay set pins to ground. Delay time $\approx\left(62.5 \times 10^{-12}\right) /$ IDELAY sec where IDELAY = Delay set voltage / RDELAY. The recommended range for IDELAY is $25 \mu \mathrm{~A} \leq \operatorname{IDELAY} \leq 1 \mathrm{~mA}$
6. Ramp delay to output time is defined in NO TAG.

OUTA
OUTB

OUTC
OUTD


Duty Cycle $=t / T \quad$ Period $=T$
$T_{D H L}(A$ to $C)=T_{D H L}(B$ to $D)=\phi$
Phase Shift, Output Skew, and Delay Time Definitions

Figure 1. Phase Shift and Output Skew


Figure 2. Delay Time

# UC2875-EP <br> PHASE SHIFT RESONANT CONTROLLER 

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## APPLICATION AND OPERATION INFORMATION

## Pin Descriptions

CLOCKSYNC (bi-directional clock and synchronization pin): Used as an output, this pin provides a clock signal. As an input, this pin provides a synchronization point. In its simplest usage, multiple devices, each with their own local oscillator frequency, may be connected together by the CLOCKSYNC pin and will synchronize on the fastest oscillator. This pin may also be used to synchronize the device to an external clock, provided the external signal is of higher frequency than the local oscillator. A resistor load may be needed on this pin to minimize the clock pulse width.
E/AOUT (error amplifier output): This is is the gain stage for overall feedback control. Error amplifier output voltage levels below 1 volt will force $0^{\circ}$ phase shift. Since the error amplifier has a relatively low current drive capability, the output may be overridden by driving with a sufficiently low impedance source.

CS+ (current sense):The non-inverting input to the current- fault comparator whose reference is set internally to a fixed 2.5 V (separate from VREF). When the voltage at this pin exceeds 2.5 V the current-fault latch is set, the outputs are forced OFF and a SOFT-START cycle is initiated. If a constant voltage above 2.5 V is applied to this pin the outputs are disabled from switching and held in a low state until the CS+ pin is brought below 2.5 V . The outputs may begin switching at 0 degrees phase shift before the SOFTSTART pin begins to rise - - this condition will not prematurely deliver power to the load.
FREQSET (oscillator frequency set pin): A resistor and a capacitor from FREQSET to GND will set the oscillator frequency.

DELAYSET A-B, DELAYSET C-D (output delay control): The user programmed current flowing from these pins to GND set the turn-on delay for the corresponding output pair. This delay is introduced between turn-off of one switch and turn-on of another in the same leg of the bridge to provide a dead time in which the resonant switching of the external power switches takes place. Separate delays are provided for the two half-bridges to accommodate differences in the resonant capacitor charging currents.

EA- (error amplifier inverting input): This is normally connected to the voltage divider resistors which sense the power supply output voltage level.
EA+ (error amplifier non-inverting input): This is normally connected to a reference voltage used for comparison with the sensed power supply output voltage level at the EA+ pin.
GND (signal ground):All voltages are measured with respect to GND. The timing capacitor, on the FREQSET pin, any bypass capacitor on the VREF pin, bypass capacitors on $\mathrm{V}_{\mathbb{I N}}$ and the ramp capacitor, on the RAMP pin, should be connected directly to the ground plane near the signal ground pin.

OUTA-OUTD (outputs A-D): The outputs are 2 A totem- pole drivers optimized for both MOSFET gates and level-shifting transformers. The outputs operate as pairs with a nominal $50 \%$ duty-cycle. The A-B pair is intended to drive one half-bridge in the external power stage and is syncronized with the clock waveform. The C-D pair will drive the other half-bridge with switching phase shifted with respect to the A-B outputs.

PWRGND (power ground):VC should be bypassed with a ceramic capacitor from the VC pin to the section of the ground plane that is connected to PWRGND. Any required bulk reservoir capacitor should parallel this one. Power ground and signal ground may be joined at a single point to optimize noise rejection and minimize DC drops.
RAMP (voltage ramp):This pin is the input to the PWM comparator. Connect a capacitor from here to GND. A voltage ramp is developed at this pin with a slope:

$$
\frac{d V}{d T}=\frac{\text { SenseVoltage }}{R_{\text {SLOPE }} \times C_{\text {RAMP }}}
$$

Current mode control may be achieved with a minimum amount of external circuitry, in which case this pin provides slope compensation.

## APPLICATION AND OPERATION INFORMATION

Because of the 1.3 V offset between the ramp input and the PWM comparator, the error amplifier output voltage can not exceed the effective ramp peak voltage and duty cycle clamping is easily achievable with appropriate values of RSLOPE and CRAMP.
SLOPE (set ramp slope/slope compensation): A resistor from this pin to $\mathrm{V}_{C C}$ will set the current used to generate the ramp. Connecting this resistor to the DC input line voltage will provide voltage feed-forward.
SOFTSTART (soft start): SOFTSTART will remain at GND as long as VIN is below the UVLO threshold. SOFTSTART will be pulled up to about 4.8 V by an internal $9 \mu \mathrm{~A}$ current source when VIN becomes valid (assuming a non-fault condition). In the event of a current-fault (CS+ voltage exceeding 2.5 V ), SOFTSTART will be pulled to GND and them ramp to 4.8 V . If a fault occurs during the SOFTSTART cycle, the outputs will be immediately disabled and SOFTSTART must charge fully prior to resetting the fault latch.
For paralleled controllers, the SOFTSTART pins may be paralled to a single capacitor, but the charge currents will be additive.

VC (output switch supply voltage): This pin supplies power to the output drivers and their associated bias circuitry. Connect VC to a stable source above 3 V for normal operation, above 12 V for best performance. This supply should be bypassed directly to the PWRGND pin with low ESR, low ESL capacitors.
VIN (primary chip supply voltage): This pin supplies power to the logic and analog circuitry on the integrated circuit that is not directly associated with driving the output stages. Connect VIN to a stable source above 12 V for normal operation. To ensure proper chip functionality, these devices will be inactive until VIN exceeds the upper undervoltage lockout threshold. This pin should by bypassed directly to the GND pin with low ESR, low ESL capacitors.

NOTE: When VIN exceeds the UVLO threshold the supply current $\left(l_{\mathbb{N}}\right)$ will jump from about $100 \mu \mathrm{~A}$ to a current in excess of $20 \mu \mathrm{~A}$. If the UC2875 is not connected to a well bypassed supply, it may immediately enter UVLO again.
VREF: This pin is an accurate 5 V voltage reference. This output is capable of delivering about 60 mA to peripheral circuitry and is internally short circuit current limited. VREF is disabled while VIN is low enough to force the chip into UVLO. The circuit is also in UVLO until VREF reaches approximately 4.75 V . For best results bypass VREF with a $0.1 \mu \mathrm{~F}$, low ESR, low ESL, capacitor to the GND pin.


Figure 3. Undervoltage Lockout
When power is applied to the circuit and VIN is below the upper UVLO threshold, $\mathrm{I}_{\mathrm{IN}}$ will be below $600 \mu \mathrm{~A}$, the reference generator will be off, the fault latch is reset, the soft-start pin is discharged, and the outputs are actively held low. When VIN exceeds the upper UVLO threshold, the reference generator turns on. All else remains in the shut-down mode until the output of the reference, VREF, exceeds 4.75 V .

## APPLICATION AND OPERATION INFORMATION





Figure 4. Oscillator Schematic, Frequency vs Resistance Graph, and Timing Diagram
The high frequency oscillator may be either free-running or externally synchronized. For free-running operation, the frequency is set via an external resistor and capacitor to ground from the FREQSET pin.

The CLOCKSYNC pin of the oscillator may be used to synchronize multiple UC2875 devices simply by connecting the CLOCKSYNC of each UC2875 to the others as in Figure 5.


FREQSET
IC1
CL




Figure 5. Synchronizing Multiple UC2875-EP Devices
All ICs will sync to chip with the fastest local oscillator.
R1 \& RN may be needed to keep sync pulse narrow due to capacitance on line.
R1 \& RN may also be needed to properly terminate RSYNC line.

## APPLICATION AND OPERATION INFORMATION

## Syncing to External TTL/CMOS



Figure 6. Snychronizing to an External TTL/CMOS Clock Signal
ICs will sync to fastest chip or TTL clock if it is higher frequency.
$R$ and RN may be needed for same reasons as above.
Although each UC2875 has a local oscillator frequency, the group of devices will synchronize to the fastest oscillator driving the CLOCKSYNC pin. This arrangement allows the synchronizing connection between ICs to be broken without any local loss of functionality.

Synchronizing the device to an external clock signal may be accomplished with a minimum of external circuitry, as shown in Figure 6.

Capacitive loading on the CLOCKSYNC pin will increase the clock pulse width, and may adversely effect system performance. Therefore, a resistor to ground from the CLOCKSYNC pin is optional, but may be required to offset capacitive loading on this pin. These resistors are shown in the oscillator schematics as R1, RN.

## Delay Blocks and Output Stages

In each of the output stages, transistors Q3 through Q6 form a high-speed totem-pole driver which will source or sink more than one amp peak with a total delay of approximately 30 nanoseconds. To ensure a low output level prior to turn-on, transistors Q7 through Q9 form a self-biased driver to hold Q6 on prior to the supply reaching its turn-on threshold. This circuit is operable when the chip supply is zero. Q6 is also turned on and held low with a signal from the fault logic portion of the chip.


Figure 7. Delay Blocks and Output Stages
The delay providing the dead-time is accomplished with C 1 which must discharge to $\mathrm{V}_{\mathrm{TH}}$ before the output can go high. The time is defined by the current sources, I1, which is programmed by an external resistor, RTD . The voltage on the Delay Set pins is internally regulated to 2.5 V and the range of dead time control is from 50 to 200 nanoseconds. NOTE: There is no way to disable the delay circuitry, and the delay time must be programmed.

## Output Switch Orientation

The four outputs of the UC2875 interface to the full bridge converter switches as shown in Figure 8.


Figure 8. Output Switch Orientation

## APPLICATION AND OPERATION INFORMATION

## Fault/Soft-Start

The fault control circuitry provides two forms of power shutdown:

- Complete turn-off of all four output power stages.
- Clamping the phase shift command to zero.

Complete turn-off is ordered for an over-current fault or a low supply voltage. When the SOFTSTART pin reaches its low threshold, switching is allowed to proceed while the phase-shift is advanced from zero to its nominal value with the time constant of the SOFT-START capacitor.

The fault logic insures that a continuous fault will institute a low frequency "hiccup" retry cycle by forcing the SOFT-START capacitor to charge through its full cycle between each restart attempt.


Figure 9. Fault/Soft-Start

## APPLICATION AND OPERATION INFORMATION

## Slope/Ramp Pins

The ramp generator may be configured for the following control methods:

- Voltage Mode
- Voltage Feedforward
- Current Mode
- Current Mode with Slope Compensation

Figure 10 shows a voltage-mode configuration. With RSLOPE tied to a stable voltage source, the waveform on $\mathrm{C}_{\text {RAMP }}$ will be a constant-slope ramp, providing conventional voltage-mode control. If $\mathrm{R}_{\text {SLOPE }}$ is connected to the power supply input voltage, a variable-slope ramp will provide voltage feedforward.


Figure 10. Slope/Ramp Pins

1. Simple voltage mode operation achieved by placing RSLOPE between VIN and SLOPE.
2. Voltage Feedforward achieved by placing RSLOPE between supply voltage and SLOPE pin of UC2875.

RAMP

$$
\frac{d V}{d T} \approx \frac{V_{\text {Rslope }}}{R_{\text {SLOPE }} \times C_{\text {RAMP }}}
$$

For current-mode control the ramp generator may be disabled by grounding the slope pin and using the ramp pin as a direct current sense input to the PWM comparator.

## PACKAGING INFORMATION

| Orderable Device | Status <br> (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan <br> (2) | Lead finish/ Ball material <br> (6) | MSL Peak Temp <br> (3) | Op Temp ( ${ }^{\circ} \mathrm{C}$ ) | Device Marking <br> (4/5) | Samples |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| UC2875SDWREP | ACTIVE | SOIC | DW | 28 | 1000 | RoHS \& Green | NIPDAU | Level-2-260C-1 YEAR | -25 to 110 | UC2875SEP | Samples |
| V62/04752-01XE | ACTIVE | SOIC | DW | 28 | 1000 | RoHS \& Green | NIPDAU | Level-2-260C-1 YEAR | -25 to 110 | UC2875SEP | Samples |

${ }^{(1)}$ The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.
${ }^{(2)}$ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed $0.1 \%$ by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as " Pb -Free".
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the $<=1000 \mathrm{ppm}$ threshold requirement.
${ }^{(3)}$ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
${ }^{(4)}$ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device
${ }^{(5)}$ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a " $\sim$ " will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
${ }^{(6)}$ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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OTHER QUALIFIED VERSIONS OF UC2875-EP :

- Catalog: UC2875

NOTE: Qualified Version Definitions:

- Catalog - Tl's standard catalog product


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