

SLOS537B - MAY 2008 - REVISED JANUARY 2014

15-W STEREO CLASS-D AUDIO POWER AMPLIFIER

Check for Samples: TPA3121D2

FEATURES

- 10-W/Ch Stereo Into an 8-Ω Load From a 24-V Supply
- 15-W/Ch Stereo Into a 4-Ω Load from a 22-V Supply
- 30-W/Ch Mono Into an 8-Ω Load from a 22-V Supply
- Operates From 10 V to 26 V
- Can Run From +24 V LCD Backlight Supply
- Efficient Class-D Operation Eliminates Need for Heat Sinks
- Four Selectable, Fixed-Gain Settings
- Internal Oscillator to Set Class D Frequency (No External Components Required)
- Single-Ended Analog Inputs
- Thermal and Short-Circuit Protection With Auto Recovery
- Space-Saving Surface Mount 24-Pin TSSOP Package
- Advanced Power-Off Pop Reduction

APPLICATIONS

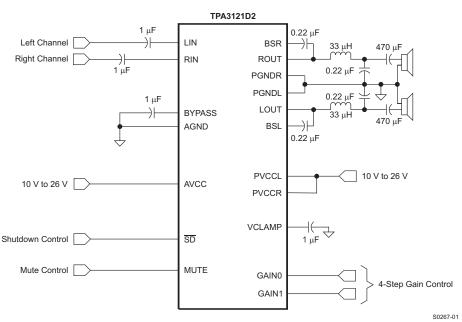
- Flat Panel Display TVs
- DLP® TVs
- CRT TVs
- Powered Speakers

DESCRIPTION

The TPA3121D2 is a 15-W (per channel), efficient, class-D audio power amplifier for driving stereo speakers in a single-ended configuration or a mono speaker in a bridge-tied-load configuration. The TPA3121D2 can drive stereo speakers as low as 4 Ω . The efficiency of the TPA3121D2 eliminates the need for an external heat sink when playing music.

The gain of the amplifier is controlled by two gain select pins. The gain selections are 20, 26, 32, and 36 dB.

The patented start-up and shutdown sequences minimize pop noise in the speakers without additional circuitry.



SIMPLIFIED APPLICATION CIRCUIT

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet. DLP is a registered trademark of Texas Instruments.

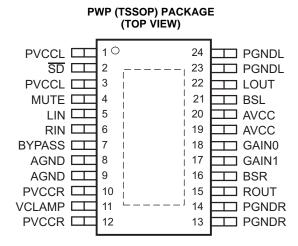
System Two, Audio Precision are trademarks of Audio Precision, Inc.



SLOS537B-MAY 2008-REVISED JANUARY 2014

www.ti.com

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.





TERMINAL			
NAME	24-PIN (PWP)	I/O/P	DESCRIPTION
SD	2	I	Shutdown signal for IC (low = disabled, high = operational). TTL logic levels with compliance to AVCC
RIN	6	I	Audio input for right channel
LIN	5	I	Audio input for left channel
GAIN0	18	I	Gain select least-significant bit. TTL logic levels with compliance to AVCC
GAIN1	17	I	Gain select most-significant bit. TTL logic levels with compliance to AVCC
MUTE	4	I	Mute signal for quick disable/enable of outputs (high = outputs switch at 50% duty cycle, low = outputs enabled). TTL logic levels with compliance to AVCC
BSL	21	I/O	Bootstrap I/O for left channel
PVCCL	1, 3	Р	Power supply for left-channel H-bridge, not internally connected to PVCCR or AVCC
LOUT	22	0	Class-D ½-H-bridge positive output for left channel
PGNDL	23, 24	Р	Power ground for left-channel H-bridge
VCLAMP	11	Р	Internally generated voltage supply for bootstrap capacitors
BSR	16	I/O	Bootstrap I/O for right channel
ROUT	15	0	Class-D 1/2-H-bridge negative output for right channel
PGNDR	13, 14	Р	Power ground for right-channel H-bridge.
PVCCR	10, 12	Р	Power supply for right-channel H-bridge, not connected to PVCCL or AVCC
AGND	9	Р	Analog ground for digital/analog cells in core
AGND	8	Р	Analog ground for analog cells in core
BYPASS	7	ο	Reference for preamplifier inputs. Nominally equal to AVCC/8. Also controls start-up time via external capacitor sizing.
AVCC	19, 20	Р	High-voltage analog power supply. Not internally connected to PVCCR or PVCCL
Thermal pad	Die pad	Р	Connect to ground. Thermal pad should be soldered down on all applications to secure the device properly to the printed wiring board.



www.ti.com

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted) ⁽¹⁾

			VALUE	UNIT
V _{CC}	Supply voltage	AVCC, PVCC	-0.3 to 30	V
VI	Logic input voltage	SD, MUTE, GAIN0, GAIN1	-0.3 to V _{CC} + 0.3	V
V _{IN}	Analog input voltage	RIN, LIN	–0.3 to 7	V
	Continuous total power dissipation		See the Thermal Inforamtion T	able
T _A	Operating free-air temperature range		-40 to 85	°C
TJ	Operating junction temperature range		-40 to 150	°C
T _{stg}	Storage temperature range		-65 to 150	°C
		SE Output Configuration	3.2	0
R _L	Load resistance (minimum value)	BTL Output Configuration	6.4	Ω
		Human body model (all pins)	±2	kV
ESD	Electrostatic Discharge	Charged-device model (all pins)	±500	V

(1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

THERMAL INFORMATION

		TPA3121D2	
	THERMAL METRIC ⁽¹⁾⁽²⁾	PWP	UNITS
		24 PINS	
θ_{JA}	Junction-to-ambient thermal resistance	30.9	
θ _{JCtop}	Junction-to-case (top) thermal resistance	29.6	
θ _{JB}	Junction-to-board thermal resistance	9.0	80 AM
Ψιτ	Junction-to-top characterization parameter	0.5	°C/W
Ψјв	Junction-to-board characterization parameter	3.6	
θ _{JCbot}	Junction-to-case (bottom) thermal resistance	0.7	

For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, SPRA953.
 For thermal estimates of this device based on PCB copper area, see the TI PCB Thermal Calculator.

RECOMMENDED OPERATING CONDITIONS

			MIN	MAX	UNIT
V _{CC}	Supply voltage	PVCC, AVCC	10	26	V
VIH	High-level input voltage	SD, MUTE, GAIN0, GAIN1	2		V
VIL	Low-level input voltage	SD, MUTE, GAIN0, GAIN1		0.8	V
		\overline{SD} , V _I = V _{CC} , V _{CC} = 30 V		125	
I _{IH}	High-level input current	MUTE, $V_I = V_{CC}$, $V_{CC} = 30$ V		125	μA
		GAIN0, GAIN1, $V_I = V_{CC}$, $V_{CC} = 24$ V		125	
		\overline{SD} , V _I = 0, V _{CC} = 30 V		1	
I _{IL}	Low-level input current	MUTE, $V_I = 0 V$, $V_{CC} = 30 V$		1	μA
		GAIN0, GAIN1, $V_I = 0 V$, $V_{CC} = 24 V$		1	
T _A	Operating free-air temperature		-40	85	°C



www.ti.com

DC CHARACTERISTICS

 $T_A = 25^{\circ}C$, $V_{CC} = 24$ V, $R_L = 8\Omega$ (unless otherwise noted)

PARAMETER		TEST CON	IDITIONS	MIN	TYP	MAX	UNIT
V _{os}	Class-D output offset voltage (measured differentially in BTL mode as shown in Figure 36)	$V_1 = 0 V, A_V = 36 dB$			7.5	50	mV
V _(BYPASS)	Bypass output voltage	No load			AVCC/8		V
I _{CC(q)}	Quiescent supply current	$\overline{SD} = 2 V, MUTE = 0 V$	/, no load		16	30	mA
I _{CC(q)}	Quiescent supply current in mute mode	MUTE = 0.8 V, no load			16		mA
I _{CC(q)}	Quiescent supply current in shutdown mode	SD = 0.8 V, no load			0.39	1	mA
r _{DS(on)}	Drain-source on-state resistance				210	450	mΩ
			GAIN0 = 0.8 V	18	20	22	
0		GAIN1 = 0.8 V	GAIN0 = 2 V	24	26	28	
G	Gain		GAIN0 = 0.8 V	30	32	34	dB
		GAIN = 2 V GAIN0 = 2 V		34	36	38	
	Mute attenuation	V _I = 1 Vrms			-75		dB

AC CHARACTERISTICS

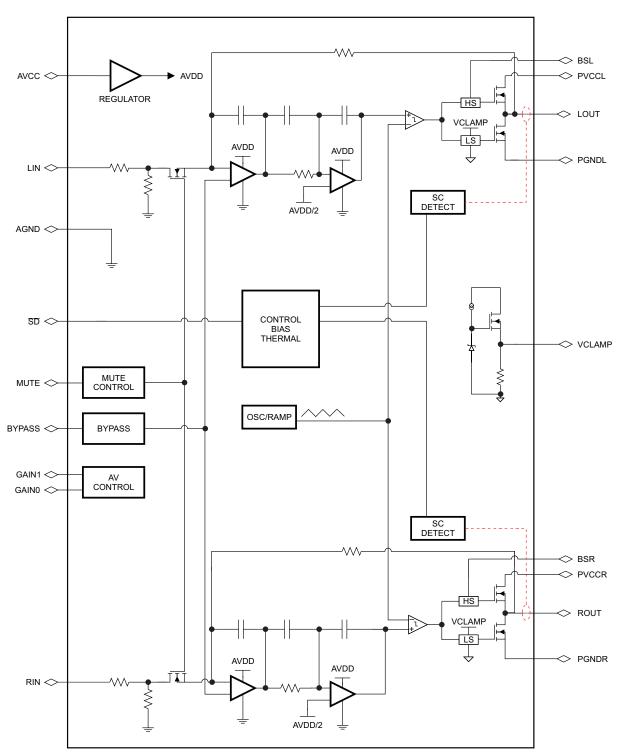
 $T_A = 25^{\circ}C$, $V_{CC} = 24$ V, $R_L = 8\Omega$ (unless otherwise noted)

	PARAMETER	TEST CONDITIONS		MIN	TYP	MAX	UNIT
	Cumulu visula vaisatian	V_{CC} = 24, V_{ripple} = 200 m V_{PP}	100 Hz		-48		-10
ksvr	Supply ripple rejection	Gain = 20 dB	1 kHz		-52		dB
Po	Output power at 1% THD+N	ver at 1% THD+N V _{CC} = 24 V, f = 1 kHz			8		W
	Output power at 10% THD+N			10		vv	
THD+N	Total harmonic distortion + noise	f = 1 kHz, P _O = 5 W			0.04%		
M	Output integrated poins floor	20 Hz to 22 kHz, A-weighted filter,			125		μV
Vn	Output integrated noise floor	Gain = 20 dB			-78		dBV
	Crosstalk	P _O = 1 W, f = 1 kHz; gain = 20	dB		-70		dB
SNR	Signal-to-noise ratio	Max output at THD+N < 1%, f = 1 kHz, gain = 20 dB			92		dB
	Thermal trip point				150		°C
	Thermal hysteresis				30		°C
f _{osc}	Oscillator frequency			250	300	350	kHz
∆t mute	Mute delay	Time from mute input switches high until outputs muted			120		msec
∆t unmute	Unmute delay	Time from mute input switches low until outputs unmuted			120		msec



www.ti.com

FUNCTIONAL BLOCK DIAGRAM



TOTAL HARMONIC DISTORTION + NOISE TOTAL HARMONIC DISTORTION + NOISE vs FREQUENCY vs FREQUENCY 10 10 $V_{CC} = 12 V$ V_{CC} = 18 V THD+N – Total Harmonic Distortion + Noise – % % $R_L = 6 \Omega (SE)$ $R_{I} = 4 \Omega (SE)$ THD+N – Total Harmonic Distortion + Noise – Gain = 20 dBGain = 20 dB 1 1 $P_{O} = 2.5 \text{ W}$ $P_{O} = 2.5 W$ $P_0 = 1 W$ $P_0 = 1 W$ 0.1 0.1 0.01 0.01 $P_{O} = 0.5 W$ Ħ $P_{O} = 0.5 W$ 0.001 0.001 20 100 1k 10k 20k 20 100 1k 10k 20k f - Frequency - Hz f - Frequency - Hz G001 G002 Figure 1. Figure 2. TOTAL HARMONIC DISTORTION + NOISE **TOTAL HARMONIC DISTORTION + NOISE** vs FREQUENCY vs FREQUENCY 10 10 V_{CC} = 18 V $V_{CC} = 24 V$ THD+N – Total Harmonic Distortion + Noise – % THD+N – Total Harmonic Distortion + Noise – % $R_I = 8 \Omega (SE)$ $R_I = 8 \Omega (SE)$ Gain = 20 dB Gain = 20 dB 1 1 $P_0 = 5 W$ $P_{O} = 2.5 \text{ W}$ P_O = 2.5 W 0.1 0.1 0.01 0.01 $P_0 = 1 W$ $P_O = 1 W$ 0.001 0.001 10k 20k 20 100 1k 10k 20k 20 100 1k f - Frequency - Hz f - Frequency - Hz G003 G004

TYPICAL CHARACTERISTICS

All tests are made at frequency = 1 kHz unless otherwise noted.

Figure 3.

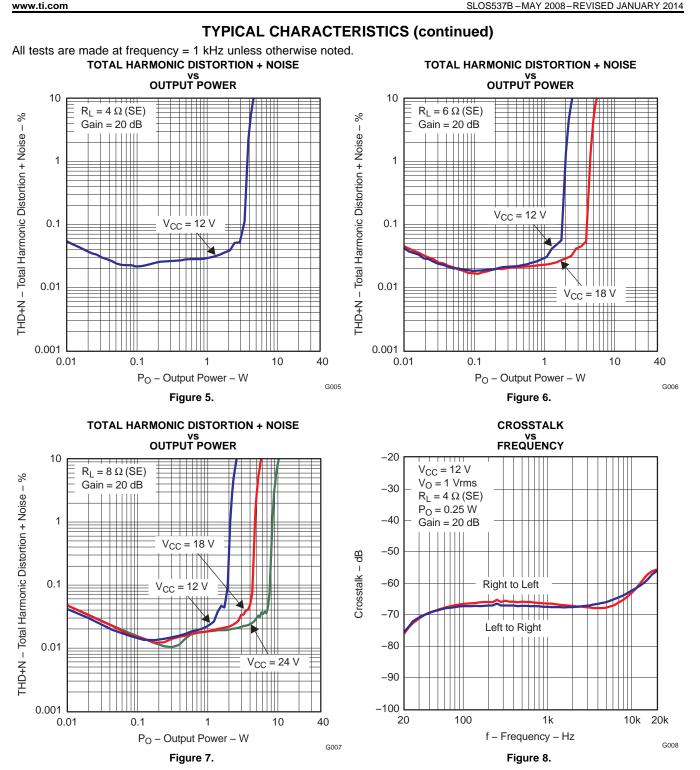
Figure 4.

Texas

INSTRUMENTS

www.ti.com

SLOS537B-MAY 2008-REVISED JANUARY 2014



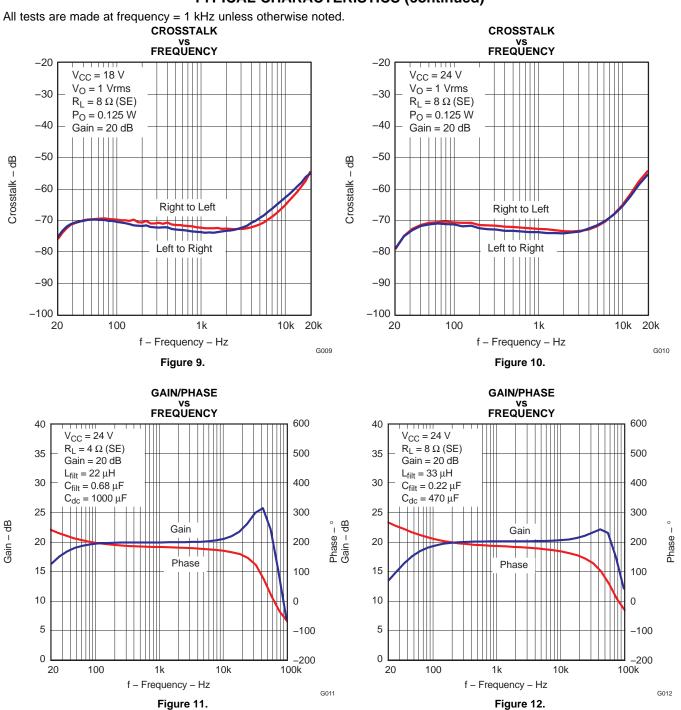
EXAS

NSTRUMENTS

Texas INSTRUMENTS

www.ti.com

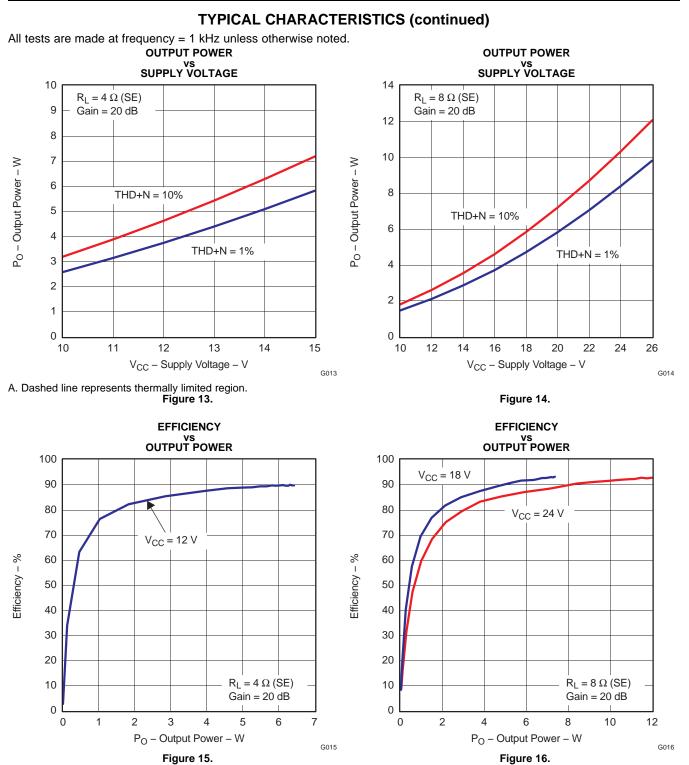
SLOS537B-MAY 2008-REVISED JANUARY 2014











SLOS537B – MAY 2008 – REVISED JANUARY 2014

All tests are made at frequency = 1 kHz unless otherwise noted. SUPPLY CURRENT SUPPLY CURRENT VS OUTPUT POWER VS OUTPUT POWER 1.5 1.2 $R_L = 4 \Omega$ (SE) $R_L = 8 \Omega (SE)$ Gain = 20 dB Gain = 20 dB 1.0 1.2 Icc – Supply Current – A Icc - Supply Current - A 0.8 0.9 $V_{CC} = 12 V$ 0.6 0.6 V_{CC} = 24 V 0.4 0.3 V_{CC} = 18 V 0.2 0.0 0.0 3 5 6 9 12 10 15 20 25 0 15 0 Po - Output Power - W P_O – Output Power – W G017 G018 Figure 17. Figure 18. Α. Dashed line represents thermally limited region. POWER SUPPLY REJECTION RATIO POWER SUPPLY REJECTION RATIO vs FREQUENCY FREQUENCY 0 0 $V_{CC} = 24 V$ $V_{CC} = 24 V$ $V_{O(ripple)} = 0.2 V_{PP}$ R_L = 8 Ω (SE) -10 V_{O(ripple)} = 0.2 V_{PP} -10 $R_L = 4 \Omega (SE)$ -20 -20 Power Supply Rejection Ratio - dB Gain = 20 dB Power Supply Rejection Ratio - dB Gain = 20 dB -30 -30 -40 -40 -50 -50 -60 -60 -70 -70 -80 -80 -90 -90 -100 -100 20 100 1k 10k 20k 20 100 1k 10k 20k f - Frequency - Hz f - Frequency - Hz G019 G025

TYPICAL CHARACTERISTICS (continued)

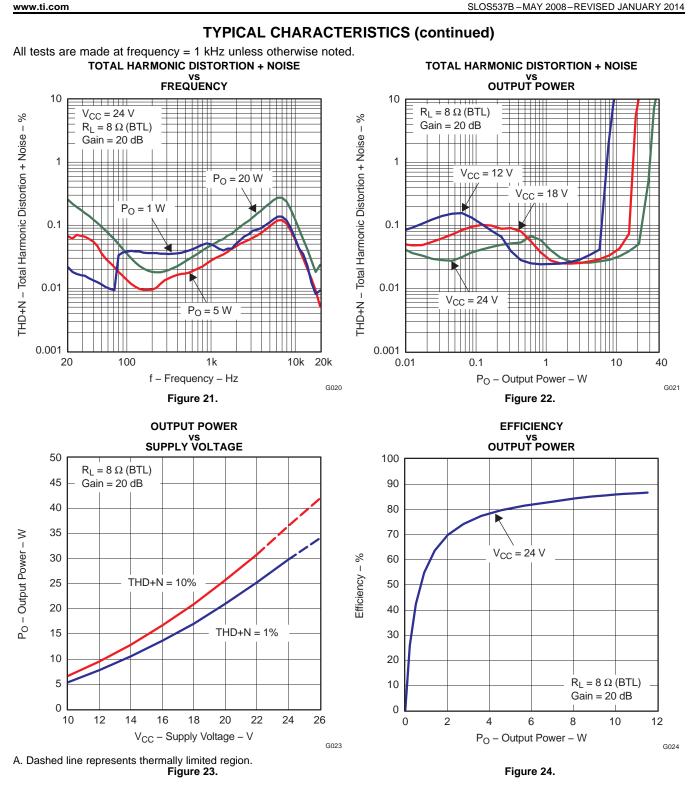
Figure 19.

Figure 20.

TEXAS INSTRUMENTS

www.ti.com

SLOS537B-MAY 2008-REVISED JANUARY 2014



EXAS

NSTRUMENTS

SLOS537B-MAY 2008-REVISED JANUARY 2014

TEXAS INSTRUMENTS

www.ti.com

APPLICATION INFORMATION

CLASS-D OPERATION

This section focuses on the class-D operation of the TPA3121D2.

Traditional Class-D Modulation Scheme

The TPA3121D2 operates in AD mode. There are two main configurations that may be used. For stereo operation, the TPA3121D2 should be configured in a single-ended (SE) half-bridge amplifier. For mono applications, TPA3121D2 may be used as a bridge-tied-load (BTL) amplifier. The traditional class-D modulation scheme, which is used in the TPA3121D2 BTL configuration, has a differential output where each output is 180 degrees out of phase and changes from ground to the supply voltage, V_{CC} . Therefore, the differential prefiltered output varies between positive and negative V_{CC} , where filtered 50% duty cycle yields 0 V across the load. The class-D modulation scheme with voltage and current waveforms is shown in Figure 25 and Figure 26.

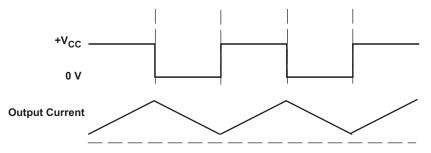


Figure 25. Class-D Modulation for TPA3121D2 SE Configuration

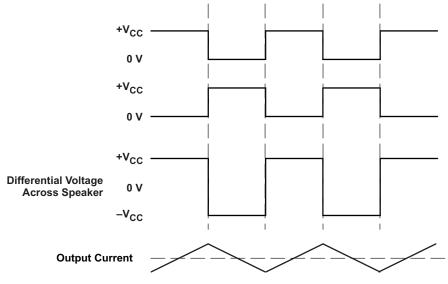


Figure 26. Class-D Modulation for TPA3121D2 BTL Configuration

Supply Pumping

One issue encountered in single-ended (SE) class-D amplifier designs is supply pumping. Power-supply pumping is a rise in the local supply voltage due to energy being driven back to the supply by operation of the class-D amplifier. This phenomenon is most evident at low audio frequencies and when both channels are operating at the same frequency and phase. At low levels, power-supply pumping results in distortion in the audio output due to fluctuations in supply voltage. At higher levels, pumping can cause the overvoltage protection to operate, which temporarily shuts down the audio output.



Several things can be done to relieve power-supply pumping. The lowest impact is to operate the two inputs out of phase 180° and reverse the speaker connections. Because most audio is highly correlated, this causes the supply pumping to be out of phase and not as severe. If this is not enough, the amount of bulk capacitance on the supply must be increased. Also, improvement is realized by hooking other supplies to this node, thereby, sinking some of the excess current. Power-supply pumping should be tested by operating the amplifier at low frequencies and high output levels.

Gain Setting via GAIN0 and GAIN1 Inputs

The gain of the TPA3121D2 is set by two input terminals, GAIN0 and GAIN1.

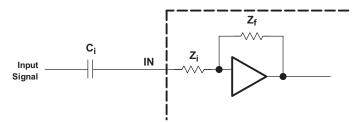
The gains listed in Table 2 are realized by changing the taps on the input resistors and feedback resistors inside the amplifier. This causes the input impedance (Z_i) to be dependent on the gain setting. The actual gain settings are controlled by ratios of resistors, so the gain variation from part-to-part is small. However, the input impedance from part-to-part at the same gain may shift by ±20% due to shifts in the actual resistance of the input resistors.

For design purposes, the input network (discussed in the next section) should be designed assuming an input impedance of 8 k Ω , which is the absolute minimum input impedance of the TPA3121D2. At the higher gain settings, the input impedance could increase as high as 72 k Ω .

GAIN1	GAIN0	AMPLIFIER GAIN (dB), TYPICAL	INPUT IMPEDANCE (kΩ), TYPICAL
0	0	20	60
0	1	26	30
1	0	32	15
1	1	36	9

INPUT RESISTANCE

Changing the gain setting can vary the input resistance of the amplifier from its smallest value, 10 k Ω ±20%, to the largest value, 60 k Ω ±20%. As a result, if a single capacitor is used in the input high-pass filter, the –3-dB cutoff frequency may change when changing gain steps.

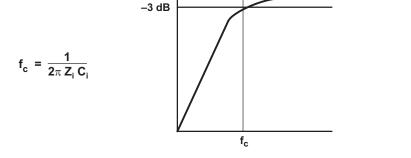


The –3-dB frequency can be calculated using Equation 1. Use the Z_i values given in Table 2.

$$f = \frac{1}{2\pi Z_i C_i}$$
(1)

INPUT CAPACITOR, C_i

In the typical application, an input capacitor (C_i) is required to allow the amplifier to bias the input signal to the proper dc level for optimum operation. In this case, C_i and the input impedance of the amplifier (Z_i) form a high-pass filter with the corner frequency determined in Equation 2.



The value of C_i is important, as it directly affects the bass (low-frequency) performance of the circuit. Consider the example where Z_i is 20 k Ω and the specification calls for a flat bass response down to 20 Hz. Equation 2 is reconfigured as Equation 3.

$$C_{i} = \frac{1}{2\pi Z_{i} f_{c}}$$
(3)

In this example, C_i is 0.4 μ F; so, one would likely choose a value of 0.47 μ F as this value is commonly used. If the gain is known and is constant, use Z_i from Table 2 to calculate C_i . A further consideration for this capacitor is the leakage path from the input source through the input network (C_i) and the feedback network to the load. This leakage current creates a dc offset voltage at the input to the amplifier that reduces useful headroom, especially in high-gain applications. For this reason, a low-leakage tantalum or ceramic capacitor is the best choice. When polarized capacitors are used, the positive side of the capacitor should face the amplifier input in most applications as the dc level there is held at 2 V, which is likely higher than the source dc level. Note that it is important to confirm the capacitor polarity in the application. Additionally, lead-free solder can create dc offset voltages, and it is important to ensure that boards are cleaned properly.

Single-Ended Output Capacitor, C_o

In single-ended (SE) applications, the dc blocking capacitor forms a high-pass filter with the speaker impedance. The frequency response rolls of with decreasing frequency at a rate of 20 dB/decade. The cutoff frequency is determined by

$$f_c = 1/2\pi C_O Z_L$$

 Table 3 shows some common component values and the associated cutoff frequencies:

Speaker Impedance (O)	C _{SE} - DC Blocking Capacitor (μF)				
Speaker Impedance (Ω)	f _c = 60 Hz (–3 dB)	f _c = 40 Hz (–3 dB)	f _c = 20 Hz (–3 dB)		
4	680	1000	2200		
6	470	680	1500		
8	330	470	1000		

For the best frequency response, a flat-passband output filter (second-order Butterworth) may be used. The output filter components consist of the series inductor and capacitor to ground at the LOUT and ROUT pins. There are several possible configurations, depending on the speaker impedance and whether the output configuration is single-ended (SE) or bridge-tied load (BTL). Table 4 lists the recommended values for the filter components. It is important to use a high-quality capacitor in this application. A rating of at least X7R is required.

 Table 3. Common Filter Responses

Output Filter and Frequency Response



(4)



www.ti.com

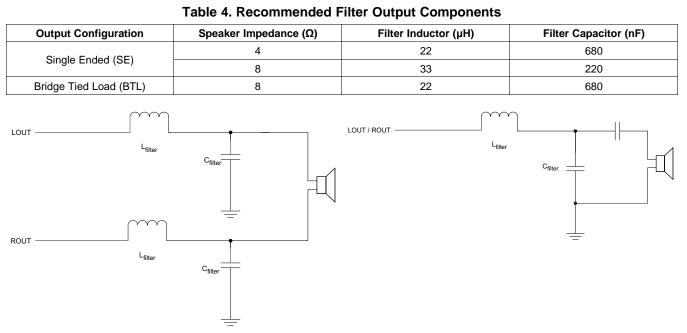


Figure 27. BTL Filter Configuration

Figure 28. SE Filter Configuration

Power-Supply Decoupling, C_s

The TPA3121D2 is a high-performance CMOS audio amplifier that requires adequate power-supply decoupling to ensure that the output total harmonic distortion (THD) is as low as possible. Power-supply decoupling also prevents oscillations for long lead lengths between the amplifier and the speaker. The optimum decoupling is achieved by using two capacitors of different types that target different types of noise on the power-supply leads. For higher-frequency transients, spikes, or digital hash on the line, a good low equivalent-series-resistance (ESR) ceramic capacitor, typically 0.1 μ F to 1 μ F, placed as close as possible to the device V_{CC} lead works best. For filtering lower frequency noise signals, a larger aluminum electrolytic capacitor of 470 μ F or greater placed near the audio power amplifier is recommended. The 470- μ F capacitor also serves as local storage capacitor for supplying current during large signal transients on the amplifier outputs. The PVCC terminals provide the power to the output transistors, so a 470- μ F or larger capacitor should be placed on each PVCC terminal. A 10- μ F capacitor on the AVCC terminal is adequate. These capacitors must be properly derated for voltage and ripple-current rating to ensure reliability.

Power Supply Rejection

TPA3121D2 has good power supply rejection due to the closed-loop architecture; however, it is possible to achieve better performance (if desired) by adding a filter between the PVCC supply and the AVCC supply. The following figures illustrate the improvement that can be obtained by adding a 220 Ω , 220 μ F filter before pins 19 and 20.



www.ti.com

SLOS537B-MAY 2008-REVISED JANUARY 2014

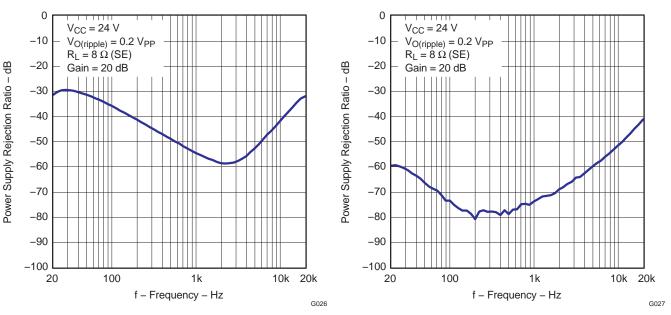




Figure 30. PSRR With AVCC Filter

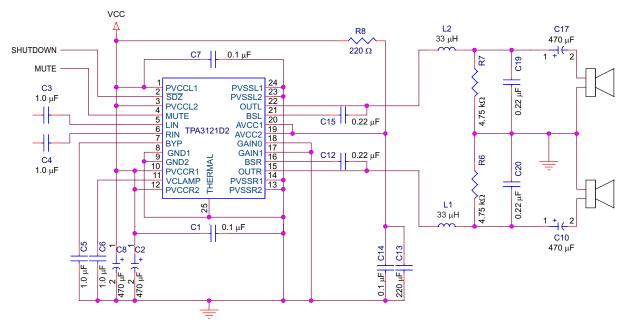


Figure 31. Application Schematic with 220- Ω /220- μ F AVCC Filter

BSN and BSP Capacitors

The half H-bridge output stages use only NMOS transistors. Therefore, they require bootstrap capacitors for the high side of each output to turn on correctly. A 220-nF ceramic capacitor, rated for at least 25 V, must be connected from each output to its corresponding bootstrap input. Specifically, one 220-nF capacitor must be connected from LOUT to BSL, and one 220-nF capacitor must be connected from ROUT to BSR.

The bootstrap capacitors connected between the BSx pins and their corresponding outputs function as a floating power supply for the high-side N-channel power MOSFET gate-drive circuitry. During each high-side switching cycle, the bootstrap capacitors hold the gate-to-source voltage high enough to keep the high-side MOSFETs turned on.



VCLAMP Capacitor

To ensure that the maximum gate-to-source voltage for the NMOS output transistors is not exceeded, one internal regulator clamps the gate voltage. One $1-\mu F$ capacitor must be connected from VCLAMP (pin 11) to ground and must be rated for at least 16 V. The voltages at the VCLAMP terminal may vary with V_{CC} and may not be used for powering any other circuitry.

VBYP Capacitor Selection

The scaled supply reference (VBYP) nominally provides an AVCC/8 internal bias for the preamplifier stages. The external capacitor for this reference (C_{BYP}) is a critical component and serves several important functions. During start-up or recovery from shutdown mode, C_{BYP} determines the rate at which the amplifier starts. The start up time is proportional to 0.5 s per microfarad. Thus, the recommended 1-µF capacitor results in a start-up time of approximately 500 ms. The second function is to reduce noise produced by the power supply caused by coupling with the output drive signal. This noise could result in degraded power-supply rejection and THD+N.

The circuit is designed for a C_{BYP} value of 1 μ F for best pop performance. The input capacitors should have the same value. A ceramic or tantalum low-ESR capacitor is recommended.

SHUTDOWN OPERATION

The TPA3121D2 employs a shutdown mode of operation designed to <u>reduce supply</u> current (I_{CC}) to the absolute minimum level during periods of nonuse for power conservation. The SHUTDOWN input terminal should be held <u>high (see specification table for trip point)</u> during normal operation when the amplifier is in use. Pulling <u>SHUTDOWN</u> low causes the outputs to mute and the amplifier to enter a low-current state. Never leave SHUTDOWN unconnected, because amplifier operation would be unpredictable.

For the best power-up *pop* performance, place the amplifier in the shutdown or mute mode prior to applying the power-supply voltage.

MUTE Operation

The MUTE pin is an input for controlling the output state of the TPA3121D2. A logic high on this terminal causes the outputs to run at a constant 50% duty cycle. A logic low on this pin enables the outputs. This terminal may be used as a quick disable/enable of outputs when changing channels on a television or transitioning between different audio sources.

The MUTE terminal should never be left floating. For power conservation, the SHUTDOWN terminal should be used to reduce the quiescent current to the absolute minimum level.

USING LOW-ESR CAPACITORS

Low-ESR capacitors are recommended throughout this application section. A real (as opposed to ideal) capacitor can be modeled simply as a resistor in series with an ideal capacitor. The voltage drop across this resistor minimizes the beneficial effects of the capacitor in the circuit. The lower the equivalent value of this resistance, the more the real capacitor behaves like an ideal capacitor.

SHORT-CIRCUIT PROTECTION

The TPA3121D2 has short-circuit protection circuitry on the outputs that prevents damage to the device during output-to-output shorts and output-to-GND shorts after the filter and output capacitor (at the speaker terminal.) Directly at the device terminals, the protection circuitry prevents damage to device during output-to-output, output-to-ground, and output-to-supply. When a short circuit is detected on the outputs, the part immediately disables the output drive. This is an unlatched fault. Normal operation is restored when the fault is removed.



THERMAL PROTECTION

Thermal protection on the TPA3121D2 prevents damage to the device when the internal die temperature exceeds 150° C. There is a $\pm 15^{\circ}$ C tolerance on this trip point from device to device. Once the die temperature exceeds the thermal set point, the device enters into the shutdown state and the outputs are disabled. This is not a latched fault. The thermal fault is cleared once the temperature of the die is reduced by 30° C. The device begins normal operation at this point with no external system interaction.

PRINTED-CIRCUIT BOARD (PCB) LAYOUT

Because the TPA3121D2 is a class-D amplifier that switches at a high frequency, the layout of the printed-circuit board (PCB) should be optimized according to the following guidelines for the best possible performance.

- Decoupling capacitors—The high-frequency 0.1-µF decoupling capacitors should be placed as close to the PVCC (pins 1, 3, 10, and 12) and AVCC (pins 19 and 20) terminals as possible. The VBYP (pin 7) capacitor and VCLAMP (pin 11) capacitor should also be placed as close to the device as possible. Large (220-µF or greater) bulk power-supply decoupling capacitors should be placed near the TPA3121D2 on the PVCCL and PVCCR terminals.
- Grounding—The AVCC (pins 19 and 20) decoupling capacitor and VBYP (pin 7) capacitor should each be grounded to analog ground (AGND, pins 8 and 9). The PVCCx decoupling capacitors and VCLAMP capacitors should each be grounded to power ground (PGND, pins 13, 14, 23, and 24). Analog ground and power ground should be connected at the thermal pad, which should be used as a central ground connection or star ground for the TPA3121D2.
- Output filter—The reconstruction filter (L1, L2, C9, and C16) should be placed as close to the output terminals as possible for the best EMI performance. The capacitors should be grounded to power ground.
- Thermal pad—The thermal pad must be soldered to the PCB for proper thermal performance and optimal reliability. The dimensions of the thermal pad and thermal land are described in the mechanical section at the back of the data sheet. See TI Technical Briefs SLMA002 and SLOA120 for more information about using the thermal pad. For recommended PCB footprints, see figures at the end of this data sheet.

For an example layout, see the TPA3121D2 Evaluation Module (TPA3121D2EVM) User Manual, (SLOU189). Both the EVM user manual and the thermal pad application note are available on the TI Web site at http://www.ti.com.



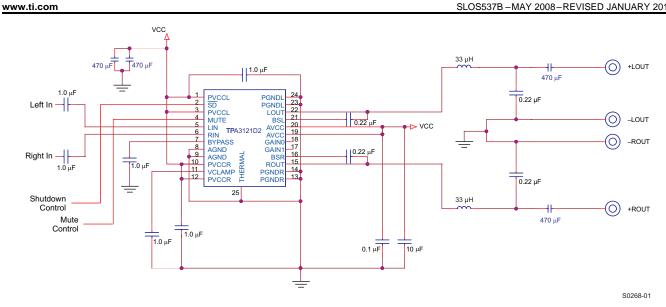


Figure 32. Schematic for Single-Ended (SE) Configuration (8-Ω Speaker)

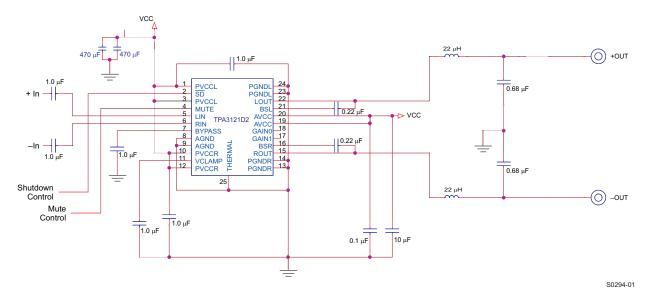


Figure 33. Schematic for Bridge-Tied-Load (BTL) Configuration (8-Ω Speaker)



BASIC MEASUREMENT SYSTEM

This section focuses on methods that use the basic equipment listed below:

- Audio analyzer or spectrum analyzer
- Digital multi meter (DMM)
- Oscilloscope
- Twisted-pair wires
- Signal generator
- Power resistor(s)
- Linear regulated power supply
- Filter components
- EVM or other complete audio circuit

Figure 34 shows the block diagrams of basic measurement systems for class-AB and class-D amplifiers. A sine wave is normally used as the input signal because it consists of the fundamental frequency only (no other harmonics are present). An analyzer is then connected to the audio power amplifier (APA) output to measure the voltage output. The analyzer must be capable of measuring the entire audio bandwidth. A regulated dc power supply is used to reduce the noise and distortion injected into the APA through the power pins. A System Two[™] audio measurement system (AP-II) by Audio Precision[™] includes the signal generator and analyzer in one package.

The generator output and amplifier input must be ac-coupled. However, the EVMs already have the ac-coupling capacitors, \mathbb{O}_{IN}), so no additional coupling is required. The generator output impedance should be low to avoid attenuating the test signal, and is important because the input resistance of APAs is not high. Conversely, the analyzer input impedance should be high. The output resistance, R_{OUT} , of the APA is normally in the hundreds of milliohms and can be ignored for all but the power-related calculations.

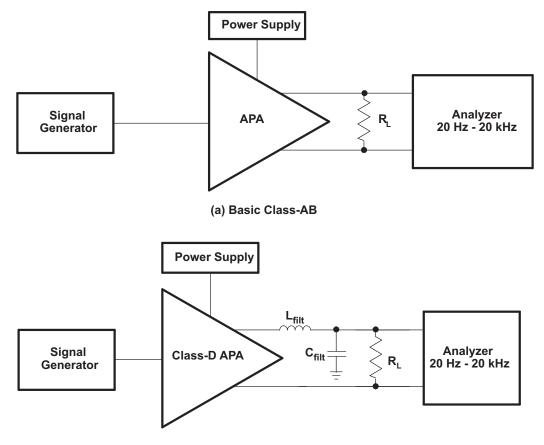
Figure 34(a) shows a class-AB amplifier system. It takes an analog signal input and produces an analog signal output. This amplifier circuit can be directly connected to the AP-II or other analyzer input.

This is not true of the class-D amplifier system shown in Figure 34(b), which requires low-pass filters in most cases in order to measure the audio output waveforms. This is because it takes an analog input signal and converts it into a pulse-width modulated (PWM) output signal that is not accurately processed by some analyzers.



SLOS537B-MAY 2008-REVISED JANUARY 2014





(b) Traditional Class-D

Figure 34. Audio Measurement Systems

SLOS537B-MAY 2008-REVISED JANUARY 2014

SE Input and SE Output (TPA3121D2 Stereo Configuration)

The SE input and output configuration is used with class-AB amplifiers. A block diagram of a fully SE measurement circuit is shown in Figure 35. SE inputs normally have one input pin per channel. In some cases, two pins are present; one is the signal and the other is ground. SE outputs have one pin driving a load through an output ac-coupling capacitor and the other end of the load is tied to ground. SE inputs and outputs are considered to be unbalanced, meaning one end is tied to ground and the other to an amplifier input/output.

The generator should have unbalanced outputs, and the signal should be referenced to the generator ground for best results. Unbalanced or balanced outputs can be used when floating, but they may create a ground loop that affects the measurement accuracy. The analyzer should have balanced inputs to cancel out any common-mode noise in the measurement.

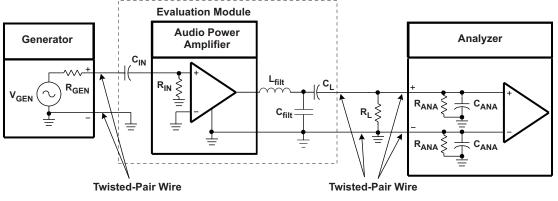


Figure 35. SE Input—SE Output Measurement Circuit

The following general rules should be followed when connecting to APAs with SE inputs and outputs:

- Use an unbalanced source to supply the input signal.
- Use an analyzer with balanced inputs.
- Use twisted-pair wire for all connections.
- Use shielding when the system environment is noisy.
- Ensure the cables from the power supply to the APA, and from the APA to the load, can handle the large currents (see Table 5).



SLOS537B-MAY 2008-REVISED JANUARY 2014

DIFFERENTIAL INPUT AND BTL OUTPUT (TPA3121D2 Mono Configuration)

Many of the class-D APAs and many class-AB APAs have differential inputs and bridge-tied-load (BTL) outputs. Differential inputs have two input pins per channel and amplify the difference in voltage between the pins. Differential inputs reduce the common-mode noise and distortion of the input circuit. BTL is a term commonly used in audio to describe differential outputs. BTL outputs have two output pins providing voltages that are 180° out of phase. The load is connected between these pins. This has the added benefits of quadrupling the output power to the load and eliminating a dc-blocking capacitor.

A block diagram of the measurement circuit is shown in Figure 36. The differential input is a balanced input, meaning the positive (+) and negative (-) pins have the same impedance to ground. Similarly, the SE output equates to a balanced output.

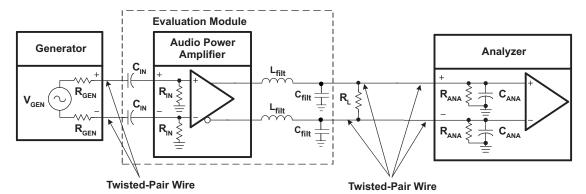


Figure 36. Differential Input, BTL Output Measurement Circuit

The generator should have balanced outputs, and the signal should be balanced for best results. An unbalanced output can be used, but it may create a ground loop that affects the measurement accuracy. The analyzer must also have balanced inputs for the system to be fully balanced, thereby cancelling out any common-mode noise in the circuit and providing the most accurate measurement.

The following general rules should be followed when connecting to APAs with differential inputs and BTL outputs:

- Use a balanced source to supply the input signal.
- Use an analyzer with balanced inputs.
- Use twisted-pair wire for all connections.
- Use shielding when the system environment is noisy.
- Ensure that the cables from the power supply to the APA, and from the APA to the load, can handle the large currents (see Table 5).

Table 5 shows the recommended wire size for the power supply and load cables of the APA system. The real concern is the dc or ac power loss that occurs as the current flows through the cable. These recommendations are based on 12-inch (30.5-cm)-long wire with a 20-kHz sine-wave signal at 25°C.

Table 5. Recommended Minimum Wire Size for Powe	er Cables
---	-----------

P _{OUT} (W)	R _L (Ω)	AWG Size			ER LOSS W)		ER LOSS W)
10	4	18	22	16	40	18	42
2	4	18	22	3.2	8	3.7	8.5
1	8	22	28	2	8	2.1	8.1
< 0.75	8	22	28	1.5	6.1	1.6	6.2

SLOS537B-MAY 2008-REVISED JANUARY 2014

REVISION HISTORY

Changes from Revision A (August 2010) to Revision B	Page				
Changed L1 and L2 From: 33 μF To: 33 μH in Figure 31					
Changes from Original (May 2008) to Revision A	Page				
Replaced the Dissipations Ratings table with the Thermal Information table	3				



PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
							(6)				
TPA3121D2PWP	ACTIVE	HTSSOP	PWP	24	60	RoHS & Green	NIPDAU	Level-3-260C-168 HR	-40 to 85	TPA3121D2	Samples
TPA3121D2PWPG4	ACTIVE	HTSSOP	PWP	24	60	RoHS & Green	NIPDAU	Level-3-260C-168 HR	-40 to 85	TPA3121D2	Samples
TPA3121D2PWPR	ACTIVE	HTSSOP	PWP	24	2000	RoHS & Green	NIPDAU	Level-3-260C-168 HR	-40 to 85	TPA3121D2	Samples

⁽¹⁾ The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

⁽²⁾ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

⁽³⁾ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

⁽⁴⁾ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

⁽⁵⁾ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

Important Information and Disclaimer:The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.



PACKAGE OPTION ADDENDUM

10-Dec-2020

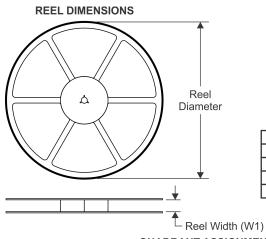
In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

PACKAGE MATERIALS INFORMATION

Texas Instruments

www.ti.com

TAPE AND REEL INFORMATION





QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



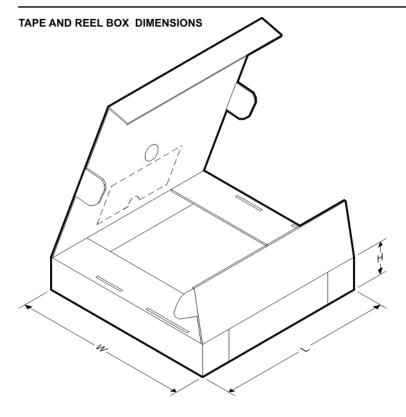
*All dimensions ar	e nominal
--------------------	-----------

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPA3121D2PWPR	HTSSOP	PWP	24	2000	330.0	16.4	6.95	8.3	1.6	8.0	16.0	Q1



PACKAGE MATERIALS INFORMATION

5-Jan-2022



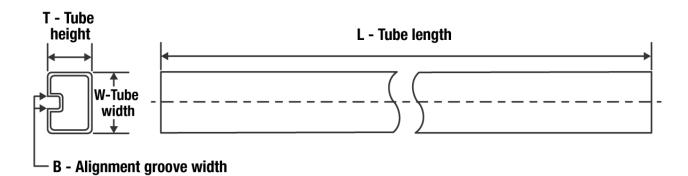
*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)	
TPA3121D2PWPR	HTSSOP	PWP	24	2000	350.0	350.0	43.0	



5-Jan-2022

TUBE



*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	Τ (μm)	B (mm)
TPA3121D2PWP	PWP	HTSSOP	24	60	530	10.2	3600	3.5
TPA3121D2PWPG4	PWP	HTSSOP	24	60	530	10.2	3600	3.5

PWP 24

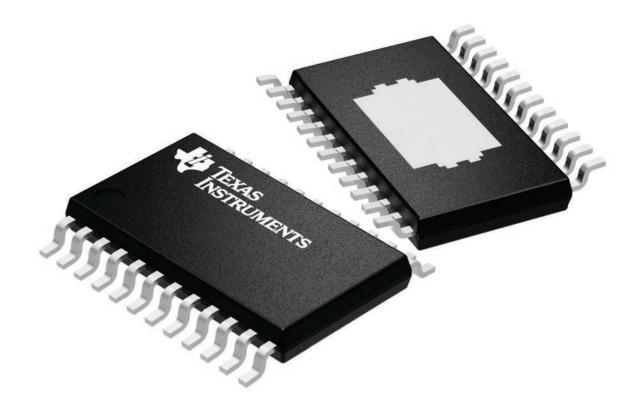
GENERIC PACKAGE VIEW

PowerPAD[™] TSSOP - 1.2 mm max height

PLASTIC SMALL OUTLINE

4.4 x 7.6, 0.65 mm pitch

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



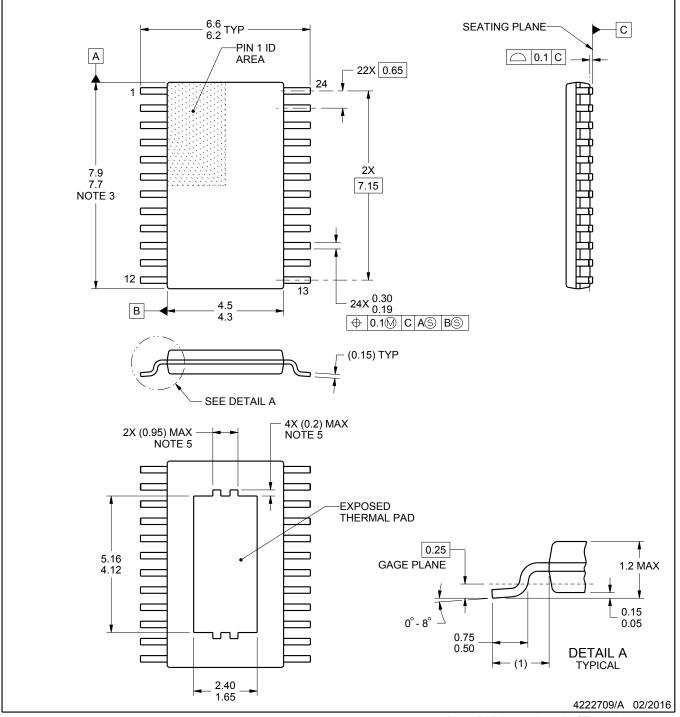


PACKAGE OUTLINE

PWP0024B

PowerPAD[™] TSSOP - 1.2 mm max height

PLASTIC SMALL OUTLINE



NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 mm per side. 4. Reference JEDEC registration MO-153.
- 5. Features may not be present and may vary.

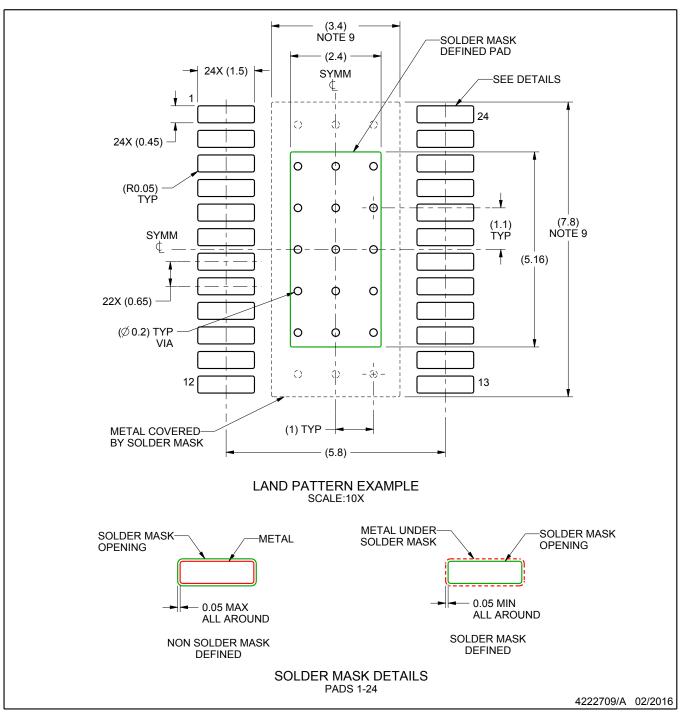


PWP0024B

EXAMPLE BOARD LAYOUT

PowerPAD[™] TSSOP - 1.2 mm max height

PLASTIC SMALL OUTLINE



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

 This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).

9. Size of metal pad may vary due to creepage requirement.

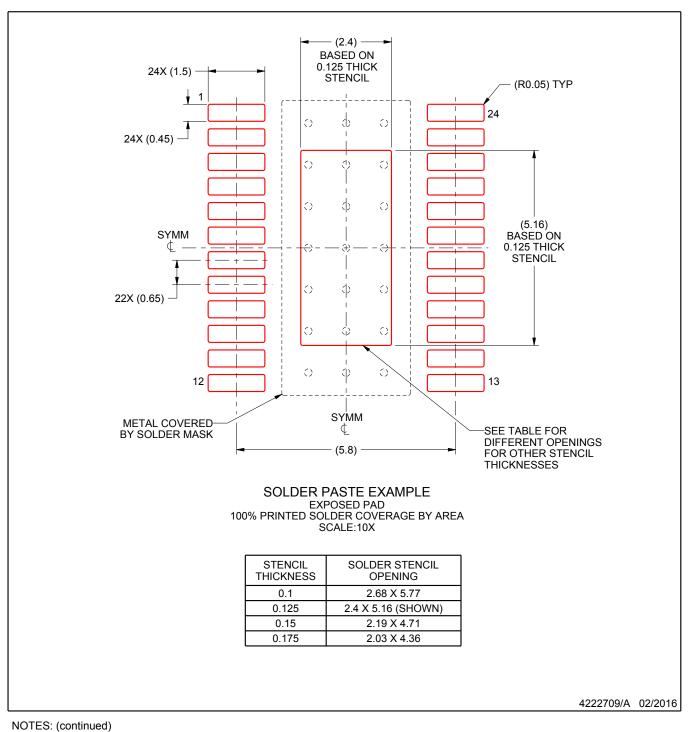


PWP0024B

EXAMPLE STENCIL DESIGN

PowerPAD[™] TSSOP - 1.2 mm max height

PLASTIC SMALL OUTLINE



10. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

11. Board assembly site may have different recommendations for stencil design.



IMPORTANT NOTICE AND DISCLAIMER

TI PROVIDES TECHNICAL AND RELIABILITY DATA (INCLUDING DATA SHEETS), DESIGN RESOURCES (INCLUDING REFERENCE DESIGNS), APPLICATION OR OTHER DESIGN ADVICE, WEB TOOLS, SAFETY INFORMATION, AND OTHER RESOURCES "AS IS" AND WITH ALL FAULTS, AND DISCLAIMS ALL WARRANTIES, EXPRESS AND IMPLIED, INCLUDING WITHOUT LIMITATION ANY IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE OR NON-INFRINGEMENT OF THIRD PARTY INTELLECTUAL PROPERTY RIGHTS.

These resources are intended for skilled developers designing with TI products. You are solely responsible for (1) selecting the appropriate TI products for your application, (2) designing, validating and testing your application, and (3) ensuring your application meets applicable standards, and any other safety, security, regulatory or other requirements.

These resources are subject to change without notice. TI grants you permission to use these resources only for development of an application that uses the TI products described in the resource. Other reproduction and display of these resources is prohibited. No license is granted to any other TI intellectual property right or to any third party intellectual property right. TI disclaims responsibility for, and you will fully indemnify TI and its representatives against, any claims, damages, costs, losses, and liabilities arising out of your use of these resources.

TI's products are provided subject to TI's Terms of Sale or other applicable terms available either on ti.com or provided in conjunction with such TI products. TI's provision of these resources does not expand or otherwise alter TI's applicable warranties or warranty disclaimers for TI products.

TI objects to and rejects any additional or different terms you may have proposed.

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2022, Texas Instruments Incorporated