Dual Operational Transconductance Amplifier

The AU5517 and NE5517 contain two current-controlled transconductance amplifiers, each with a differential input and push-pull output. The AU5517/NE5517 offers significant design and performance advantages over similar devices for all types of programmable gain applications. Circuit performance is enhanced through the use of linearizing diodes at the inputs which enable a 10 dB signal-to-noise improvement referenced to 0.5% THD. The AU5517/NE5517 is suited for a wide variety of industrial and consumer applications.

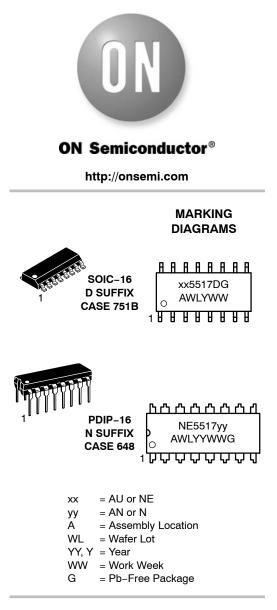
Constant impedance of the buffers on the chip allow general use of the AU5517/NE5517. These buffers are made of Darlington transistors and a biasing network that virtually eliminate the change of offset voltage due to a burst in the bias current I_{ABC} , hence eliminating the audible noise that could otherwise be heard in high quality audio applications.

Features

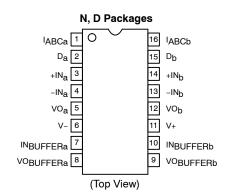
- Constant Impedance Buffers
- ΔV_{BE} of Buffer is Constant with Amplifier I_{BIAS} Change
- Excellent Matching Between Amplifiers
- Linearizing Diodes
- High Output Signal-to-Noise Ratio
- Pb-Free Packages are Available*

Applications

- Multiplexers
- Timers
- Electronic Music Synthesizers
- Dolby® HX Systems
- Current-Controlled Amplifiers, Filters
- Current-Controlled Oscillators, Impedances



PIN CONNECTIONS



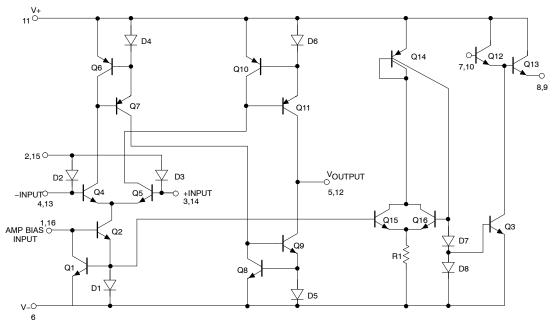
ORDERING INFORMATION

See detailed ordering and shipping information in the package dimensions section on page 13 of this data sheet.

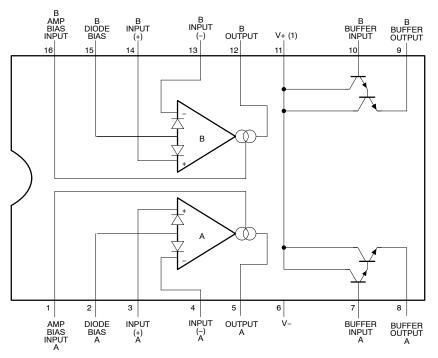
*For additional information on our Pb-Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

PIN DESCRIPTION

| Pin No. | Symbol | Description |
|---------|-----------------------|------------------------|
| 1 | I _{ABCa} | Amplifier Bias Input A |
| 2 | Da | Diode Bias A |
| 3 | +IN _a | Non-inverted Input A |
| 4 | -IN _a | Inverted Input A |
| 5 | VO _a | Output A |
| 6 | V– | Negative Supply |
| 7 | IN _{BUFFERa} | Buffer Input A |
| 8 | VO _{BUFFERa} | Buffer Output A |
| 9 | VO _{BUFFERb} | Buffer Output B |
| 10 | IN _{BUFFERb} | Buffer Input B |
| 11 | V+ | Positive Supply |
| 12 | VOb | Output B |
| 13 | -IN _b | Inverted Input B |
| 14 | +IN _b | Non-inverted Input B |
| 15 | D _b | Diode Bias B |
| 16 | I _{ABCb} | Amplifier Bias Input B |







NOTE: V+ of output buffers and amplifiers are internally connected.

Figure 2. Connection Diagram

MAXIMUM RATINGS

| Rating | Symbol | Value | Unit |
|---|------------------|-------------------------------------|------|
| Supply Voltage (Note 1) | V _S | 44 V _{DC} or ±22 | V |
| Power Dissipation, T _{amb} = 25 °C (Still Air) (Note 2) NE5517N, NE5517AN NE5517D, AU5517D | PD | 1500 1125 | mW |
| Thermal Resistance, Junction-to-Ambient D Package N Package | R _{θJA} | 140 94 | °C/W |
| Differential Input Voltage | V _{IN} | ±5.0 | V |
| Diode Bias Current | ا _D | 2.0 | mA |
| Amplifier Bias Current | I _{ABC} | 2.0 | mA |
| Output Short-Circuit Duration | I _{SC} | Indefinite | |
| Buffer Output Current (Note 3) | I _{OUT} | 20 | mA |
| Operating Temperature Range NE5517N, NE5517AN AU5517T | T _{amb} | 0 °C to +70 °C -40 °C to +125 °C | °C |
| Operating Junction Temperature | TJ | 150 | °C |
| DC Input Voltage | V _{DC} | $+V_{S}$ to $-V_{S}$ | |
| Storage Temperature Range | T _{stg} | –65 °C to +150 °C | °C |
| Lead Soldering Temperature (10 sec max) | T _{sld} | 230 | °C |

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

1. For selections to a supply voltage above ±22 V, contact factory.

2. The following derating factors should be applied above 25 $^\circ\mathrm{C}$

N package at 10.6 mW/°C D package at 7.1 mW/°C.

3. Buffer output current should be limited so as to not exceed package dissipation.

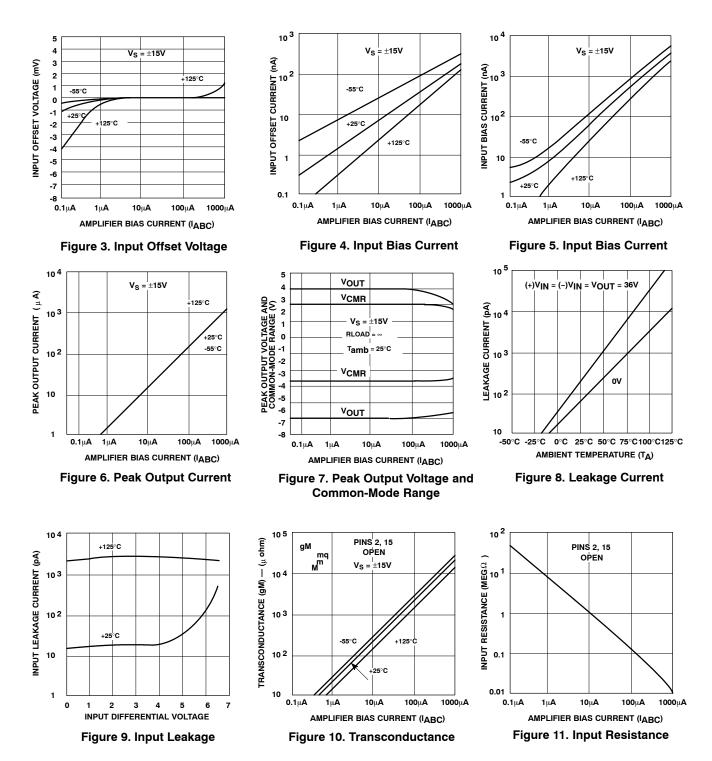
ELECTRICAL CHARACTERISTICS (Note 4)

| | | | AU5517/NE5517 | | | NE5517A | | | |
|---|--|----------------------|---------------|----------------|------------|-------------------|----------------|------------|-------|
| Characteristic | Test Conditions | Symbol | Min | Тур | Max | Min | Тур | Max | Unit |
| Input Offset Voltage | Overtemperature Range | V _{OS} | | 0.4 | 5.0 | | 0.4 | 2.0 5.0 | mV |
| | I _{ABC} 5.0 μA | | | 0.3 | 5.0 | | 0.3 | 2.0 | |
| $\Delta V_{OS} / \Delta T$ | Avg. TC of Input Offset Voltage | | | 7.0 | | | 7.0 | | μV/°C |
| V _{OS} Including Diodes | Diode Bias Current (I _D) = 500 μA | | | 0.5 | 5 | | 0.5 | 2.0 | mV |
| Input Offset Change | 5.0 μA ≤ I _{ABC} ≤ 500 μA | V _{OS} | | 0.1 | | | 0.1 | 3.0 | mV |
| Input Offset Current | | I _{OS} | | 0.1 | 0.6 | | 0.1 | 0.6 | μA |
| $\Delta I_{OS} / \Delta T$ | Avg. TC of Input Offset Current | | | 0.001 | | | 0.001 | | μA/°C |
| Input Bias Current | Overtemperature Range | I _{BIAS} | | 0.4 1.0 | 5.0 8.0 | | 0.4 1.0 | 5.0 7.0 | μA |
| $\Delta I_{B} / \Delta T$ | Avg. TC of Input Current | | | 0.01 | | | 0.01 | | μA/°C |
| Forward Transconductance | Overtemperature Range | Ям | 6700 5400 | 9600 | 13000 | 7700 4000 | 9600 | 12000 | μmho |
| g _M Tracking | | | | 0.3 | | | 0.3 | | dB |
| Peak Output Current | $\begin{array}{l} R_L = 0, \ I_{ABC} = 5.0 \ \mu A \\ R_L = 0, \ I_{ABC} = 500 \ \mu A \\ R_L = 0, \ Overtemperature \\ Range \end{array}$ | I _{OUT} | 350 300 | 5.0 500 | 650 | 3.0 350 300 | 5.0 500 | 7.0 650 | μΑ |
| Peak Output Voltage Positive Negative | $ \begin{aligned} R_L &= \infty, \ 5.0 \ \mu A \leq I_{ABC} \leq 500 \ \mu A \\ R_L &= \infty, \ 5.0 \ \mu A \leq I_{ABC} \leq 500 \ \mu A \end{aligned} $ | V _{OUT} | +12 -12 | +14.2 -14.4 | | +12 -12 | +14.2 -14.4 | | V |
| Supply Current | I_{ABC} = 500 μ A, both channels | I _{CC} | | 2.6 | 4.0 | | 2.6 | 4.0 | mA |
| V _{OS} Sensitivity Positive Negative | Δ V _{OS} / Δ V+ Δ V _{OS} / Δ V- | | | 20 20 | 150 150 | | 20 20 | 150 150 | μV/V |
| Common-mode Rejection Ration | | CMRR | 80 | 110 | | 80 | 110 | | dB |
| Common-mode Range | | | ±12 | ±13.5 | | ±12 | ±13.5 | | V |
| Crosstalk | Referred to Input (Note 5) 20 Hz < f < 20 kHz | | | 100 | | | 100 | | dB |
| Differential Input Current | $I_{ABC} = 0$, Input = $\pm 4.0 \text{ V}$ | l _{IN} | | 0.02 | 100 | | 0.02 | 10 | nA |
| Leakage Current | I _{ABC} = 0 (Refer to Test Circuit) | | | 0.2 | 100 | | 0.2 | 5.0 | nA |
| Input Resistance | | R _{IN} | 10 | 26 | | 10 | 26 | | kΩ |
| Open-loop Bandwidth | | B _W | | 2.0 | | | 2.0 | | MHz |
| Slew Rate | Unity Gain Compensated | SR | | 50 | | | 50 | | V/μs |
| Buffer Input Current | 5 | IN _{BUFFER} | | 0.4 | 5.0 | | 0.4 | 5.0 | μA |
| Peak Buffer Output Voltage | 5 | VO _{BUFFER} | 10 | | | 10 | | | V |
| ΔV_{BE} of Buffer | Refer to Buffer V _{BE} Test Circuit (Note 6) | | | 0.5 | 5.0 | | 0.5 | 5.0 | mV |

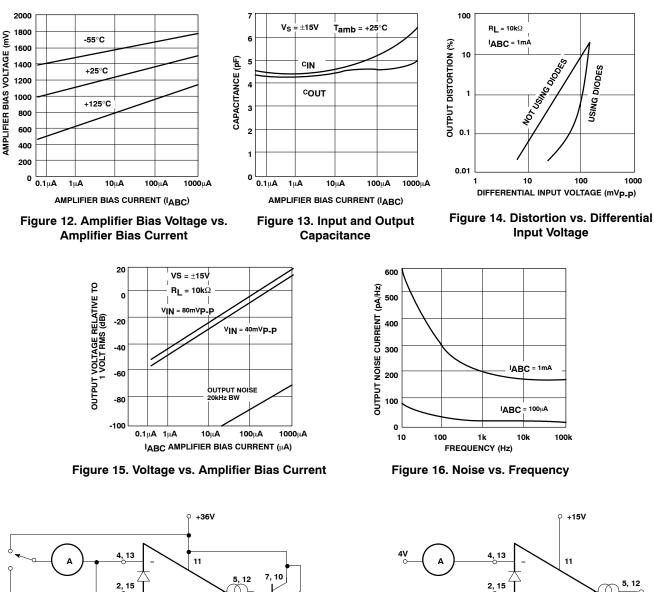
4. These specifications apply for V_S = ±15 V, T_{amb} = 25°C, amplifier bias current (I_{ABC}) = 500 μA, Pins 2 and 15 open unless otherwise specified. The inputs to the buffers are grounded and outputs are open.
5. These specifications apply for V_S = ±15 V, I_{ABC} = 500 μA, R_{OUT} = 5.0 kΩ connected from the buffer output to -V_S and the input of the buffer is connected to the transconductance amplifier output.

6. V_S = ±15, R_{OUT} = 5.0 k Ω connected from Buffer output to -V_S and 5.0 μ A ≤ I_{ABC} ≤ 500 μ A.

TYPICAL PERFORMANCE CHARACTERISTICS



TYPICAL PERFORMANCE CHARACTERISTICS (continued)



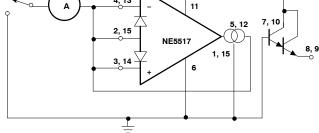


Figure 17. Leakage Current Test Circuit

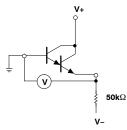


Figure 19. Buffer V_{BE} Test Circuit

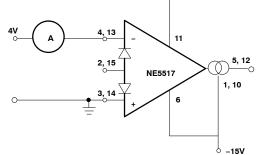


Figure 18. Differential Input Current Test Circuit

APPLICATIONS

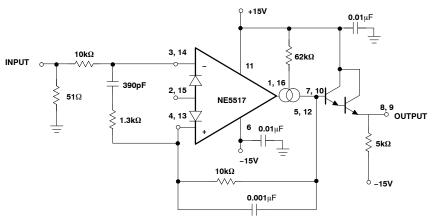


Figure 20. Unity Gain Follower

CIRCUIT DESCRIPTION

The circuit schematic diagram of one-half of the AU5517/NE5517, a dual operational transconductance amplifier with linearizing diodes and impedance buffers, is shown in Figure 21.

Transconductance Amplifier

The transistor pair, Q_4 and Q_5 , forms a transconductance stage. The ratio of their collector currents (I_4 and I_5 , respectively) is defined by the differential input voltage, V_{IN} , which is shown in Equation 1.

$$V_{IN} = \frac{KT}{q} \ln \frac{I_5}{I_4}$$
 (eq. 1)

Where V_{IN} is the difference of the two input voltages

 $KT \cong 26 \text{ mV}$ at room temperature (300°k).

Transistors Q_1 , Q_2 and diode D_1 form a current mirror which focuses the sum of current I_4 and I_5 to be equal to amplifier bias current I_B :

$$I_4 + I_5 = I_B \tag{eq. 2}$$

If V_{IN} is small, the ratio of I_5 and I_4 will approach unity and the Taylor series of In function can be approximated as

$$\begin{array}{l} \frac{\text{KT}}{\text{q}} \, \ln \, \frac{\text{I}_5}{\text{I}_4} \approx \frac{\text{KT}}{\text{q}} \, \frac{\text{I}_5 - \text{I}_4}{\text{I}_4} \\ \\ \text{and} \, \text{I}_4 \cong \text{I}_5 \cong \text{I}_B \end{array} \tag{eq. 3}$$

$$\frac{\text{KT}}{\text{q}} \text{In} \frac{\text{I}_{5}}{\text{I}_{4}} \approx \frac{\text{KT}}{\text{q}} \frac{\text{I}_{5} - \text{I}_{4}}{1/2\text{I}_{\text{B}}} = \frac{2\text{KT}}{\text{q}} \frac{\text{I}_{5} - \text{I}_{4}}{\text{I}_{\text{B}}} = \text{V}_{\text{IN}} \quad (\text{eq. 4})$$
$$\text{I}_{5} - \text{I}_{4} = \text{V}_{\text{IN}} \frac{\left(\text{I}_{\text{B}}^{\text{q}}\right)}{2\text{KT}}$$

The remaining transistors (Q_6 to Q_{11}) and diodes (D_4 to D_6) form three current mirrors that produce an output current equal to I_5 minus I_4 . Thus:

$$V_{IN}\left(I_{B}\frac{q}{2KT}\right) = I_{O} \qquad (eq. 5)$$

The term $\frac{(I_B^{q})}{2KT}$ is then the transconductance of the amplifier and is proportional to I_B.

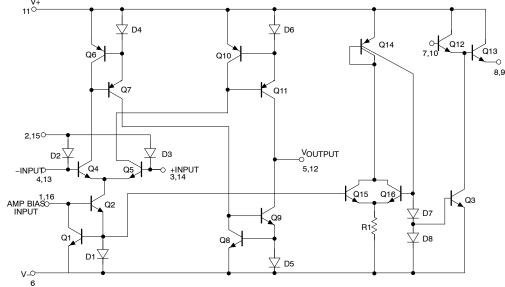


Figure 21. Circuit Diagram of NE5517

Linearizing Diodes

For V_{IN} greater than a few millivolts, Equation 3 becomes invalid and the transconductance increases non-linearly. Figure 22 shows how the internal diodes can linearize the transfer function of the operational amplifier. Assume D₂ and D₃ are biased with current sources and the input signal current is I_S. Since I₄ + I₅ = I_B and I₅ - I₄ = I₀, that is: I₄ = (I_B - I₀), I₅ = (I_B + I₀)

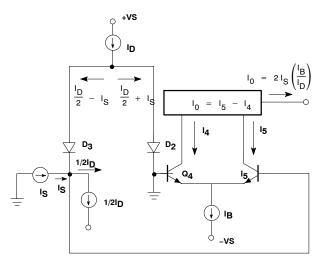


Figure 22. Linearizing Diode

For the diodes and the input transistors that have identical geometries and are subject to similar voltages and temperatures, the following equation is true:

$$\frac{T}{q} \ln \frac{\frac{I_D}{2} + I_S}{\frac{I_D}{2} - I_S} = \frac{KT}{q} \ln \frac{1/2(I_B + I_O)}{1/2(I_B - I_O)}$$
(eq. 6)
$$I_O = I_S \frac{2IB}{I_D} \text{ for } |I_S| < \frac{I_D}{2}$$

The only limitation is that the signal current should not exceed I_D .

Impedance Buffer

The upper limit of transconductance is defined by the maximum value of I_B (2.0 mA). The lowest value of I_B for which the amplifier will function therefore determines the overall dynamic range. At low values of I_B , a buffer with very low input bias current is desired. A Darlington amplifier with constant-current source ($Q_{14}, Q_{15}, Q_{16}, D_7, D_8$, and R_1) suits the need.

APPLICATIONS

Voltage-Controlled Amplifier

In Figure 23, the voltage divider R_2 , R_3 divides the input-voltage into small values (mV range) so the amplifier operates in a linear manner.

It is:

$$I_{OUT} = -V_{IN} \cdot \frac{R_3}{R_2 + R_3} \cdot g_M;$$
$$V_{OUT} = I_{OUT} \cdot R_L;$$
$$A = \frac{V_{OUT}}{V_{IN}} = \frac{R_3}{R_2 + R_3} \cdot g_M \cdot R_L$$
(3) $g_M = 19.2 I_{ABC}$ (g_M in umbos for I_{ABC} in mA)

Since g_M is directly proportional to I_{ABC} , the amplification is controlled by the voltage V_C in a simple way.

When V_C is taken relative to $-V_{CC}$ the following formula is valid:

$$I_{ABC} = \frac{(V_C - 1.2V)}{R_1}$$

The 1.2 V is the voltage across two base-emitter baths in the current mirrors. This circuit is the base for many applications of the AU5517/NE5517.

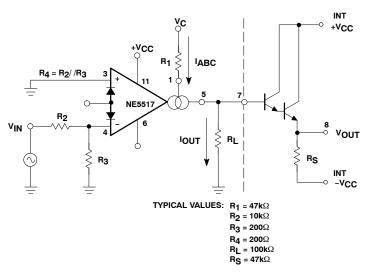


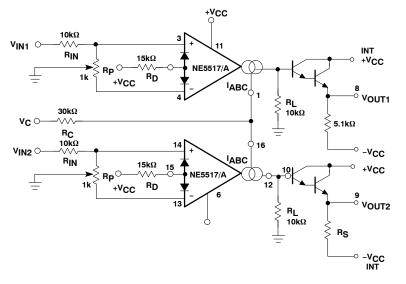
Figure 23.

Stereo Amplifier With Gain Control

Figure 24 shows a stereo amplifier with variable gain via a control input. Excellent tracking of typical 0.3 dB is easy to achieve. With the potentiometer, R_P , the offset can be adjusted. For AC-coupled amplifiers, the potentiometer may be replaced with two 510 Ω resistors.

Modulators

Because the transconductance of an OTA (Operational Transconductance Amplifier) is directly proportional to I_{ABC} , the amplification of a signal can be controlled easily. The output current is the product from transconductance×input voltage. The circuit is effective up to approximately 200 kHz. Modulation of 99% is easy to achieve.





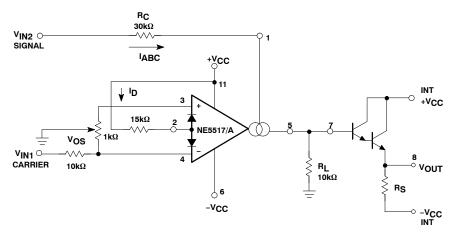


Figure 25. Amplitude Modulator

Voltage-Controlled Resistor (VCR)

Because an OTA is capable of producing an output current proportional to the input voltage, a voltage variable resistor can be made. Figure 26 shows how this is done. A voltage presented at the R_X terminals forces a voltage at the input. This voltage is multiplied by g_M and thereby forces a current through the R_X terminals:

$$R_x = \frac{R + R_A}{g_M + R_A}$$

where g_M is approximately 19.21 μ MHOs at room temperature. Figure 27 shows a Voltage Controlled Resistor using linearizing diodes. This improves the noise performance of the resistor.

Voltage-Controlled Filters

Figure 28 shows a Voltage Controlled Low-Pass Filter. The circuit is a unity gain buffer until X_C/g_M is equal to R/R_A . Then, the frequency response rolls off at a 6dB per octave with the -3 dB point being defined by the given equations. Operating in the same manner, a Voltage Controlled High-Pass Filter is shown in Figure 29. Higher order filters can be made using additional amplifiers as shown in Figures 30 and 31.

Voltage-Controlled Oscillators

Figure 32 shows a voltage-controlled triangle-square wave generator. With the indicated values a range from 2.0 Hz to 200 kHz is possible by varying I_{ABC} from 1.0 mA to 10 μ A.

The output amplitude is determined by $I_{OUT} \times R_{OUT}$.

Please notice the differential input voltage is not allowed to be above 5.0 V.

With a slight modification of this circuit you can get the sawtooth pulse generator, as shown in Figure 33.

APPLICATION HINTS

To hold the transconductance g_M within the linear range, I_{ABC} should be chosen not greater than 1.0 mA. The current mirror ratio should be as accurate as possible over the entire current range. A current mirror with only two transistors is not recommended. A suitable current mirror can be built with a PNP transistor array which causes excellent matching and thermal coupling among the transistors. The output current range of the DAC normally reaches from 0 to -2.0 mA. In this application, however, the current range is set through R_{REF} (10 k Ω) to 0 to -1.0 mA.

$$I_{DACMAX} = 2 \cdot \frac{V_{REF}}{R_{REF}} = 2 \cdot \frac{5V}{10k\Omega} = 1mA$$

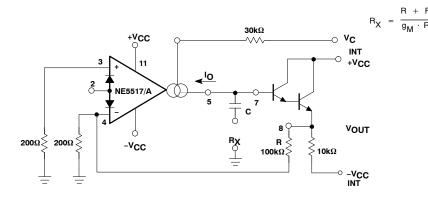


Figure 26. VCR

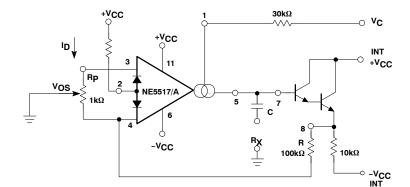
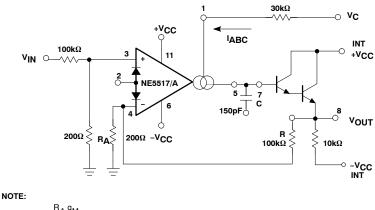
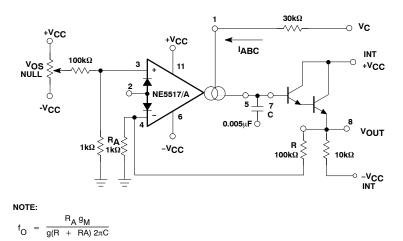


Figure 27. VCR with Linearizing Diodes



 $f_{O} = \frac{R_{A}g_{M}}{g(R + RA) 2\pi C}$

Figure 28. Voltage-Controlled Low-Pass Filter





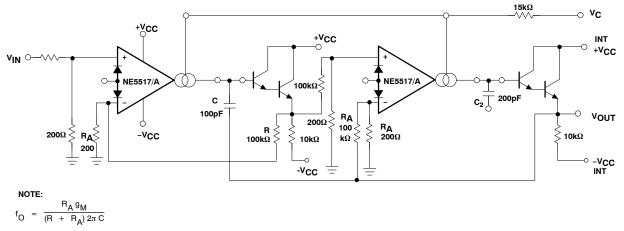


Figure 30. Butterworth Filter – 2nd Order

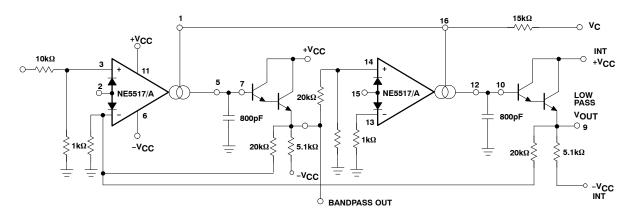


Figure 31. State Variable Filter

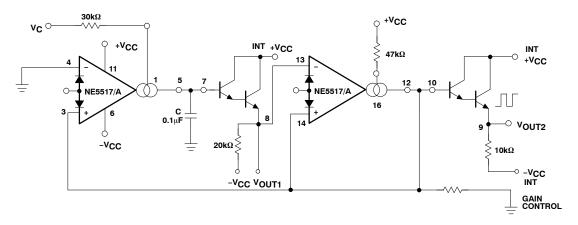


Figure 32. Triangle-Square Wave Generator (VCO)

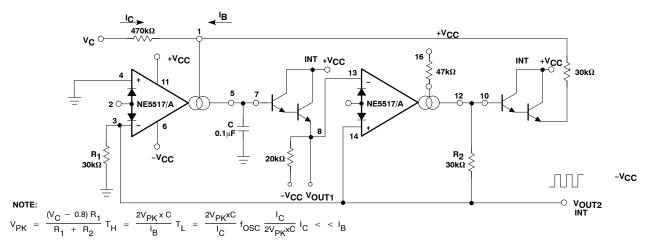


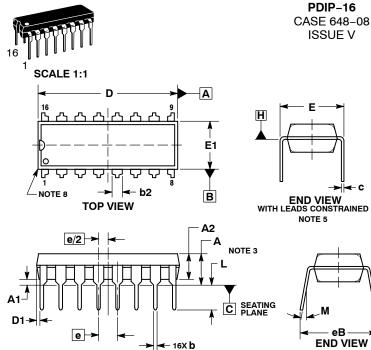
Figure 33. Sawtooth Pulse VCO

ORDERING INFORMATION

| Device | Temperature Range | Package | Shipping [†] | |
|------------|-------------------|----------------------|-----------------------|--|
| AU5517DR2 | | SOIC-16 | | |
| AU5517DR2G | −40 to +125 °C | SOIC-16 (Pb-Free) | 2500 Tape & Reel | |
| NE5517D | | SOIC-16 | | |
| NE5517DG | | SOIC-16 (Pb-Free) | 48 Units/Rail | |
| NE5517DR2 | | SOIC-16 | | |
| NE5517DR2G | | SOIC-16 (Pb-Free) | 2500 Tape & Reel | |
| NE5517N | 0 to +70 °C | PDIP-16 | | |
| NE5517NG | | PDIP-16 (Pb-Free) | | |
| NE5517AN | | PDIP-16 | 25 Units/Rail | |
| NE5517ANG | 1 | PDIP-16 (Pb-Free) | | |

+For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specifications Brochure, BRD8011/D.

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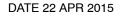


🕀 0.010 🕅 C A 🕅 B 🕅

STYLE 1: STYLE 2: PIN 1. COMMON DRAIN CATHODE CATHODE PIN 1. 2. 2. з. CATHODE 3. COMMON DRAIN COMMON DRAIN 4. 5. CATHODE 4. CATHODE 5. 6. CATHODE 6. COMMON DRAIN 7. CATHODE 7. COMMON DRAIN CATHODE COMMON DRAIN 8. 9. 8. 9. ANODE GATE 10. ANODE 10. SOURCE ANODE ANODE 11. 12. GATE SOURCE 11. 12. 13. ANODE 13. GATE 14. 15. ANODE ANODE 14. 15. SOURCE GATE 16. ANODE 16. SOURCE

SIDE VIEW

NOTE 6



NOTES:

- 1. DIMENSIONING AND TOLERANCING PER ASME Y14.5M, 1994. 2
- 3.
- DIMENSIONING AND TOLERANGURA PER ASIME 114.300, 1994. CONTROLLING DIMENSION: INCHES. DIMENSIONS A, A1 AND L ARE MEASURED WITH THE PACK-AGE SEATED IN JEDEC SEATING PLANE GAUGE GS-3. DIMENSIONS D, D1 AND E1 DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTRUSIONS ARE NOT TO EXCEED 0.10 INCH. 4.
- DIMENSION E IS MEASURED AT A POINT 0.015 BELOW DATUM PLANE H WITH THE LEADS CONSTRAINED PERPENDICULAR 5. TO DATUM C.
- DIMENSION 6B IS MEASURED AT THE LEAD TIPS WITH THE LEADS UNCONSTRAINED. DATUM PLANE H IS COINCIDENT WITH THE BOTTOM OF THE 6.
- 7
- LEADS, WHERE THE LEADS EXIT THE BODY. PACKAGE CONTOUR IS OPTIONAL (ROUNDED OR SQUARE 8 CORNERS).

| | INC | | MILLIMETERS | | |
|-----|-----------|-------|-------------|-------|--|
| DIM | MIN | MAX | MIN | MAX | |
| | IVITIN | | IVITIN | | |
| Α | | 0.210 | | 5.33 | |
| A1 | 0.015 | | 0.38 | | |
| A2 | 0.115 | 0.195 | 2.92 | 4.95 | |
| b | 0.014 | 0.022 | 0.35 | 0.56 | |
| b2 | 0.060 |) TYP | 1.52 TYP | | |
| С | 0.008 | 0.014 | 0.20 | 0.36 | |
| D | 0.735 | 0.775 | 18.67 | 19.69 | |
| D1 | 0.005 | | 0.13 | | |
| Е | 0.300 | 0.325 | 7.62 | 8.26 | |
| E1 | 0.240 | 0.280 | 6.10 | 7.11 | |
| е | 0.100 BSC | | 2.54 BSC | | |
| eВ | | 0.430 | | 10.92 | |
| L | 0.115 | 0.150 | 2.92 | 3.81 | |
| Μ | | 10° | | 10° | |

GENERIC **MARKING DIAGRAM***

| 16 <u> </u> | 1 |
|--|---|
| XXXXXXXXXXXXXX | |
| • XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX | |
| O AWLYYWWG | |
| 1 00000000 | Ţ |

XXXXX = Specific Device Code

- = Assembly Location
- WL = Wafer Lot

А

- YY = Year
- WW = Work Week
- G = Pb-Free Package

*This information is generic. Please refer to device data sheet for actual part marking. Pb-Free indicator, "G" or microdot " .", may or may not be present.

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